

# **Campi Elettromagnetici**

**Corso di Laurea in Ingegneria Informatica,  
Biomedica e delle Telecomunicazioni**

**a.a. 2020-2021 - Laurea "Triennale" – Secondo semestre - Secondo anno**

**Università degli Studi di Napoli "Parthenope"**

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# Color legend

New formulas, important considerations,  
important formulas, important concepts

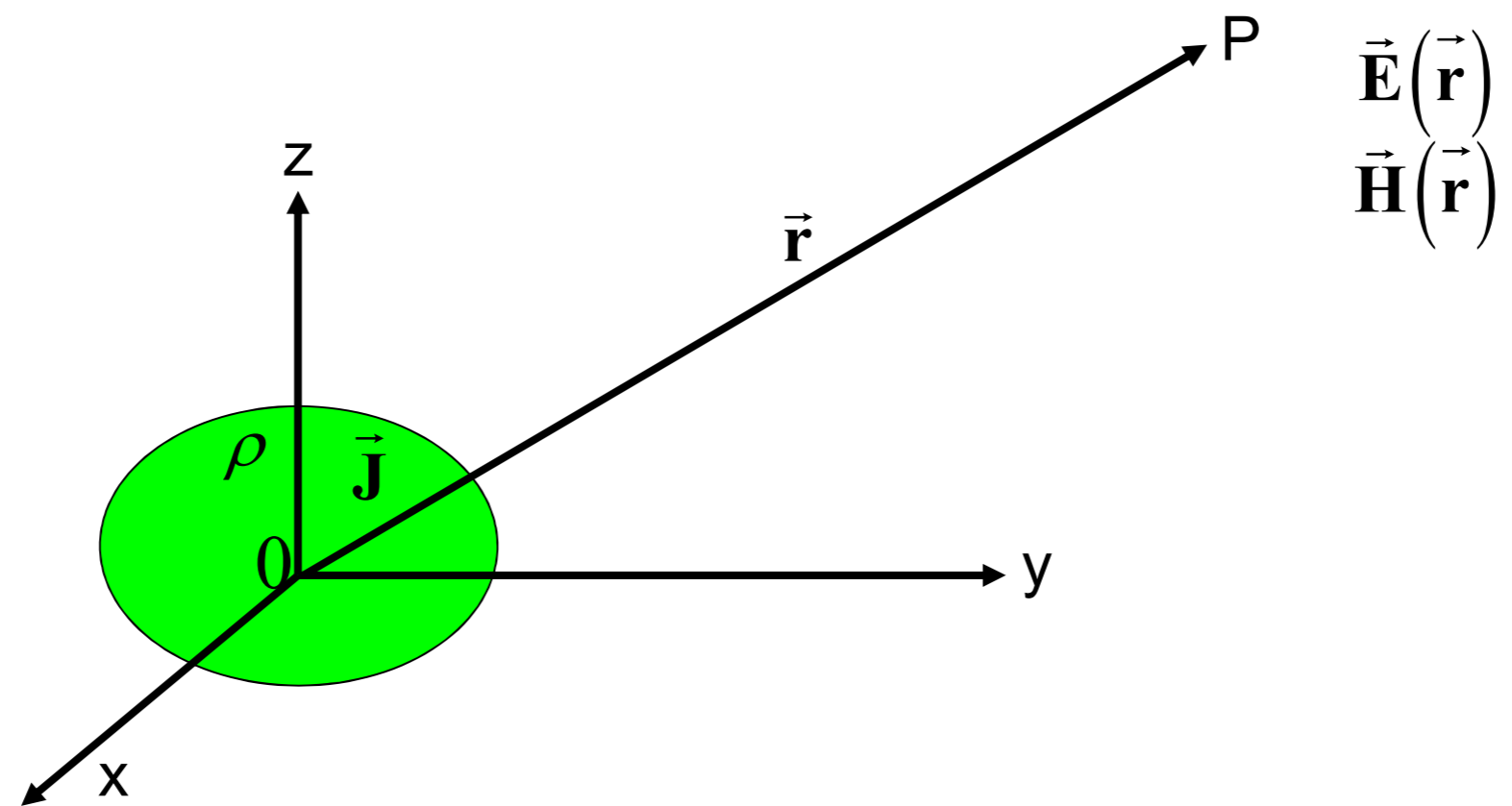
Very important for the discussion

Memo

Mathematical tools to be exploited

Mathematics

# Radiation problem



# Potentials

↓  $\mathbf{J}(\mathbf{r})$

$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$

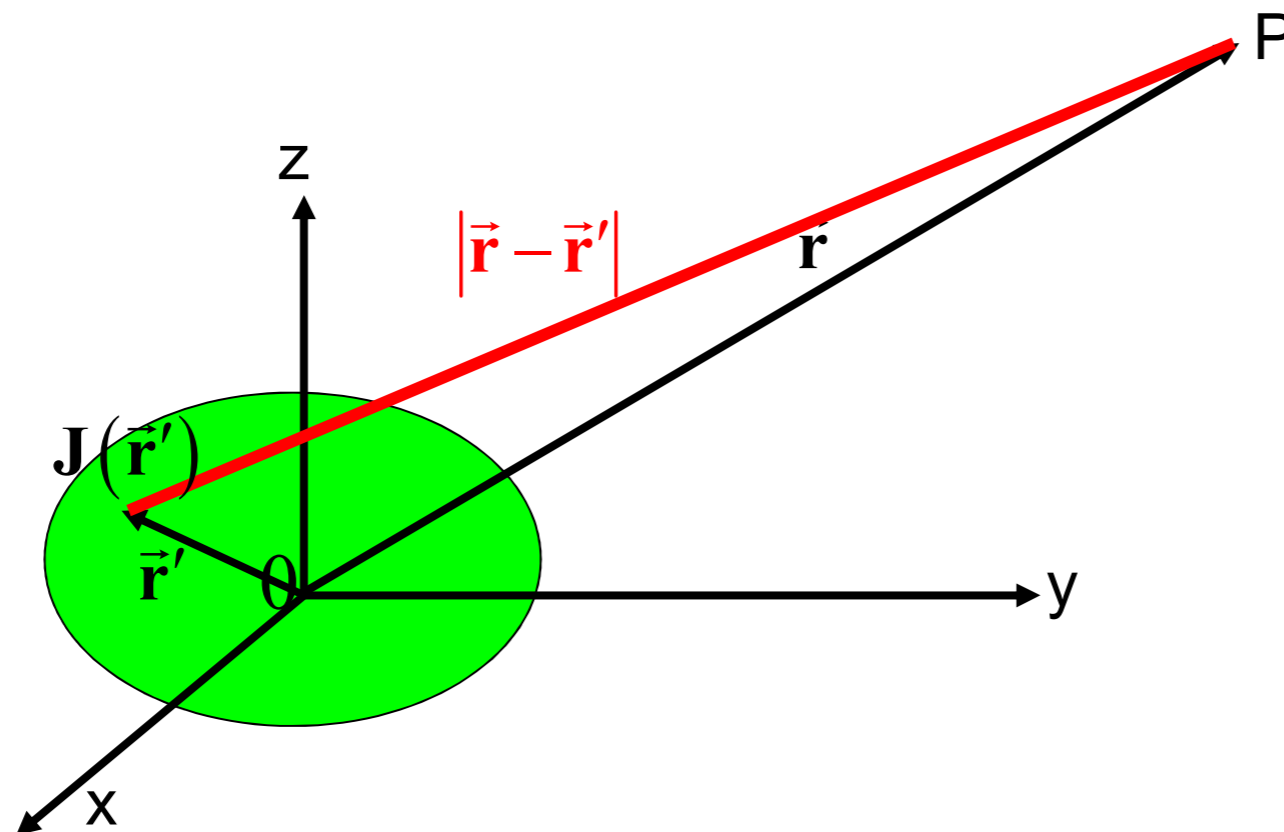
$$\downarrow \mathbf{A}(\mathbf{r}) = \frac{\mu}{4\pi} \int \mathbf{J}(\mathbf{r}') \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} d\mathbf{r}'$$

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} \quad \text{and} \quad \mathbf{E} = -j\omega \mathbf{A} + \frac{\nabla \nabla \cdot \mathbf{A}}{j\omega \epsilon \mu}$$

↓  $\mathbf{E}(\mathbf{r})$   
 $\mathbf{H}(\mathbf{r})$

# Potentials

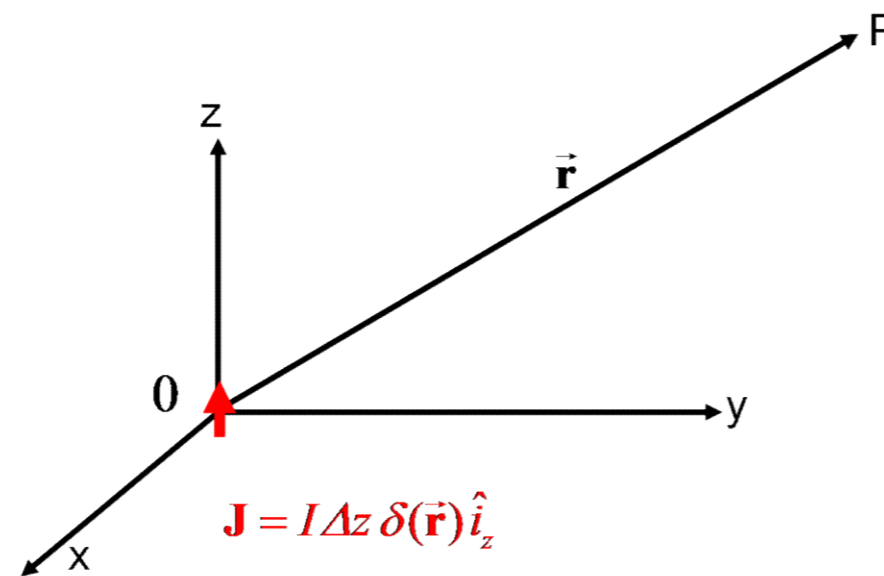
$$\mathbf{A}(\vec{\mathbf{r}}) = \frac{\mu}{4\pi} \int \mathbf{J}(\vec{\mathbf{r}}') \frac{e^{-jk|\vec{\mathbf{r}}-\vec{\mathbf{r}}'|}}{|\vec{\mathbf{r}}-\vec{\mathbf{r}}'|} d\vec{\mathbf{r}}'$$



# Elementary electrical dipole

- A  $\delta$ -source radiating element is also known as elementary electrical dipole.

$$\mathbf{J} = I \Delta z \delta(\vec{\mathbf{r}}) \hat{i}_z = I \Delta z \delta(x) \delta(y) \delta(z) \hat{i}_z$$



- Why are we interested in such a radiating element?
- Why is such a radiating element referred to as elementary electrical dipole?
- How can we physically approximate an elementary electrical dipole?

# Elementary electrical dipole

- A  $\delta$ -source radiating element is also known as elementary electrical dipole.

$$\mathbf{J} = I \Delta z \delta(\vec{\mathbf{r}}) \hat{i}_z = I \Delta z \delta(x) \delta(y) \delta(z) \hat{i}_z$$

$\mathbf{J}$   
↓

$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$

↓  
 $\mathbf{A}$

$$\begin{cases} \nabla^2 A_x + k^2 A_x = 0 & \Rightarrow A_x = 0 \\ \nabla^2 A_y + k^2 A_y = 0 & \Rightarrow A_y = 0 \\ \nabla^2 A_z + k^2 A_z = -\mu J_z = -\mu I \Delta z \delta(x) \delta(y) \delta(z) = -\mu I \Delta z \delta(\vec{\mathbf{r}}) \end{cases}$$

# Elementary electrical dipole

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$$\mathbf{J} = I \Delta z \delta(\vec{\mathbf{r}}) \hat{i}_z = I \Delta z \delta(x) \delta(y) \delta(z) \hat{i}_z$$

↓  $J$

$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$

↓

$$\mathbf{A} = \frac{\mu}{4\pi} I \Delta z \frac{e^{-jkr}}{r} \hat{i}_z$$

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} \quad \text{and} \quad \mathbf{E} = -j\omega \mathbf{A} + \frac{\nabla \nabla \cdot \mathbf{A}}{j\omega \epsilon \mu}$$

↓  $E$   
 $H$



# Elementary electrical dipole

- A  $\delta$ -source radiating element is also known as elementary electrical dipole.

$$\mathbf{J} = I \Delta z \delta(\vec{\mathbf{r}}) \hat{i}_z = I \Delta z \delta(x) \delta(y) \delta(z) \hat{i}_z$$

The E.M. field radiated by the elementary electrical dipole

$$\begin{aligned} \vec{\mathbf{E}}(\vec{\mathbf{r}}) &= E_r(r, \vartheta) \hat{i}_r + E_\vartheta(r, \vartheta) \hat{i}_\vartheta \\ \vec{\mathbf{H}}(\vec{\mathbf{r}}) &= H_\varphi(r, \vartheta) \hat{i}_\varphi \end{aligned} \quad \left\{ \begin{aligned} E_r &= \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta &= \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi &= \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{aligned} \right.$$

Because of the problem symmetry there is no dependence on the azimuth angle  $\varphi$ .

# Elementary electrical dipole: static case

The E.M. field radiated by the elementary electrical dipole

$$\begin{cases} E_r = \zeta \frac{jQ\Delta z}{2\pi} \left( \frac{\cancel{\omega}}{r^2} + \frac{\omega}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{jQ\Delta z}{4\pi} \left( \frac{j\omega\beta}{r} + \frac{\cancel{\omega}}{r^2} + \frac{\omega}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{jQ\Delta z}{4\pi} \left( \frac{j\omega\beta}{r} + \frac{\cancel{\omega}}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$j\omega Q = I$

... for  $\omega=0$  simplifies as

$$\begin{cases} E_r = \frac{\zeta}{\sqrt{\mu\varepsilon}} \frac{Q\Delta z}{2\pi} \frac{1}{r^3} \cos \vartheta = \frac{Q\Delta z}{2\pi} \frac{1}{\varepsilon r^3} \cos \vartheta \\ E_\vartheta = \frac{\zeta}{\sqrt{\mu\varepsilon}} \frac{Q\Delta z}{4\pi} \frac{1}{r^3} \sin \vartheta = \frac{Q\Delta z}{4\pi} \frac{1}{\varepsilon r^3} \sin \vartheta \\ H_\varphi = 0 \end{cases}$$

$$\zeta = \sqrt{\frac{\mu}{\varepsilon}}$$

→

$$\frac{\zeta}{\sqrt{\mu\varepsilon}} = \frac{1}{\varepsilon}$$

# Elementary electrical dipole: far field

The E.M. field radiated by the elementary electrical dipole

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

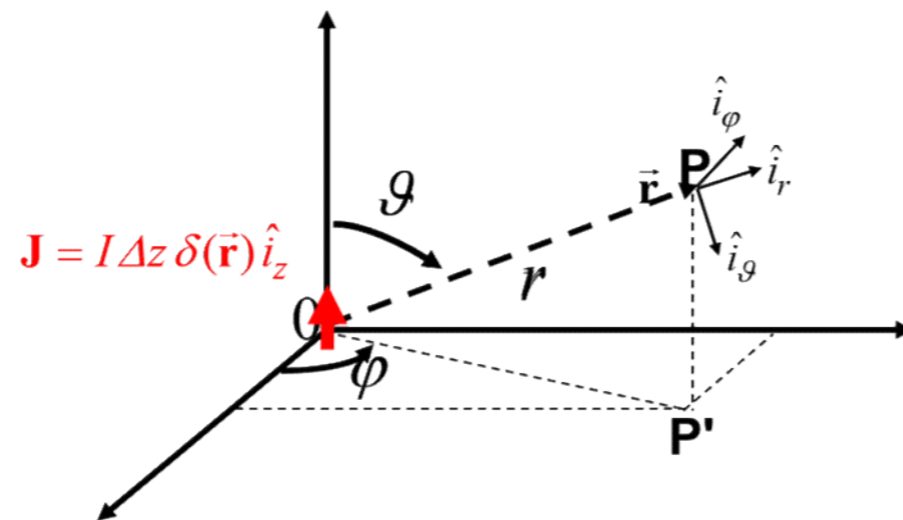
... for  $r \gg \lambda$  simplifies as

$$\begin{cases} E_r = 0 \\ E_\vartheta = j\zeta \frac{I \Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{E_\vartheta}{\zeta} \end{cases}$$

# Elementary electrical dipole: far field

In the far-field case ( $r \gg \lambda$ ) the elementary electrical dipole behaves as follows

$$\begin{aligned} \vec{\mathbf{E}}(\vec{\mathbf{r}}) &= E_{\vartheta}(r, \vartheta) \hat{i}_{\vartheta} \\ \vec{\mathbf{H}}(\vec{\mathbf{r}}) &= H_{\varphi}(r, \vartheta) \hat{i}_{\varphi} \end{aligned} \quad \left\{ \begin{aligned} E_{\vartheta} &= j\zeta \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) \\ H_{\varphi} &= \frac{E_{\vartheta}}{\zeta} \end{aligned} \right.$$



- the e.m. field propagates along  $\hat{i}_r$
- the e.m. field lies on the plane orthogonal to the propagation direction
- $|E|$  and  $|H|$  exhibit the decaying factor  $1/r$
- $|E|$  and  $|H|$  are proportional through  $\zeta$

$$\zeta \mathbf{H} = \hat{i}_r \times \mathbf{E}$$

$$\vec{\mathbf{S}} = \frac{1}{2\zeta} |\vec{\mathbf{E}}|^2 \hat{i}_r = \frac{\zeta}{2} |\vec{\mathbf{H}}|^2 \hat{i}_r$$

# Elementary electrical dipole: power flux

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

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$$P = \frac{1}{2} \oiint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS = \frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\vartheta H_\varphi^*$$

$$dS = r^2 \sin \vartheta d\vartheta d\varphi$$

$$[\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r = \left[ (E_\vartheta \hat{i}_\vartheta + E_r \hat{i}_r) \times (H_\varphi^* \hat{i}_\varphi) \right] \cdot \hat{i}_r = E_\vartheta H_\varphi^* \hat{i}_r \cdot \hat{i}_r = E_\vartheta H_\varphi^*$$

$$\hat{i}_\varphi = \hat{i}_r \times \hat{i}_\vartheta$$

$$\hat{i}_\vartheta = \hat{i}_\varphi \times \hat{i}_r$$

$$\hat{i}_r = \hat{i}_\vartheta \times \hat{i}_\varphi$$

# Elementary electrical dipole: power flux

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$\begin{aligned} P &= \frac{1}{2} \oiint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS = \frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\vartheta H_\varphi^* \\ &= \frac{1}{2} \left[ \zeta \frac{|I|^2 \Delta z^2}{(4\pi)^2} \right] \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta \left[ \sin^2 \vartheta \right] \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \left( \frac{j\beta}{r} + \frac{1}{r^2} \right)^* \end{aligned}$$

# Elementary electrical dipole: power flux

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

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$$\begin{aligned} \int_0^{2\pi} d\varphi &= 2\pi \\ \int_0^\pi d\vartheta \sin^3 \vartheta &= \frac{4}{3} \end{aligned}$$



# Elementary electrical dipole: power flux

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = \frac{1}{2} \oiint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS = \frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\vartheta H_\varphi^* = \frac{1}{2} \left[ \zeta \frac{|I|^2 \Delta z^2}{(4\pi)^2} \right] r^2 \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \left( \frac{j\beta}{r} + \frac{1}{r^2} \right)^* 2\pi \frac{4}{3}$$

$$= \frac{1}{2} \left[ \zeta \frac{|I|^2 \Delta z^2}{(4\pi)^2} \right] r^2 \frac{\beta^2}{r^2} \left[ 1 - j \frac{1}{(\beta r)^3} \right] 2\pi \frac{4}{3} = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \left[ 1 - j \frac{1}{(\beta r)^3} \right] |I|^2$$

$$\left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \left( \frac{-j\beta}{r} + \frac{1}{r^2} \right) = \left( \frac{\beta}{r} \right)^2 + \cancel{\frac{j\beta}{r^3}} - \cancel{\frac{j\beta}{r^3}} + \cancel{\frac{1}{r^4}} - \cancel{\frac{1}{r^4}} - j \frac{1}{\beta r^5} = \left( \frac{\beta}{r} \right)^2 - j \frac{1}{\beta r^5} = \frac{\beta^2}{r^2} \left[ 1 - j \frac{1}{(\beta r)^3} \right]$$

# Elementary electrical dipole: power flux

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 |I|^2$$

$$P_2 = -\frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

$$P = \frac{1}{2} \iint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS$$

$$= \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \left[ 1 - j \frac{1}{(\beta r)^3} \right] |I|^2$$

# Elementary electrical dipole: power flux

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 |I|^2$$

$$P_2 = -\frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

- Note that in the far-field case only the first active power term exists and it does not depend on  $r$
- Note that the real part of the power, in lossless medium, is independent of  $r$ , therefore if one consider two different spherical surfaces one gets the same result. Only the so-called radiative terms contribute.
- The reactive part depends on  $r$ . Its sign is negative showing that there is an excess of stored **electric** energy in the neighbor of the electrical dipole (see Poynting's theorem)

$$\int_0^{\pi} d\vartheta \sin^3 \vartheta = \frac{4}{3}$$

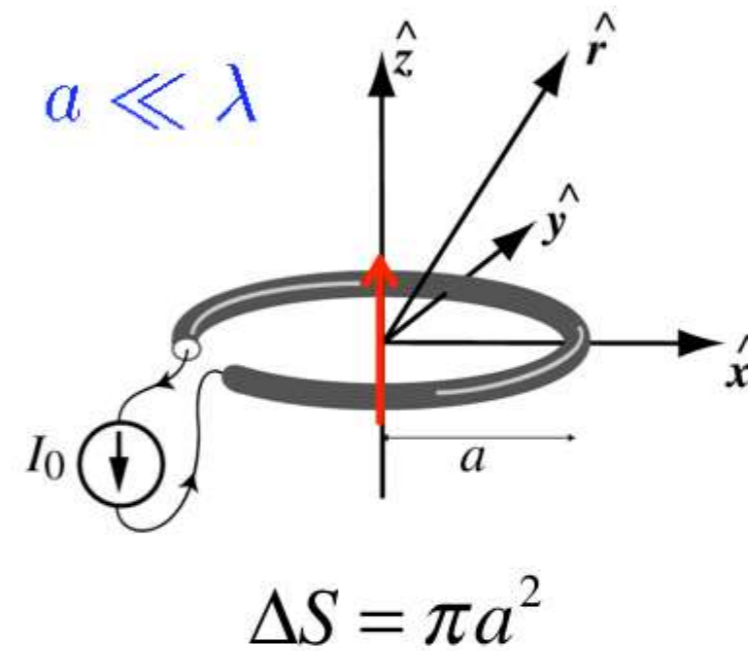
$$\int_0^{\pi} d\vartheta \sin^3 \vartheta = \int_0^{\pi} d\vartheta \sin \vartheta (1 - \cos^2 \vartheta) = \int_{-1}^1 dx (1 - x^2) = \left[ x - \frac{1}{3} x^3 \right]_{-1}^1 = \frac{4}{3}$$

$$x = \cos \vartheta$$

$$dx = -d\vartheta \sin \vartheta$$

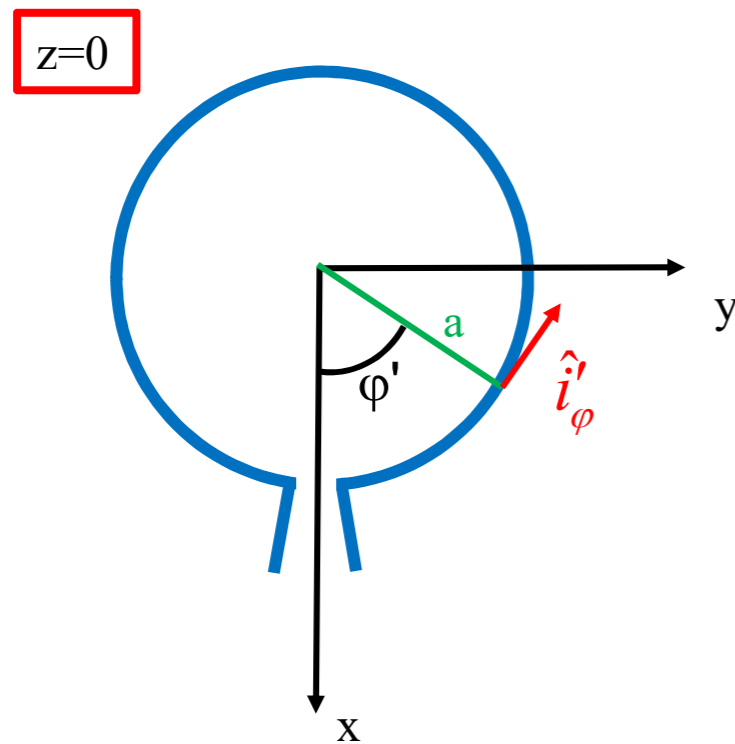
# Small loop antenna

A simple and inexpensive antenna type is the loop antenna



# Small loop antenna

$$\mathbf{J} = I\delta(z)\delta(r-a)\hat{i}'_{\varphi}$$



↓  $\mathbf{J}$

$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$

↓

$$\mathbf{A}(\mathbf{r}) = \frac{\mu}{4\pi} \int \mathbf{J}(\mathbf{r}') \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} d\mathbf{r}'$$

↓

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} \quad \text{and} \quad \mathbf{E} = -j\omega \mathbf{A} + \frac{\nabla \nabla \cdot \mathbf{A}}{j\omega \epsilon \mu}$$

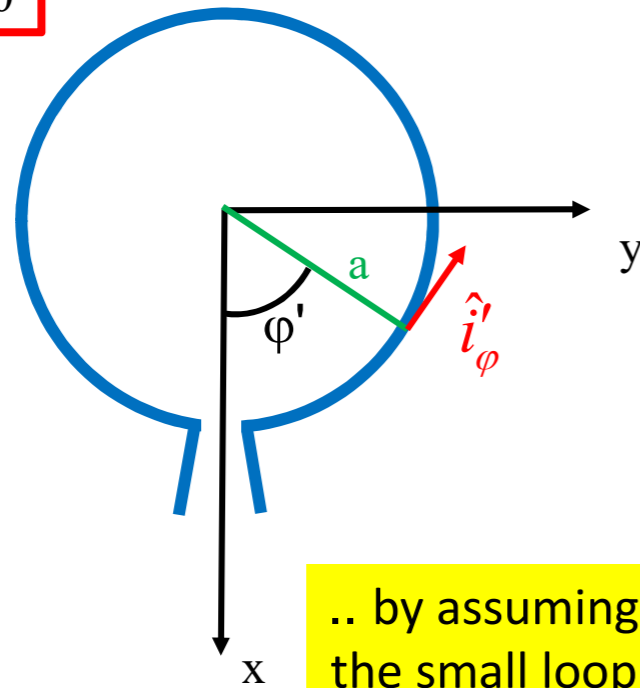
↓

$\mathbf{E}(\mathbf{r})$   
 $\mathbf{H}(\mathbf{r})$

# Small loop antenna

$$\mathbf{J} = I\delta(z)\delta(r-a)\hat{i}'_{\varphi}$$

$z=0$



.. by assuming that the current  $I$  in the small loop is constant and that the radius of the loop  $a \ll \lambda$

$\mathbf{J}$

$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$

$$\mathbf{A} \approx \frac{j\beta I \mu \Delta S}{4\pi} \frac{e^{-j\beta r}}{r} \left[ 1 + \frac{1}{j\beta r} \right] \sin \vartheta \hat{i}'_{\varphi}$$

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} \quad \text{and} \quad \mathbf{E} = -j\omega \mathbf{A} + \frac{\nabla \nabla \cdot \mathbf{A}}{j\omega \epsilon \mu}$$

$\mathbf{E}$   $\mathbf{H}$

# Small loop antenna

The E.M. field radiated by the the small loop antenna

$$\begin{aligned}\vec{\mathbf{H}}(\vec{\mathbf{r}}) &= H_r(r, \vartheta) \hat{i}_r + H_\vartheta(r, \vartheta) \hat{i}_\vartheta \\ \vec{\mathbf{E}}(\vec{\mathbf{r}}) &= E_\varphi(r, \vartheta) \hat{i}_\varphi\end{aligned}\quad \left\{ \begin{aligned}H_r &= \frac{I \Delta S (j\beta)^2}{2\pi r} \left( \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \cos \vartheta \exp(-j\beta r) \\ H_\vartheta &= \frac{I \Delta S (j\beta)^2}{4\pi r} \left( 1 + \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \sin \vartheta \exp(-j\beta r) \\ E_\varphi &= -\frac{\zeta I \Delta S (j\beta)^2}{4\pi r} \left( 1 + \frac{1}{j\beta r} \right) \sin \vartheta \exp(-j\beta r)\end{aligned}\right.$$

Because of the problem symmetry there is no dependence on the azimuth angle  $\varphi$ .



# Small loop antenna: far field

The E.M. field radiated by the the small loop antenna

$$\begin{aligned} \vec{\mathbf{H}}(\vec{\mathbf{r}}) &= H_r(r, \vartheta) \hat{i}_r + H_\vartheta(r, \vartheta) \hat{i}_\vartheta \\ \vec{\mathbf{E}}(\vec{\mathbf{r}}) &= E_\varphi(r, \vartheta) \hat{i}_\varphi \end{aligned} \quad \left\{ \begin{aligned} H_r &= \frac{I \Delta S (j\beta)^2}{2\pi r} \left( \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \cos \vartheta \exp(-j\beta r) \\ H_\vartheta &= \frac{I \Delta S (j\beta)^2}{4\pi r} \left( 1 + \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \sin \vartheta \exp(-j\beta r) \\ E_\varphi &= -\frac{\zeta I \Delta S (j\beta)^2}{4\pi r} \left( 1 + \frac{1}{j\beta r} \right) \sin \vartheta \exp(-j\beta r) \end{aligned} \right.$$

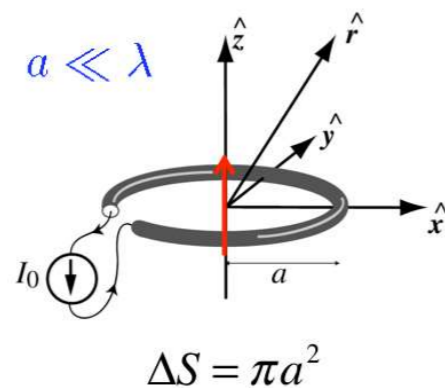
... for  $r \gg \lambda$  ( $\beta r \gg 1$ ) simplifies as

$$\left\{ \begin{aligned} H_r &= 0 \\ H_\vartheta &= -\frac{\beta \Delta S I}{2\lambda r} \sin \vartheta \exp(-j\beta r) = \frac{-E_\varphi}{\zeta} \\ E_\varphi &= \frac{\zeta \beta \Delta S I}{2\lambda r} \sin \vartheta \exp(-j\beta r) \end{aligned} \right.$$

# Small loop antenna: far field

In the far-field case ( $r \gg \lambda$ ) the small loop antenna behaves as follows

$$\begin{aligned} \vec{\mathbf{E}}(\vec{\mathbf{r}}) &= E_{\varphi}(r, \vartheta) \hat{i}_{\varphi} \\ \vec{\mathbf{H}}(\vec{\mathbf{r}}) &= H_{\vartheta}(r, \vartheta) \hat{i}_{\vartheta} \end{aligned} \quad \left\{ \begin{aligned} E_{\varphi} &= \frac{\zeta \beta \Delta s I}{2\lambda r} \sin \vartheta \exp(-j\beta r) \\ H_{\vartheta} &= -\frac{\beta \Delta s I}{2\lambda r} \sin \vartheta \exp(-j\beta r) = \frac{-E_{\varphi}}{\zeta} \end{aligned} \right.$$



- the e.m. field propagates along  $\hat{i}_r$
- the e.m. field lies on the plane orthogonal to the propagation direction
- $|E|$  and  $|H|$  exhibit the decaying factor  $1/r$
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$$\zeta \vec{\mathbf{H}} = \zeta H_\vartheta \hat{i}_\vartheta = -E_\varphi \hat{i}_\vartheta$$

$$\hat{i}_r \times \vec{\mathbf{E}} = \hat{i}_r \times E_\varphi \hat{i}_\varphi = -E_\varphi \hat{i}_\vartheta$$



$$\zeta \mathbf{H} = \hat{i}_r \times \mathbf{E}$$

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$$\vec{\mathbf{S}} = \frac{1}{2 \zeta} |\vec{\mathbf{E}}|^2 \hat{i}_r = \frac{\zeta}{2} |\vec{\mathbf{H}}|^2 \hat{i}_r$$

# Small loop antenna: power flux

$$\begin{cases} H_r = \frac{I\Delta S (j\beta)^2}{2\pi r} \left( \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \cos \vartheta \exp(-j\beta r) \\ H_\vartheta = \frac{I\Delta S (j\beta)^2}{4\pi r} \left( 1 + \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \sin \vartheta \exp(-j\beta r) \\ E_\varphi = -\frac{\zeta I\Delta S (j\beta)^2}{4\pi r} \left( 1 + \frac{1}{j\beta r} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = \frac{1}{2} \oiint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS = -\frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\varphi H_\vartheta^*$$

$$dS = r^2 \sin \vartheta d\vartheta d\varphi$$

$$[\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r = \left[ (E_\varphi \hat{i}_\varphi) \times (H_\vartheta \hat{i}_\vartheta + H_r \hat{i}_r)^* \right] \cdot \hat{i}_r = -E_\varphi H_\vartheta^* \hat{i}_r \cdot \hat{i}_r = -E_\varphi H_\vartheta^*$$

$$\begin{aligned} \hat{i}_\varphi &= \hat{i}_r \times \hat{i}_\vartheta \\ \hat{i}_\vartheta &= \hat{i}_\varphi \times \hat{i}_r \\ \hat{i}_r &= \hat{i}_\vartheta \times \hat{i}_\varphi \end{aligned}$$

## Small loop antenna: power flux

$$\begin{cases} H_r = \frac{I\Delta S}{2\pi} \frac{(j\beta)^2}{r} \left( \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \cos \vartheta \exp(-j\beta r) \\ H_\vartheta = \frac{I\Delta S}{4\pi} \frac{(j\beta)^2}{r} \left( 1 + \frac{1}{j\beta r} + \frac{1}{[j\beta r]^2} \right) \sin \vartheta \exp(-j\beta r) \\ E_\varphi = -\frac{\zeta I\Delta S}{4\pi} \frac{(j\beta)^2}{r} \left( 1 + \frac{1}{j\beta r} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta\Delta S}{\lambda} \right)^2 |I|^2$$

$$P_2 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta\Delta S}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

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# Small loop antenna: power flux

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- Note that in the far-field case only the first active power term exists and it does not depend on  $r$
- Note that the real part of the power, in lossless medium, is independent of  $r$ , therefore if one consider two different spherical surfaces one gets the same result. Only the so-called radiative terms contribute.
- The reactive part depends on  $r$ . The reactive part depends on  $r$ . Its sign is positive showing that there is an excess of stored **magnetic** energy in the neighbor of the magnetic dipole (see Poynting's theorem)

# Elementary electrical dipole vs. small loop antenna

## Elementary electrical dipole

$$P = P_1 + jP_2$$
$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 |I|^2$$
$$P_2 = -\frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

## Small loop antenna

$$P = P_1 + jP_2$$
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# Small loop antenna

WHY?

