



Course of
"Automatic Control Systems"
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Nyquist plots

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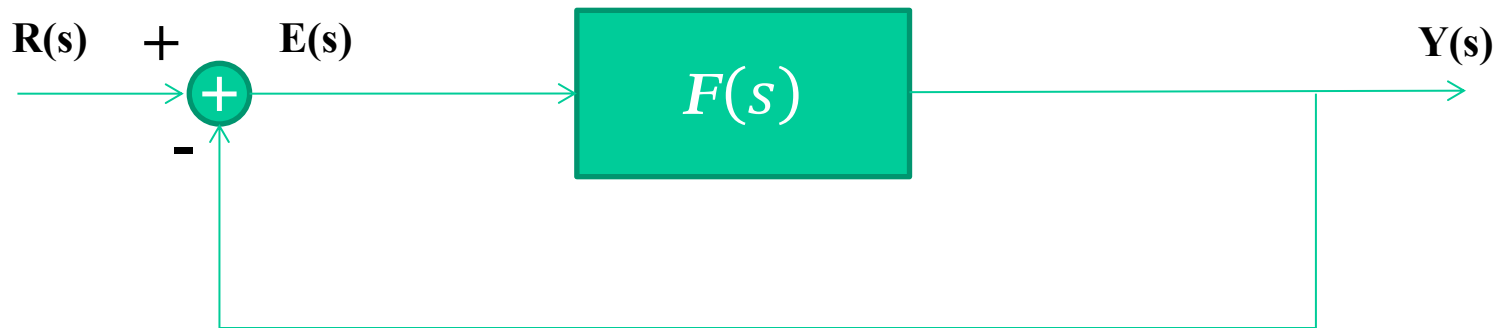
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Team code: **uxbsz19**

Stability of the closed loop system

- Let us consider the $R(s) \rightarrow Y(s)$ closed loop system



- Assume that the **hidden modes** of the open loop function $F(s) = K(s)G(s)$ are asymptotically stable
- The stability of the closed loop system depends on the poles of the transfer function

$$T(s) = \frac{F(s)}{1+F(s)}$$



Stability of the closed loop system

- ✦ Indicate with $N_F(s)$ and $D_F(s)$ the numerator and the denominator of the open loop function

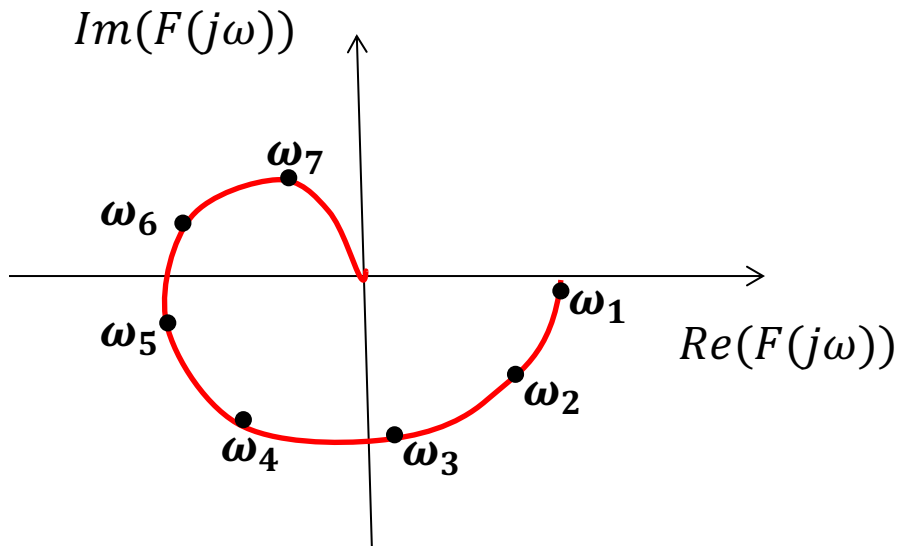
$$F(s) = \frac{N_F(s)}{D_F(s)} = \frac{N_K(s)N_G(s)}{D_K(s)D_G(s)}$$

- ✦ The closed loop function can be written as

$$T(s) = \frac{\frac{N_F(s)}{D_F(s)}}{1 + \frac{N_F(s)}{D_F(s)}} = \frac{N_F(s)}{D_F(s) + N_F(s)}$$

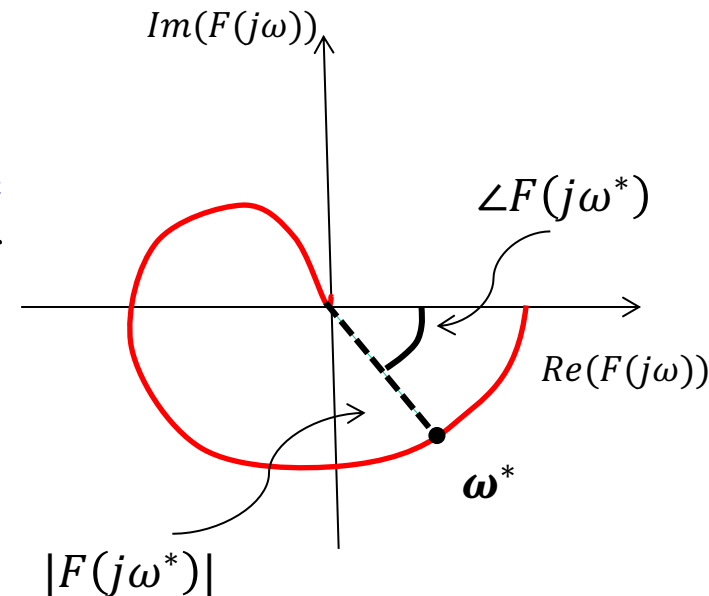
- ✦ The denominator of $T(s)$ is given by the sum of $N_F(s)$ and $D_F(s)$; therefore, the design problem of a controller able to guarantee the stability of the closed loop system is to be very demanding.
- ✦ By means of the Nyquist plots and the *Nyquist criteria*, we are going *to determine the stability of the closed loop system from the open loop system features*

- ▶ *The Nyquist plots are polar diagrams of the transfer function $F(s)|_{s=j\omega}$*



$F(s)$ is represented in the polar plane as a function of $j\omega$ assuming ω moving from 0 to $+\infty$

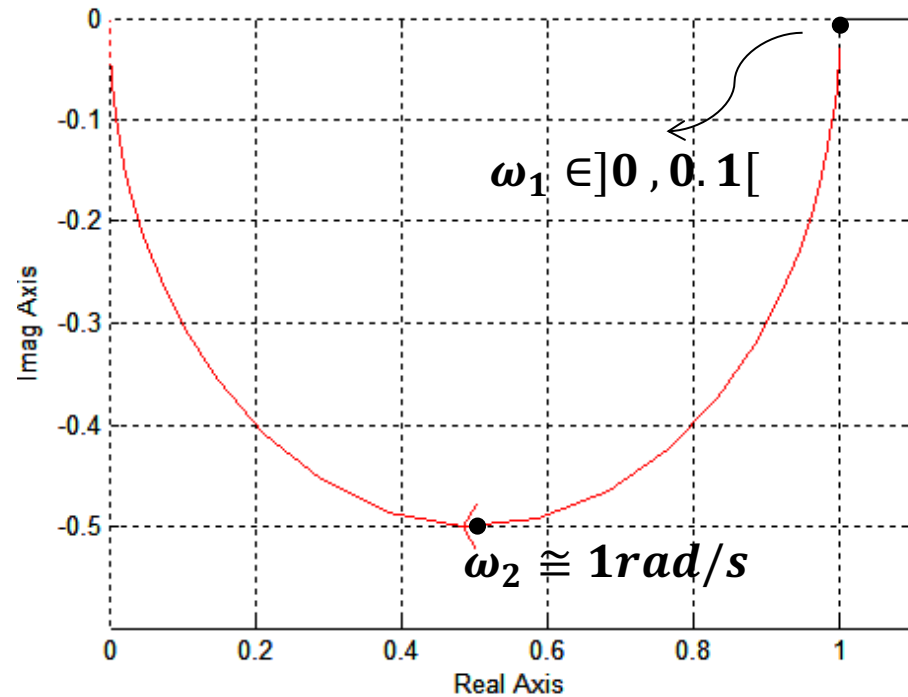
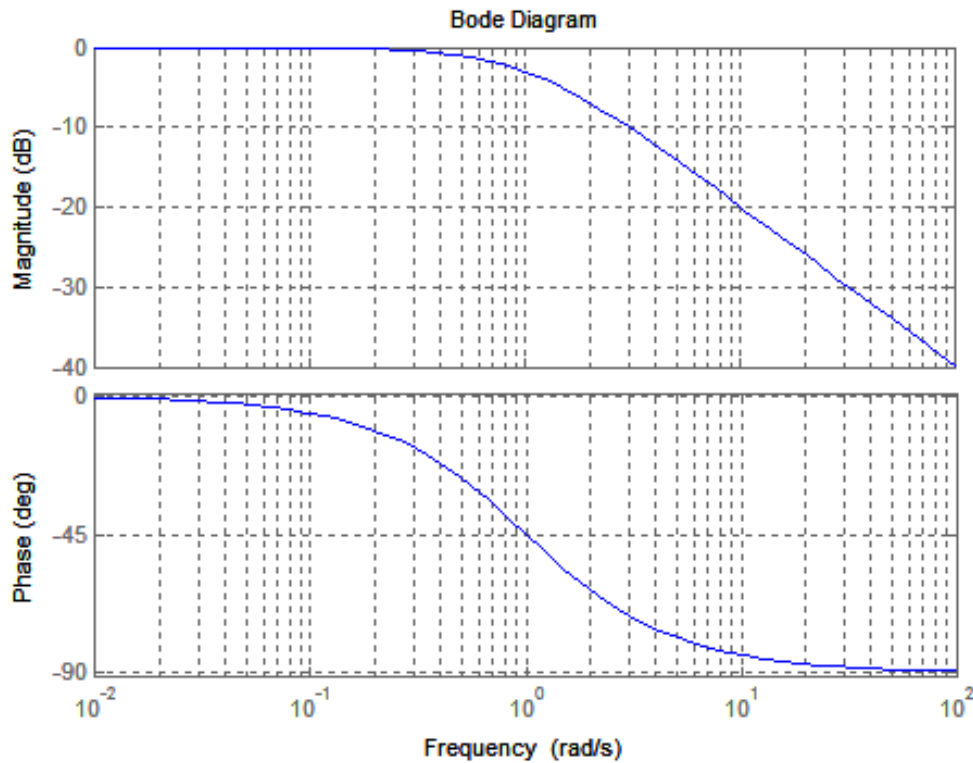
- ▶ They are an alternative solution to the Bode diagrams for the representation of the transfer functions.
- ▶ In a Nyquist plot *magnitude and phase of $F(j\omega)$ are represented by a curve parametrized in ω .*



Nyquist plots: example 1

✦ The Nyquist plots can be obtained from the magnitude and phase Bode plots of

$$F(s) = \frac{1}{1+s}$$



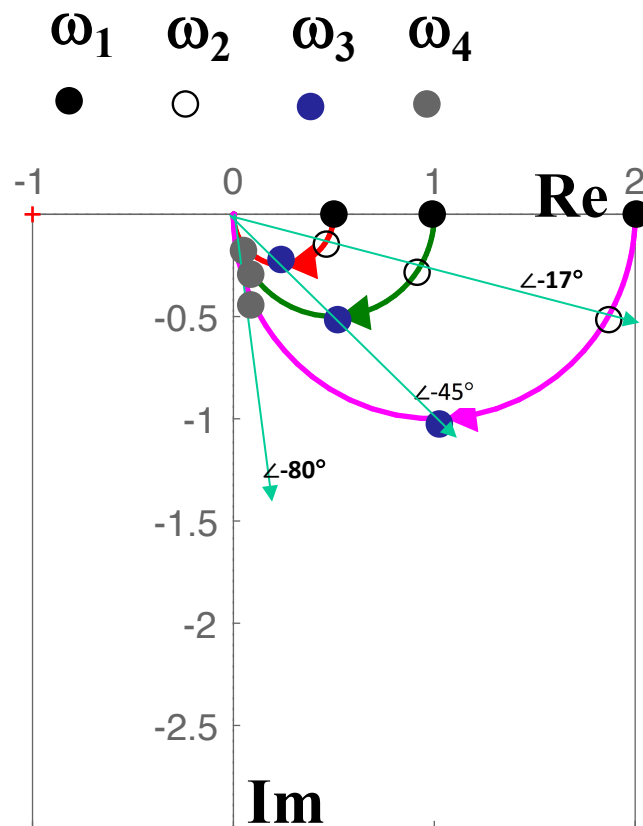
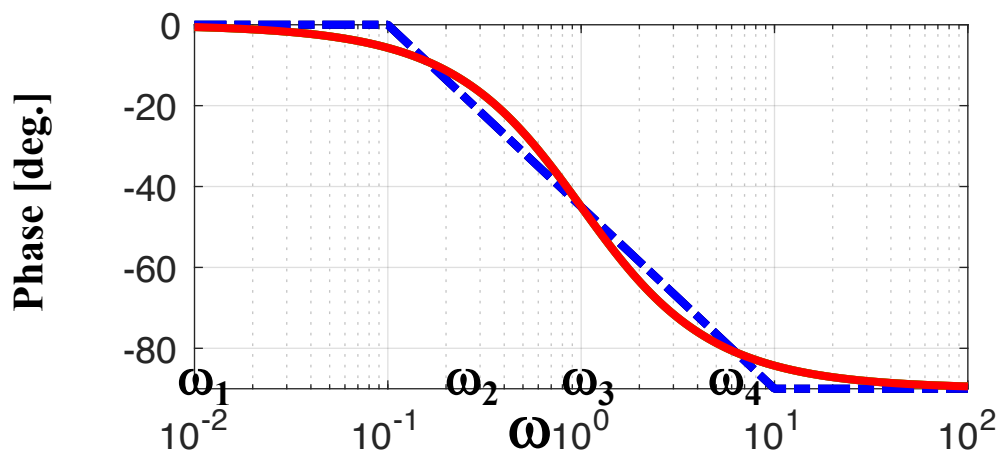
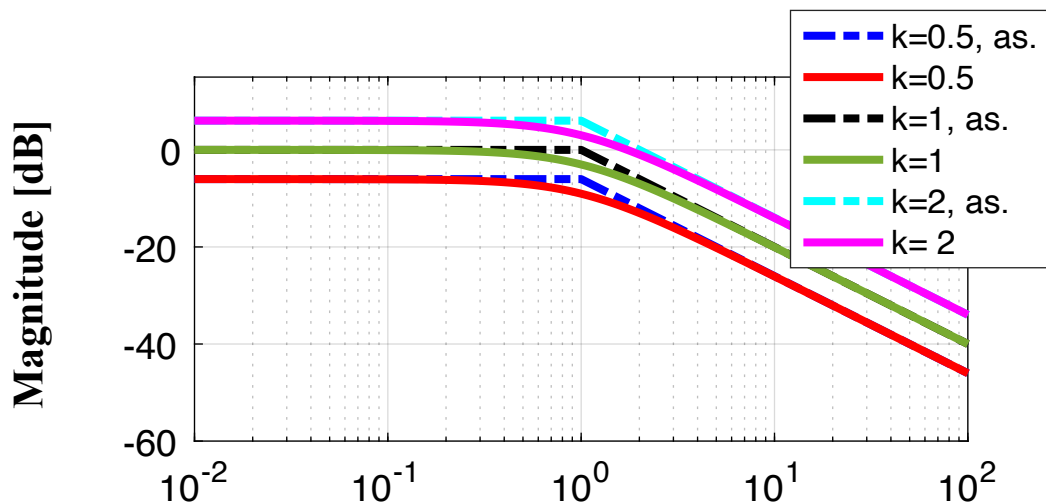
✦ Note that a single point on the Nyquist plots can also indicate the value of $F(j\omega)$ in a finite interval of ω .



Nyquist plots: first-order open loop system

$$F(s) = \frac{k}{1+s\tau}, \quad \tau = 1 \text{ s}, \quad F(j\omega) = F(s)|_{s=j\omega}. \quad |F(j\omega)| = k \left| \frac{1}{1+j\omega\tau} \frac{1-j\omega\tau}{1-j\omega\tau} \right| = \frac{k\sqrt{1+(\omega\tau)^2}}{1+(\omega\tau)^2} = \frac{k}{\sqrt{1+(\omega\tau)^2}};$$

$$|F(j\omega)|_{\text{dB}} = 20\log_{10}|F(j\omega)|; \quad \arg F(j\omega) = -\arg(1+j\omega\tau) = -\tan^{-1}(\omega\tau).$$



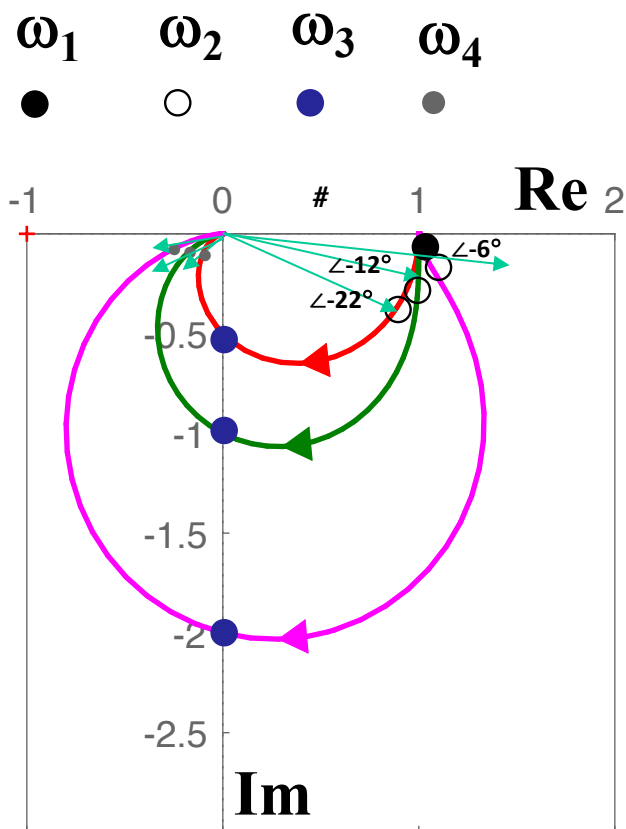
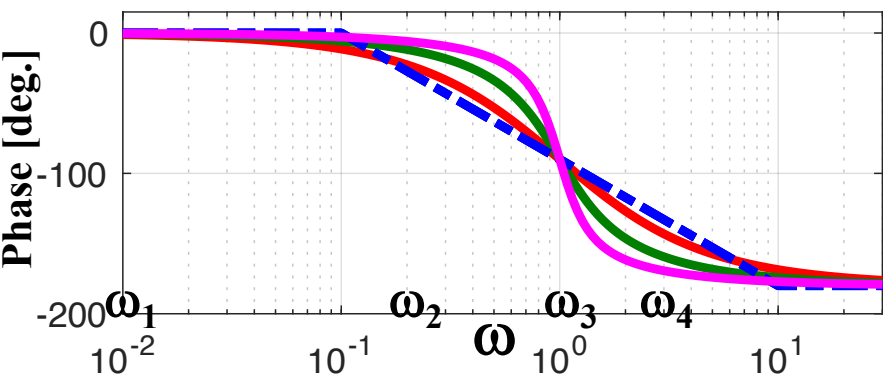
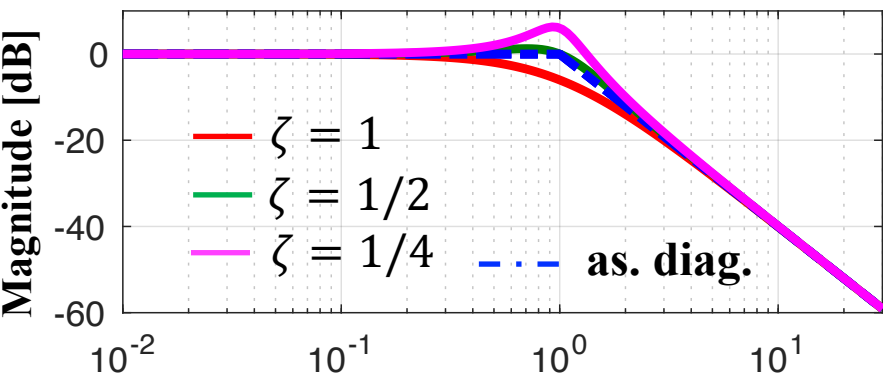


Nyquist plots: second-order open loop system

$$F(s) = \frac{1}{\frac{s^2}{\omega_n^2} + \frac{2\zeta}{\omega_n}s + 1}, \quad \omega_n = 1 \text{ rad/s.}$$

$$|F(j\omega)| = \frac{1}{\sqrt{\left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(\frac{2\zeta}{\omega_n}\right)^2}}, \quad \arg F(j\omega) = -\tan^{-1} \frac{\frac{2\zeta}{\omega_n}}{1 - \frac{\omega^2}{\omega_n^2}}.$$

$$|F(j\omega)|_{\text{dB}} = -20 \log_{10} \sqrt{\left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(\frac{2\zeta}{\omega_n}\right)^2}$$



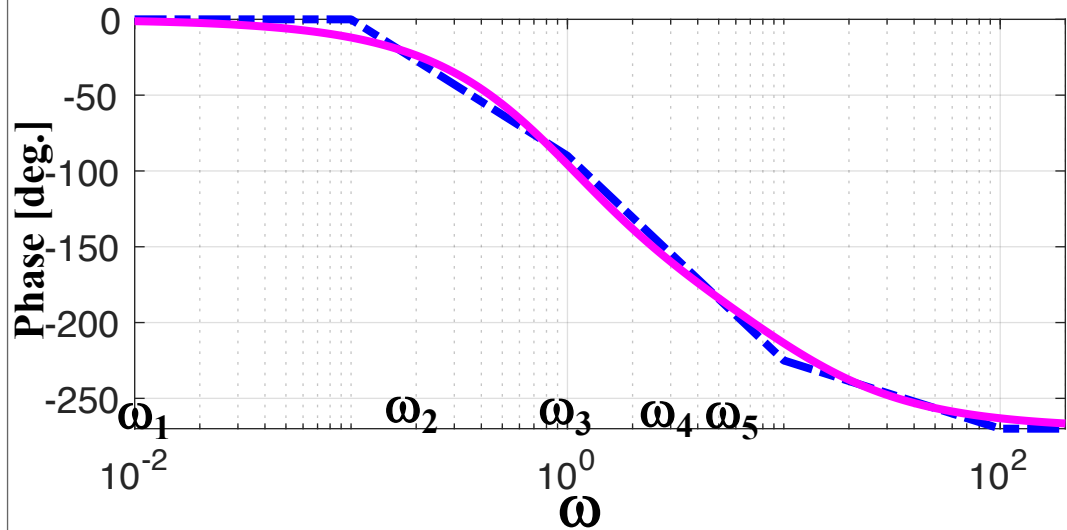
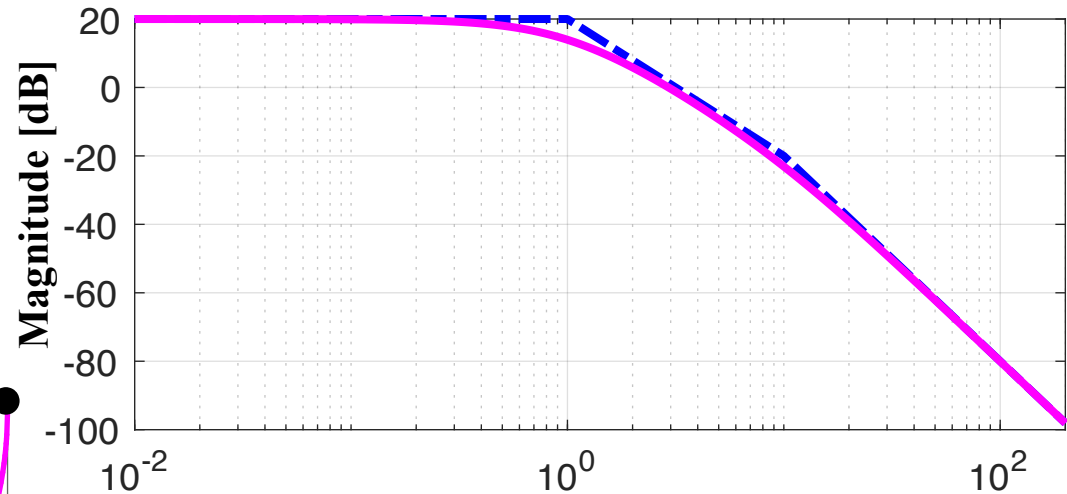
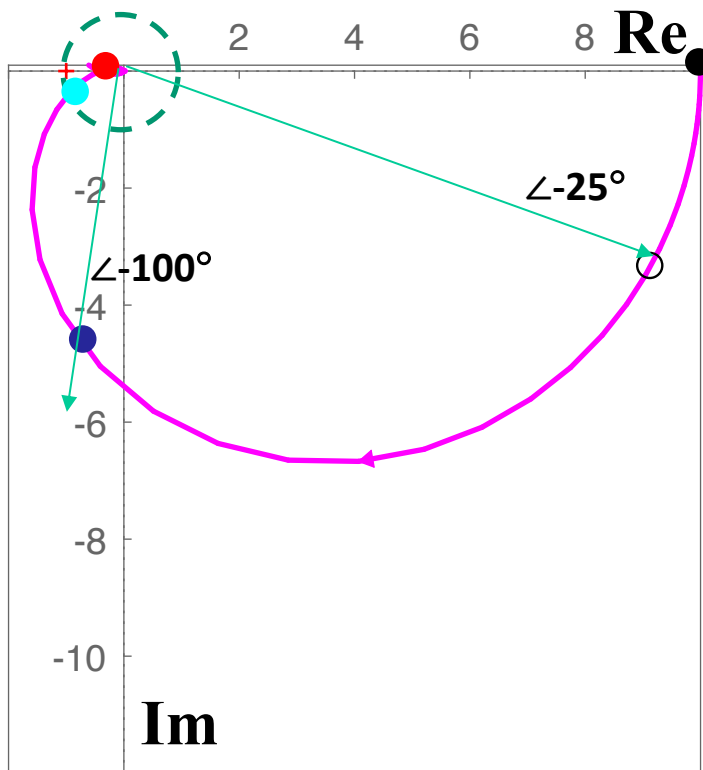


Nyquist plots: third-order open loop system

$$F(s) = \frac{10}{(s^2 + 2s + 1) \left(\frac{s}{10} + 1\right)}$$

ω_1 ω_2 ω_3 ω_4 ω_5

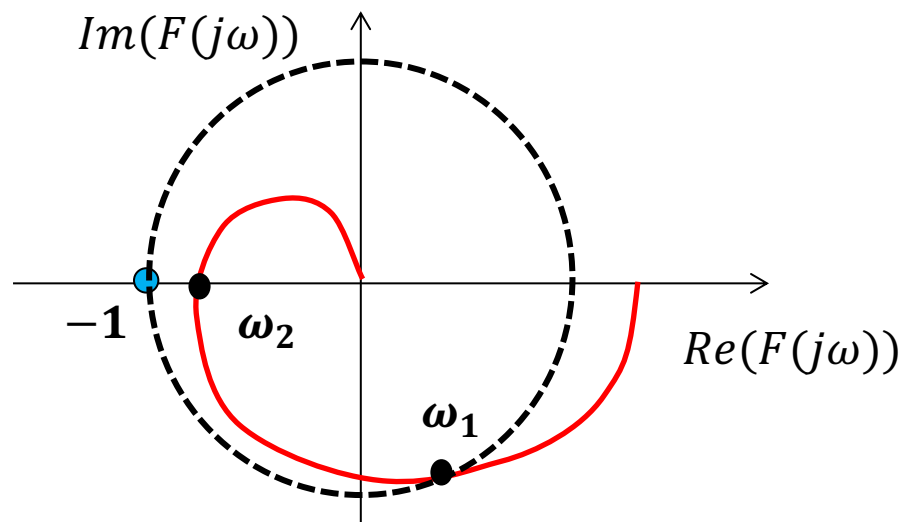
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- ✦ A precise representation of the Nyquist plots from magnitude and phase Bode plots isn't an easy job.
- ✦ However, if we focus on the closed loop stability performance, **only a limited set of points on the Nyquist point need to be traced precisely:**

1. *Intersection of the diagram with the unit circle*
2. *Intersection of the diagram with the negative real axis.*

Indeed, it is of interest to verify if the diagram intersects, encircles the **Critical point $-1 + j0$**





Phase variation

- For the analysis of closed loop system an important parameter to be considered is the *Phase Variation*

$$\Delta \angle F(j\omega)$$

$-\infty \quad \omega \quad \infty$

defined as the phase variation of $F(j\omega)$ when ω moves from $-\infty$ to ∞ counted positive if counterclockwise.

- In order to evaluate the phase variation we also need to plot $F(j\omega)$ when ω moves from $-\infty$ to 0 .
- For polynomial functions

$$\operatorname{Re}(F(-j\omega)) = \operatorname{Re}(F(j\omega)) \quad \textit{Pair function}$$

$$\operatorname{Im}(F(-j\omega)) = -\operatorname{Im}(F(j\omega)) \quad \textit{Odd function}$$

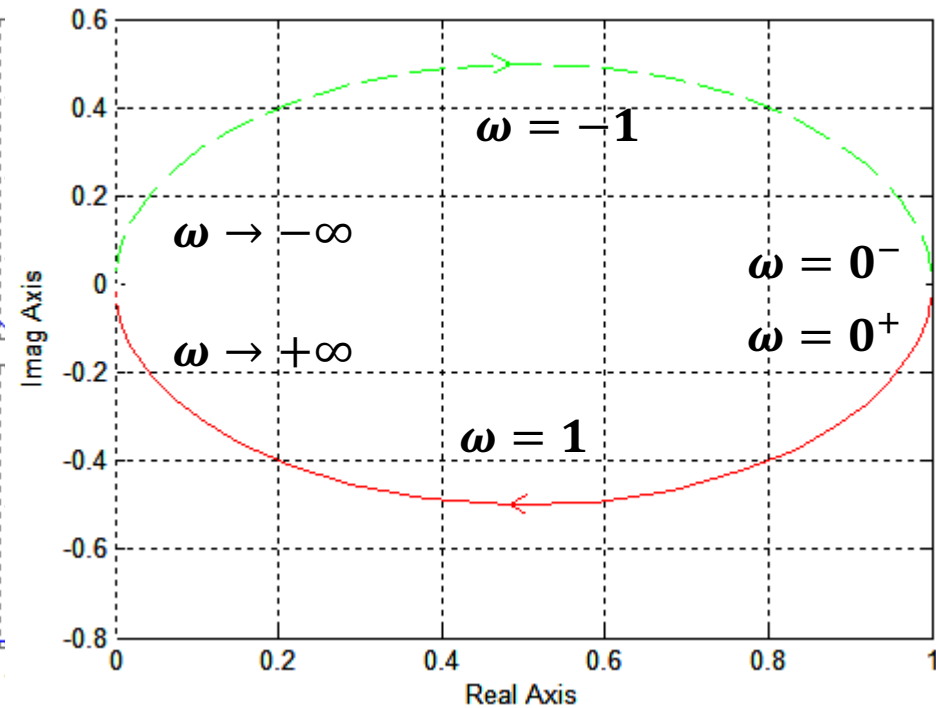
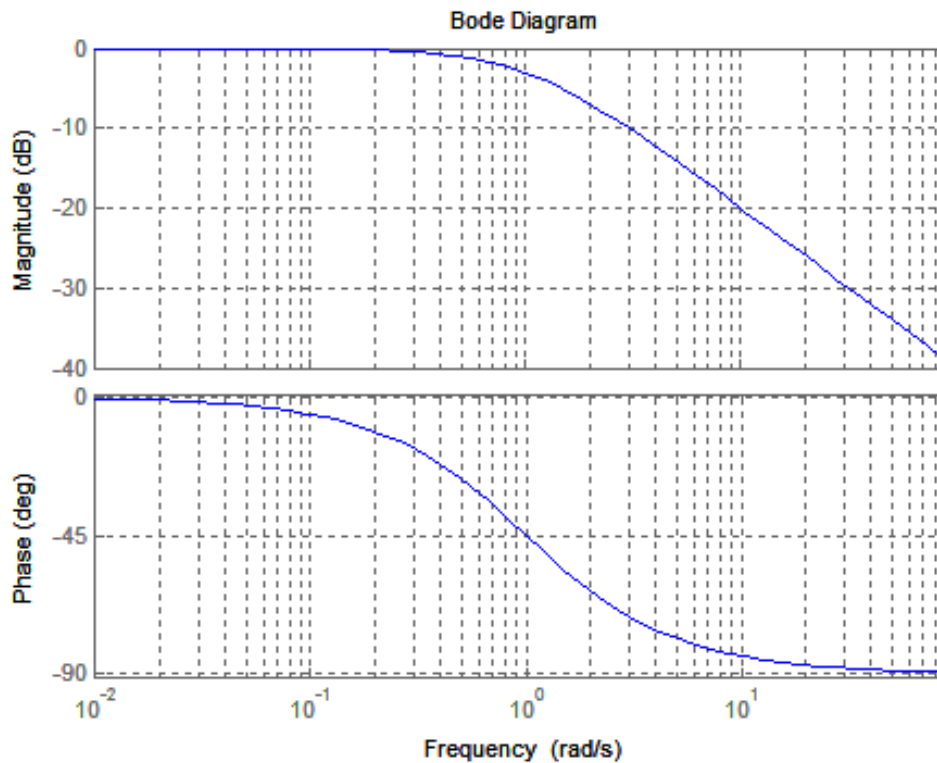
- Hence, the Nyquist plots of $F(j\omega)$ for negative and positive angular frequencies are symmetric wrt the real axis.



Nyquist plot and phase variation: example

Let us consider again the transfer function

$$F(s) = \frac{1}{1+s}$$



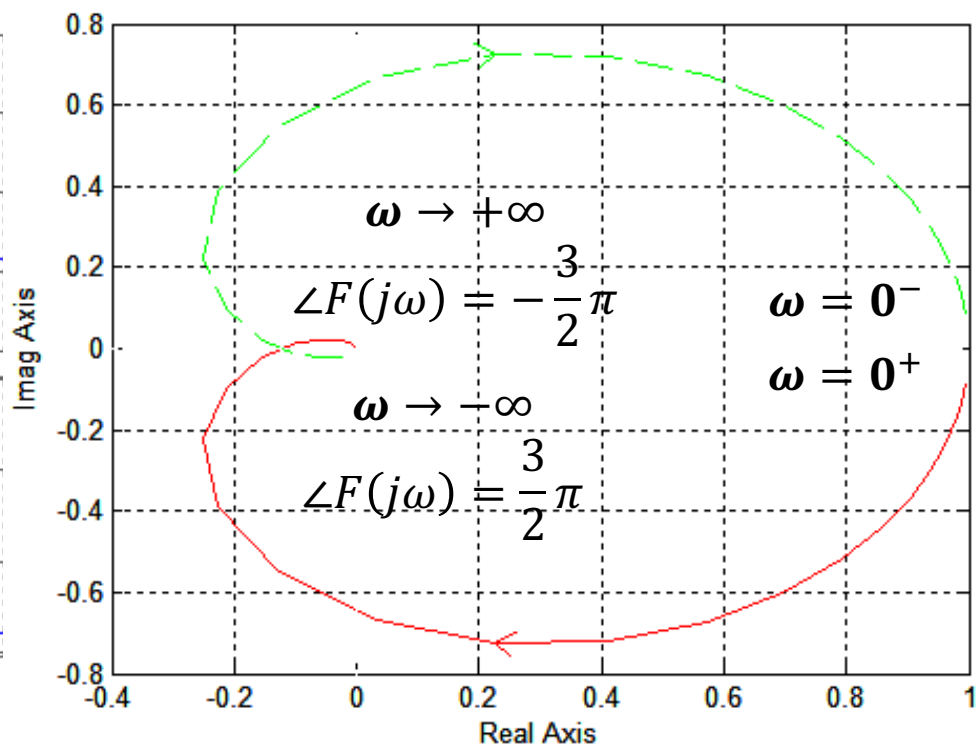
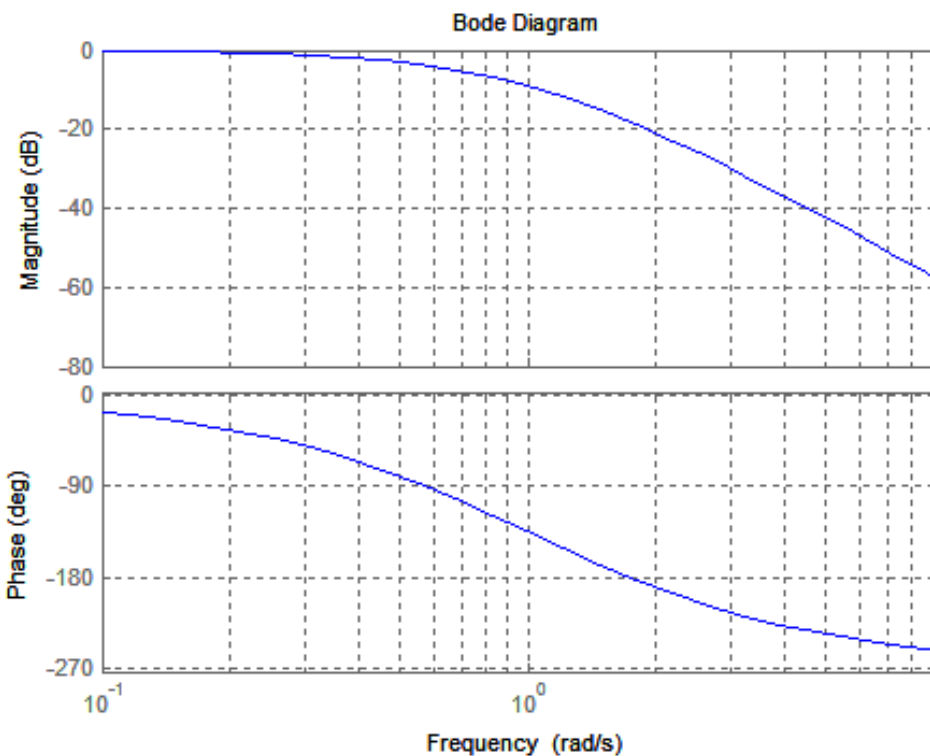
$$\Delta \angle F(j\omega) \Big|_{-\infty}^{\infty} = -\pi$$



Nyquist plot and phase variation: example

Let us consider the transfer function

$$F(s) = \frac{1}{(1+s)^3}$$



$$\Delta \angle F(j\omega) = -3\pi$$

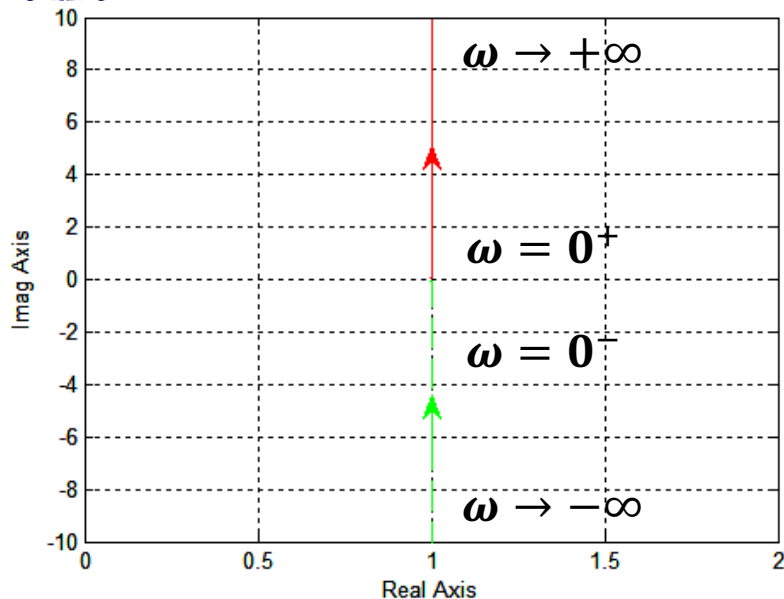
$-\infty \quad \omega \quad \infty$



Formula for the phase variation

- ✦ In the following we propose a *formula for the phase variation* of a transfer function $F(j\omega)$ as a function of the number and sign of $F(j\omega)$ poles and zeros
- ✦ We will *first* evaluate the *phase variation* due to real no null poles and zeros.
- ✦ *Then*, we will extend the evaluation to the case of *complex* poles and zeros having a *null real part*.

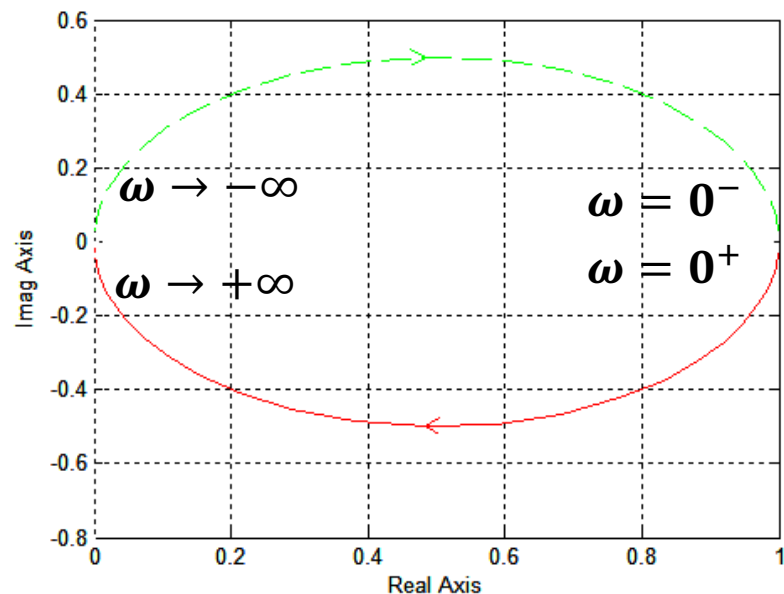
Phase variation for negative real poles and zeros



Negative real zero ($\tau > 0$)

$$F(s) = 1 + \tau s \rightarrow \Delta \angle F(j\omega) = \pi$$

$\begin{matrix} \curvearrowright \\ -\infty & \omega & \infty \\ \curvearrowleft \end{matrix}$



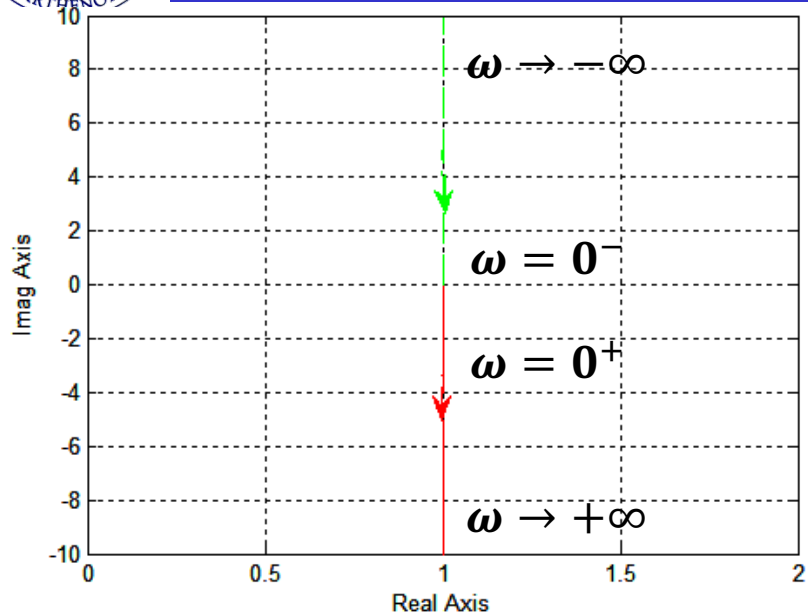
Negative real pole ($\tau > 0$)

$$F(s) = \frac{1}{1 + \tau s} \rightarrow \Delta \angle F(j\omega) = -\pi$$

$\begin{matrix} \curvearrowright \\ -\infty & \omega & \infty \\ \curvearrowleft \end{matrix}$



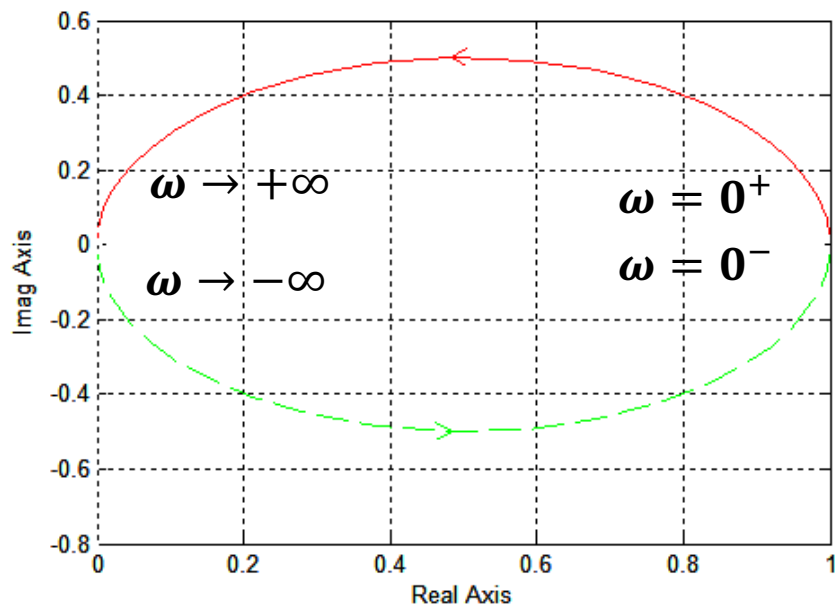
Phase variation for positive real poles and zeros



Positive real zero ($\tau < 0$)

$$F(s) = 1 + \tau s \rightarrow \Delta \angle F(j\omega) = -\pi$$

$-\infty \quad \omega \quad \infty$



Positive real pole ($\tau < 0$)

$$F(s) = \frac{1}{1 + \tau s} \rightarrow \Delta \angle F(j\omega) = \pi$$

$-\infty \quad \omega \quad \infty$



Phase variation for complex poles with $\zeta \neq 0$

Negative complex poles ($\zeta > 0$)

$$F(s) = \frac{1}{1 + \frac{2\zeta}{\omega_n}s + \frac{s^2}{\omega_n^2}} \rightarrow \Delta \angle F(j\omega) = -2\pi$$

Positive complex poles ($\zeta < 0$)

$$F(s) = \frac{1}{1 + \frac{2\zeta}{\omega_n}s + \frac{s^2}{\omega_n^2}} \rightarrow \Delta \angle F(j\omega) = 2\pi$$

Negative complex zeros ($\zeta > 0$)

$$F(s) = 1 + \frac{2\zeta}{\omega_n}s + \frac{s^2}{\omega_n^2} \rightarrow \Delta \angle F(j\omega) = 2\pi$$

Negative complex zeros ($\zeta < 0$)

$$F(s) = 1 + \frac{2\zeta}{\omega_n}s + \frac{s^2}{\omega_n^2} \rightarrow \Delta \angle F(j\omega) = -2\pi$$



Phase variation formula

- ✦ The previous results allows to relate the phase variation to the number and sign of poles/zeros of the transfer function.

Given a transfer function $F(j\omega)$, said:

- n the total number of poles
- m the total number of zeros
- n_p (n_n) the number of poles with positive (negative) real part
- m_p (m_n) the total number of zeros with positive (negative) real part

$$n = n_n + n_p \quad m = m_n + m_p$$

$$\begin{aligned} \Delta \angle F(j\omega) &= \pi(m_n - n_n) - \pi(m_p - n_p) \\ \int_{-\infty}^{\infty} \Delta \angle F(j\omega) &= \pi(m - n) - 2\pi(m_p - n_p) \end{aligned}$$