



Course of "Automatic Control Systems"
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Control system requirements

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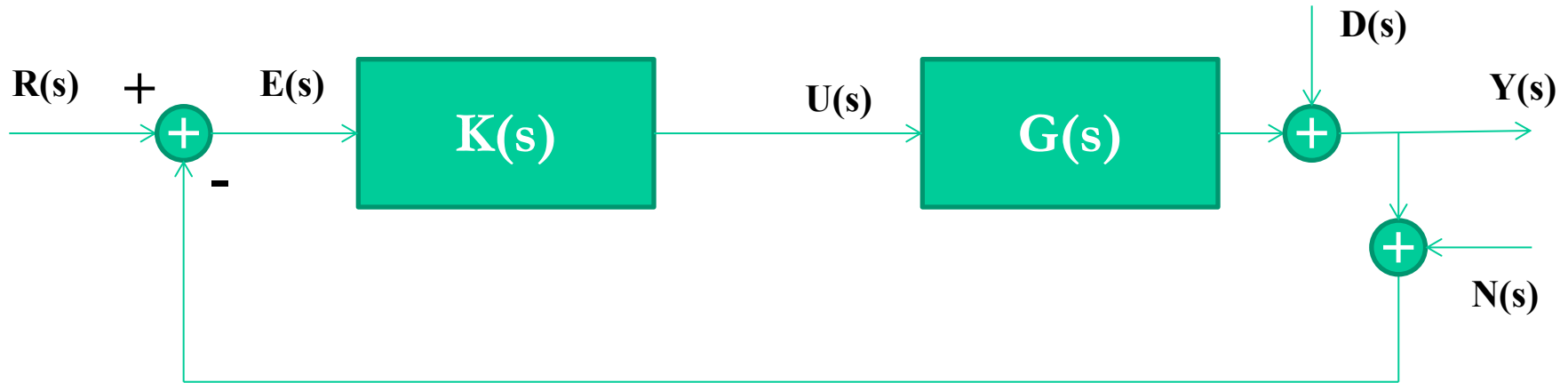
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Closed loop transfer function

✦ A SISO closed loop control system in the Laplace domain can be indicated as



- $G(s)$ plant to be controlled
- $K(s)$ controller
- $R(s)$ reference
- $Y(s)$ controlled output
- $U(s)$ control variable
- $E(s)$ tracking error
- $D(s)$ disturb
- $N(s)$ measurement noise

Closed loop function

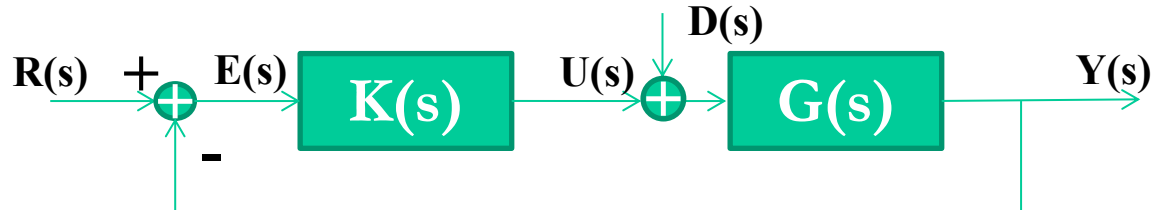
$$W(s) = \frac{Y(s)}{R(s)} = \frac{G(s)K(s)}{1 + G(s)K(s)}$$

$$(N(s)=0; D(s)=0)$$

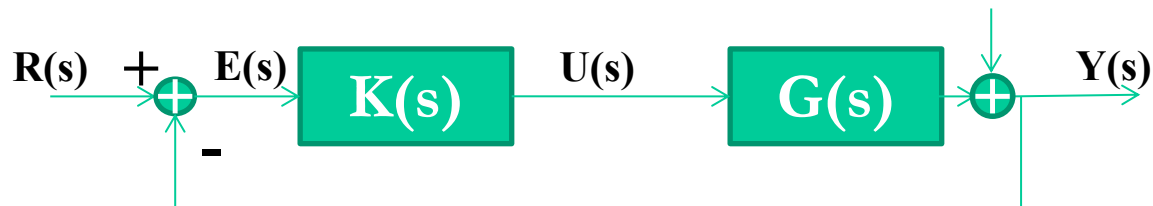


Closed loop function

- The *transfer function* $G(s)$ usually contains the plant and the actuator and the sensors dynamics.
- In the previous scheme, the *disturb signal* $D(s)$ is additive on the output. In other cases, it could also be summed to the plant input.

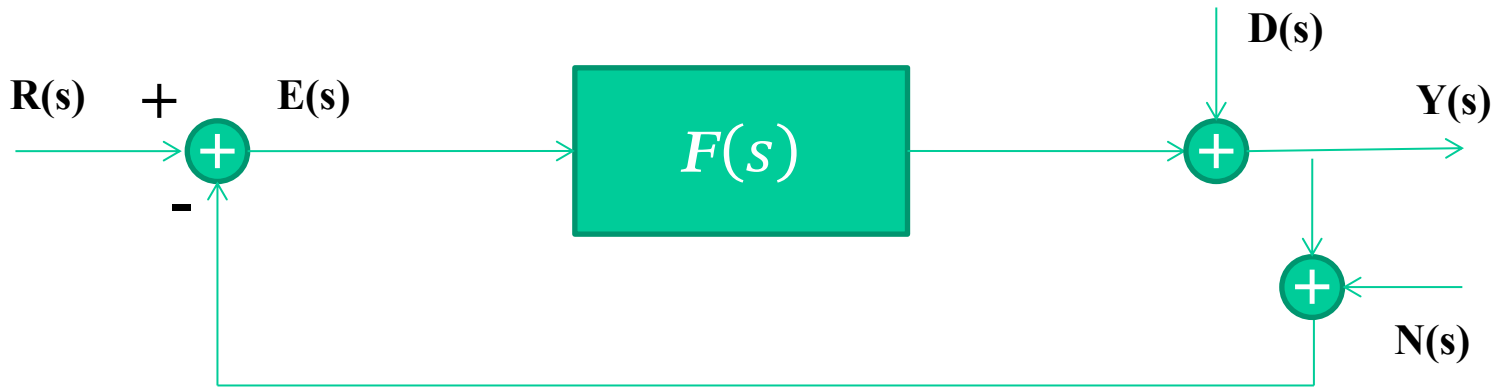


$$D'(s) = G(s)D(s)$$



Open loop function $F(s)$

- The transfer function given by the series of controller $K(s)$ and plant $G(s)$ is called *Open Loop (O.L.) function* $F(s) = G(s)K(s)$



- The O.L. function $F(s)$ assumes a main role in the control theory
- Indeed, it is easier to design a controller $K(s)$ able to modify as desired $F(s)$ instead of closed loop function $W(s) = \frac{G(s)K(s)}{1+G(s)K(s)}$
- It makes important to transform the closed loop requirements in terms of $F(s)$ constraints.



Control requirements

- ✦ The closed loop control requirements can be divided in four classes:
 - ✦ *Stability*
 - ✦ *Robust stability*
 - ✦ *Steady-state performances*
 - ✦ *Transient performances*
- ✦ The control requirements must be verified taking into account **the limits of the actuators.**
- ✦ In this lesson we will introduce the main parameters usually used to quantify the set of requirements
- ✦ Then we will care about how to **transform the requirements in terms of open loop function $F(s)$ constraints**



Stability

- ✦ The asymptotic stability of the nominal closed loop system is the most important property to be guaranteed.
- ✦ The asymptotic stability of the closed loop system implies that all the poles of the transfer function

$$W(s) = \frac{G(s)K(s)}{1 + G(s)K(s)} = \frac{F(s)}{1 + F(s)}$$

have negative real part.

- ✦ The poles of $W(s)$ are the roots of the polynomial

$$\text{num}(F(s)) + \text{den}(F(s))$$



Stability

- ⤴ However, it is difficult to design the controller $K(s)$ such that the roots of
$$\text{num}(F(s)) + \text{den}(F(s))$$
have negative real parts
- ⤴ Routh criterion is useful for the system analysis but not for the control design
- ⤴ The *Nyquist criterion* provides a necessary and sufficient condition for the stability of the closed loop system related to the behavior of the open loop transfer function $F(s)|_{s=j\omega}$.

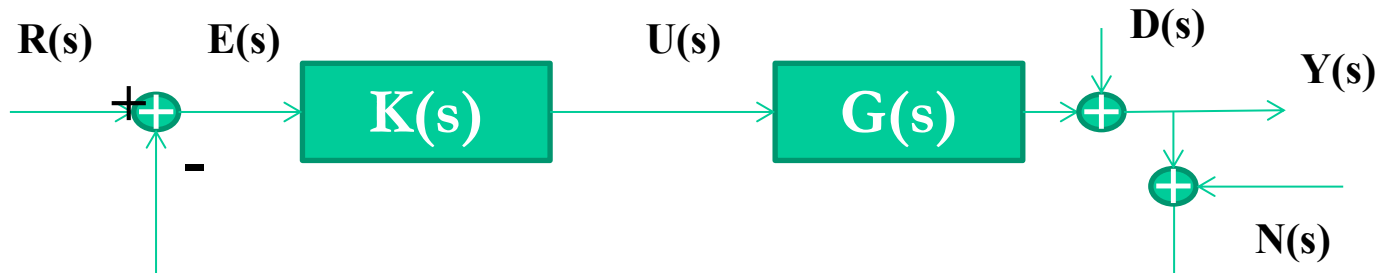


Robust Stability

- ✦ Due to *model uncertainties* (uncertain parameters, model simplification, linearization), it is usually required a controller assuring the asymptotic stability of the C.L. system with a certain ‘*safety margin*’.
- ✦ This concept is called *robust stability* of the closed loop system.
- ✦ The robust stability of the closed loop system *depends on the class and the range of uncertainties*.
- ✦ The *stability margins (gain and phase margins)* relate the robust stability of the closed loop system to the behavior of the open loop transfer function $F(s)|_{s=j\omega}$

Closed loop tracking performances

- ⤴ The performance of the closed loop system are evaluated in terms of
 - ✦ *Tracking of the reference input*
 - ✦ *Rejection of the disturbs*
 - ✦ *Insensibility to the noise*



- ⤴ When the stability of the C.L. system is guaranteed, the responses of the system can be divided in a transient and a steady-state parts.
- ⤴ The *steady-state performance* cares about the steady-state behavior of the closed loop system while the *transient performance* cares about the tracking of the reference signal during the transient phase



Steady-state performance

- ✧ The steady-state performance depends on the class of input signals $R(s)$, $D(s)$, $N(s)$ and the type of transfer function $F(s)$

Tracking of the reference input $R(s)$

- ✧ Null or bounded steady-state error to *polynomial inputs* (step, ramp,...)
- ✧ Null or bounded error to *sinusoidal inputs* at fixed frequency

✧ *Rejection of the disturbs $D(s)$*

- ✧ Null or bounded steady-state error to *polynomial inputs*
- ✧ Bounded error to *multi-frequency sinusoidal inputs*

✧ *Insensibility to the noise $N(s)$*

- ✧ Bounded error to *multi-frequency sinusoidal inputs*

Due to the superposition principle, the three requirements are treated separately

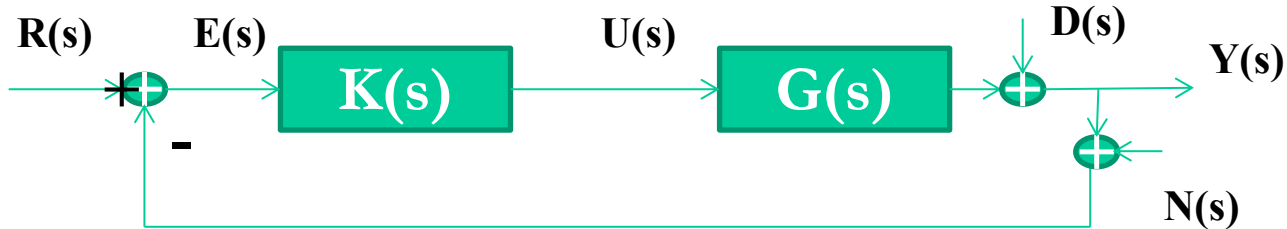


Transient performance

- ✦ The *transient performance* are usually expressed in terms of *tracking properties* of the reference signal $R(s)$.
- ✦ $R(s)$ is usually assumed as a *polynomial signal of order 0 (step)*
- ✦ The transient performance can be classified in
 - ✦ *Dynamic precision performance* (overshoot, oscillation period ...)
 - ✦ *Time response performance* (rise time, peak time, settling time...)
- ✦ The rejection of the disturbs is usually not included among the transient performance because the transfer functions $R(s) \rightarrow Y(s)$ and $D(s) \rightarrow Y(s)$ have the same poles (excluding poles-zeros cancellation).

Closed loop functions

- From the previous analysis, it turns out that the closed loop performance depends on the relations between the input and outputs on the systems
- The closed loop system has three inputs $R(s)$, $D(s)$, $N(s)$ and three outputs $E(s)$, $U(s)$, $Y(s)$.



- The dynamic relations between inputs and outputs of the systems are expressed by 9 transfer functions.



Closed loop functions

- ✦ The 9 transfer functions connecting inputs and outputs depends by three main functions

$$\begin{pmatrix} Y(s) \\ E(s) \\ U(s) \end{pmatrix} = \begin{pmatrix} \mathbf{T}(s) & \mathbf{S}(s) & * \\ * & * & * \\ \mathbf{Q}(s) & * & * \end{pmatrix} \begin{pmatrix} R(s) \\ D(s) \\ N(s) \end{pmatrix}$$

- ✦ $\mathbf{T}(s) = \frac{G(s)K(s)}{1+G(s)K(s)}$ *COMPLEMENTARY SENSITIVITY FUNCTION*

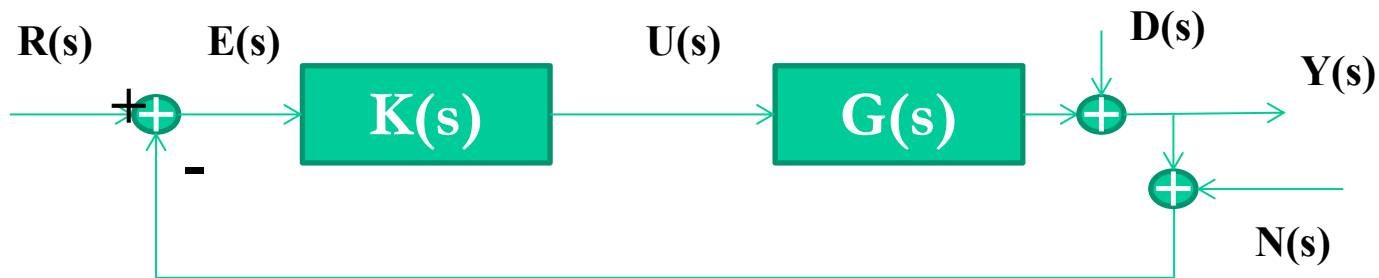
- ✦ $\mathbf{S}(s) = \frac{1}{1+G(s)K(s)}$ *SENSITIVITY FUNCTION*

- ✦ $\mathbf{Q}(s) = \frac{K(s)}{1+G(s)K(s)}$ *CONTROL SENSITIVITY FUNCTION*



Closed loop functions

- ▲ The nine input-output relations can be written as functions of $T(s)$, $S(s)$, $Q(s)$



$$\begin{pmatrix} Y(s) \\ E(s) \\ U(s) \end{pmatrix} = \begin{pmatrix} T(s) & S(s) & -T(s) \\ S(s) & -S(s) & -S(s) \\ Q(s) & -Q(s) & -Q(s) \end{pmatrix} \begin{pmatrix} R(s) \\ D(s) \\ N(s) \end{pmatrix}$$



Ideal control performance

✦ The performance of the closed loop system have been classified in

✦ *Tracking of the reference input* → $T(s) = \mathbf{1}$

✦ *Rejection of the disturbs* → $S(s) = \mathbf{0}$

✦ This is in accordance with the fact that

$$T(s) + S(s) = \frac{G(s)K(s)}{1 + G(s)K(s)} + \frac{1}{1 + G(s)K(s)} = \mathbf{1}$$



Ideal control performance

✧ However this choice has two main drawbacks

1. $Q(s) = T(s)G^{-1}(s) = G^{-1}(s)$

If the plant is strictly proper, $Q(s)$ is improper and it causes a **very high or infinity request of the control input for $t \rightarrow 0$** (initial value theorem)

2. $Y(s) = T(s)R(s) + S(s)D(s) - T(s)N(s),$

The noise is not filtered by the system



Real control performance

- ✦ To overcome these problems the control theory takes advantage to the fact that the input signals have usually different intervals of frequency
 - ✦ *Reference and disturbs at low frequencies*
 - ✦ *Noise at high frequencies*
- ✦ So, a rule of thumb is to choose
 - ✦ $T(s) = 1$ and $S(s) = 0$ at low frequencies
 - ✦ $T(s) = 0$ at high frequencies
- ✦ In this way also the problem related to the input signal is reduced.