

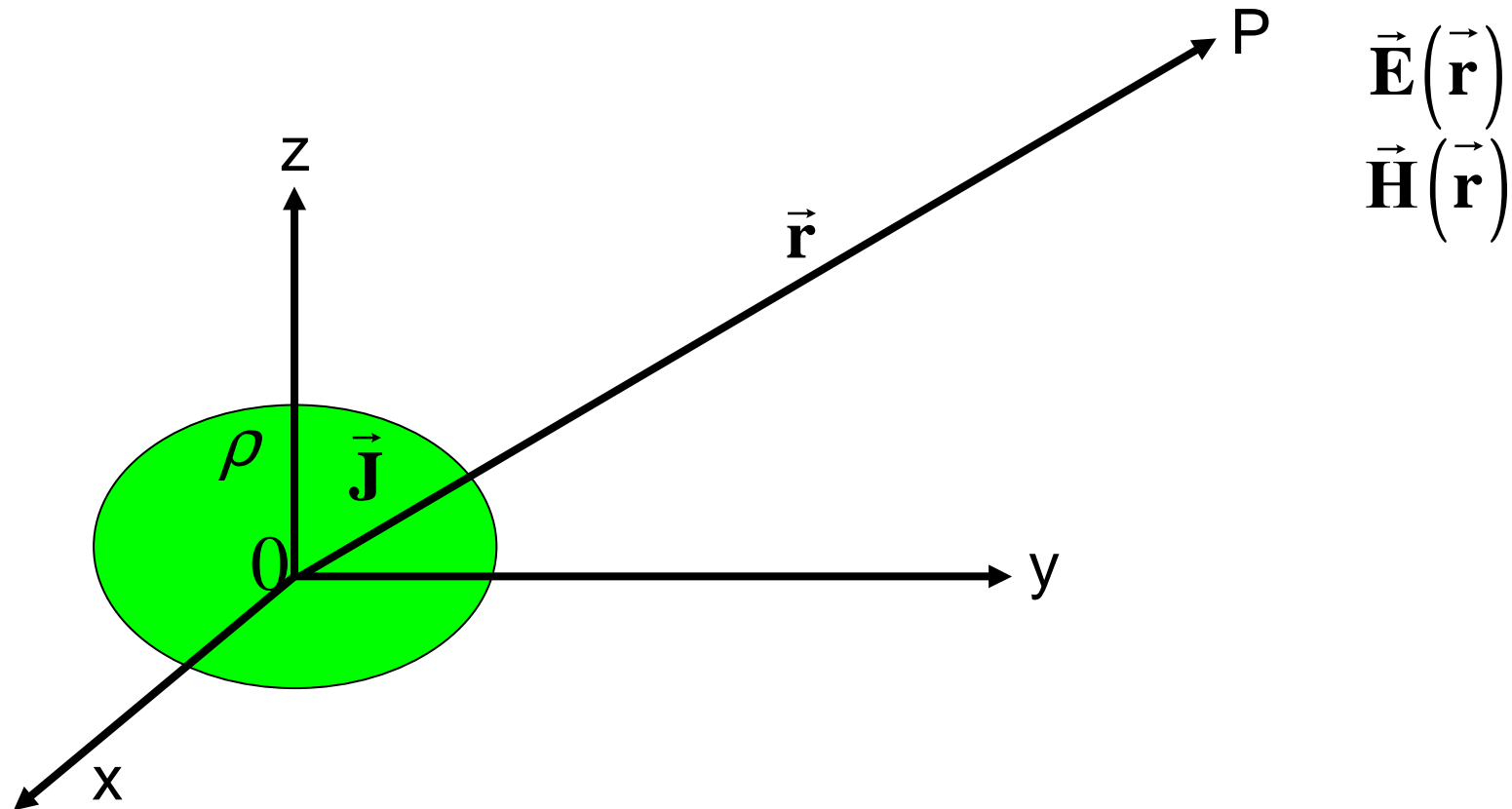
# Corso di Laurea in Ingegneria Informatica, Biomedica e delle Telecomunicazioni

Corso di Campi Elettromagnetici  
a.a. 2017-2018

11 Maggio 2018

# Summary of the past lecture

## Radiation problem

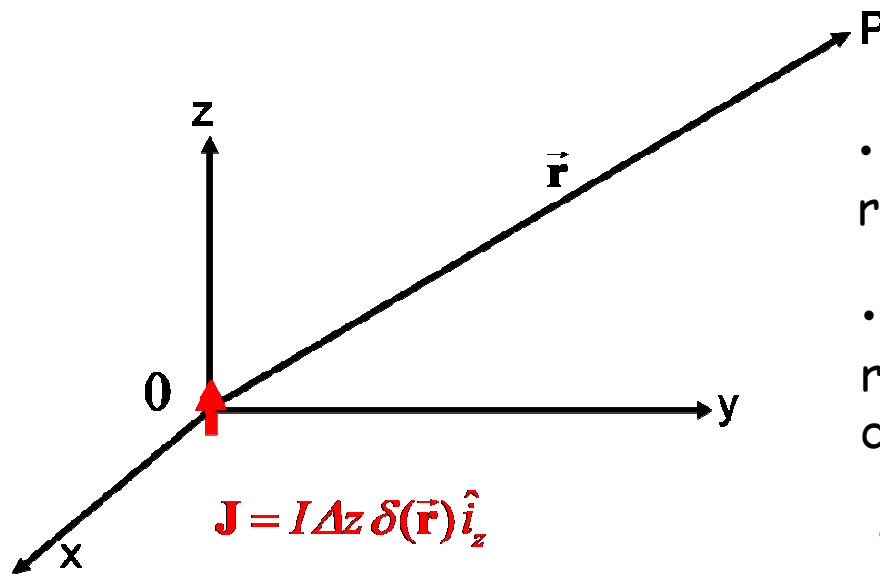


# Summary of the past lecture

## Elementary electrical dipole

- A  $\delta$ -source radiating element is also known as elementary electrical dipole.

$$\mathbf{J} = I \Delta z \delta(\vec{\mathbf{r}}) \hat{i}_z = I \Delta z \delta(x) \delta(y) \delta(z) \hat{i}_z$$



- Why are we interested in such a radiating element?
- Why is such a radiating element referred to as elementary electrical dipole?
- How can we physically approximate an elementary electrical dipole?

# Summary of the past lecture

## Elementary electrical dipole

The E.M. field radiated by the elementary electrical dipole

$$\left\{ \begin{array}{l} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{array} \right.$$

... for  $\omega=0$  simplifies as

$$\left\{ \begin{array}{l} E_r = \frac{Q \Delta z}{2\pi} \frac{1}{\epsilon r^3} \cos \vartheta \\ E_\vartheta = \frac{Q \Delta z}{4\pi} \frac{1}{\epsilon r^3} \sin \vartheta \\ H_\varphi = 0 \end{array} \right.$$

# Summary of the past lecture

## Elementary electrical dipole

...the E.M. field radiated by the elementary electrical dipole..

$$\left\{ \begin{array}{l} E_r = \zeta \frac{I\Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I\Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I\Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{array} \right.$$

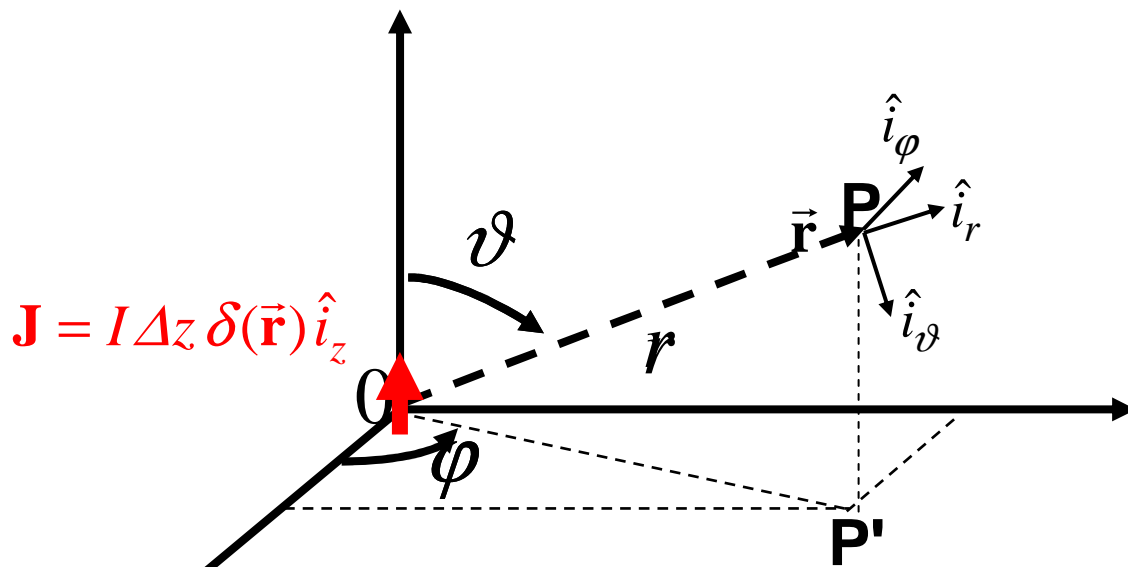
... for  $r \gg \lambda$  simplifies as

$$\left\{ \begin{array}{l} E_r = 0 \\ E_\vartheta = j\zeta \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) \\ H_\varphi = j \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) = \frac{E_\vartheta}{\zeta} \end{array} \right.$$

# Elementary electrical dipole

for  $r \gg \lambda$

$$\begin{aligned} \vec{\mathbf{E}} = \vec{\mathbf{E}}(\vec{\mathbf{r}}) &= E_{\vartheta}(r, \vartheta) \hat{i}_{\vartheta} \\ \vec{\mathbf{H}} = \vec{\mathbf{H}}(\vec{\mathbf{r}}) &= H_{\varphi}(r, \vartheta) \hat{i}_{\varphi} \end{aligned} \quad \left\{ \begin{aligned} E_{\vartheta} &= j\zeta \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) \\ H_{\varphi} &= j \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) = \frac{E_{\vartheta}}{\zeta} \end{aligned} \right.$$



- the e.m. field propagates along  $\hat{i}_r$
- the e.m. field lies on the plane orthogonal to the propagation direction

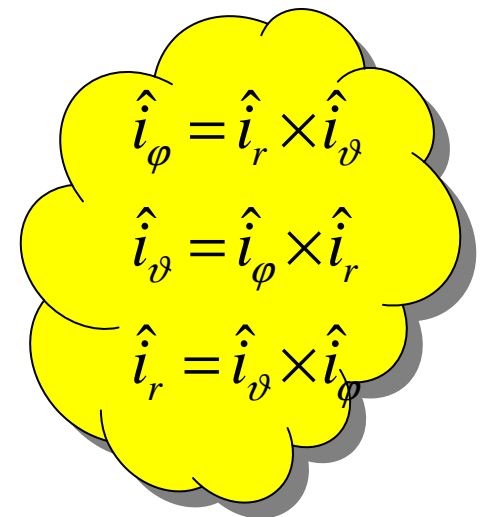
# Elementary electrical dipole

In the far-field region, we have

$$\left\{ \begin{array}{l} E_r = 0 \\ E_{\vartheta} = j\zeta \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) \\ H_{\varphi} = j \frac{I\Delta z}{2\lambda r} \sin \vartheta \exp(-j\beta r) = \frac{E_{\vartheta}}{\zeta} \end{array} \right. \quad \longrightarrow \quad \zeta \mathbf{H} = \hat{i}_r \times \mathbf{E}$$

and the Poynting vector:

$$\mathbf{S} = \frac{1}{2} \mathbf{E} \times \mathbf{H}^* = \frac{1}{2} \frac{|E_{\vartheta}|^2}{\zeta} \hat{i}_r = \frac{1}{2} \frac{|\mathbf{E}|^2}{\zeta} \hat{i}_r$$





# Elementary electrical dipole

- In order to further characterize its behavior one can evaluate the Poynting vector and the associated power for the overall e.m. field (over a sphere centered in the origin):

$$P = \frac{1}{2} \oiint_S \left[ \mathbf{E} \times \mathbf{H}^* \right] \cdot \hat{i}_r dS = \frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\vartheta H_\varphi^*$$

$$\begin{aligned} \text{I)} \quad dS &= r^2 \sin \vartheta d\vartheta d\varphi \\ \text{II)} \quad \left[ \mathbf{E} \times \mathbf{H}^* \right] \cdot \hat{i}_r &= \left[ \begin{array}{l} E_\vartheta \hat{i}_\vartheta \\ H_\varphi \hat{i}_\varphi \end{array} \right] \times \left[ \begin{array}{l} E_r \hat{i}_r \\ H_\varphi \hat{i}_\varphi \end{array} \right] \cdot \hat{i}_r = E_\vartheta H_\varphi^* \end{aligned}$$

$$P = \frac{1}{2} \iint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS = \frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\vartheta H_\varphi^* = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \left[ 1 - j \frac{1}{(\beta r)^3} \right] |I|^2$$

$$\begin{cases} E_r = \zeta \frac{I \Delta z}{2\pi} \left( \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \cos \vartheta \exp(-j\beta r) \\ E_\vartheta = \zeta \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \sin \vartheta \exp(-j\beta r) \\ H_\varphi = \frac{I \Delta z}{4\pi} \left( \frac{j\beta}{r} + \frac{1}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 |I|^2$$

$$P_2 = -\frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

$$\left( \frac{j\beta}{r} + \frac{1}{r^2} + \frac{1}{j\beta r^3} \right) \left( \frac{-j\beta}{r} + \frac{1}{r^2} \right) = \left( \frac{\beta}{r} \right)^2 - j \frac{1}{\beta r^5}$$

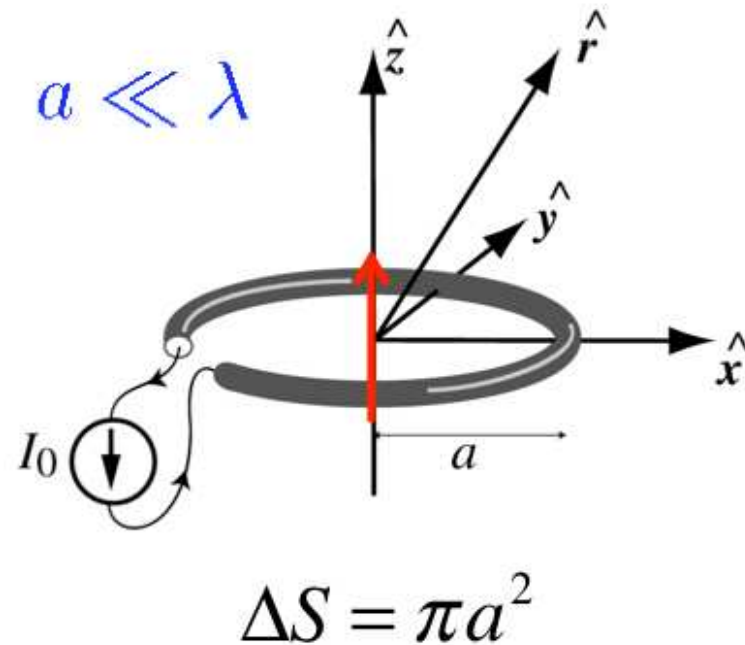
- Note that in the far-field case only the first active power term exists and it does not depend on  $r$ .

# Elementary electrical dipole

- Note that the real part of the power, in lossless medium, is independent of  $r$ , therefore if one consider two different spherical surfaces one gets the same result. Only the so-called radiative terms contribute.
- The reactive part depends on  $r$ . Its sign is negative showing that there is an excess of stored **electric** energy in the neighbor of the electrical dipole (see Poynting's theorem)

# Small loop antenna

- A simple and inexpensive antenna type is the loop antenna.





## Small loop antenna

Electrically small antennas are those whose overall length (circumference) is usually less than about one-tenth of a wavelength ( $C < \lambda/10$ ).

# Small loop antenna

$$\mathbf{J} = I \delta(z) \delta(r - a) \hat{i}'_{\phi}$$



$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$



$$\mathbf{A}(\mathbf{r}) = \frac{\mu}{4\pi} \int \mathbf{J}(\mathbf{r}') \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|}}{|\mathbf{r}-\mathbf{r}'|} d\mathbf{r}'$$

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} \quad \text{and} \quad \mathbf{E} = -j\omega \mathbf{A} + \frac{\nabla \nabla \cdot \mathbf{A}}{j\omega \epsilon \mu}$$



$$\mathbf{E}(\mathbf{r})$$
$$\mathbf{H}(\mathbf{r})$$

# Small loop antenna

$$\mathbf{J} = I \delta(z) \delta(r - a) \hat{i}'_{\phi}$$

$$\mathbf{A}(\vec{\mathbf{r}}) = \frac{\mu}{4\pi} \int \mathbf{J}(\vec{\mathbf{r}}') \frac{e^{-j\beta|\vec{\mathbf{r}}-\vec{\mathbf{r}}'|}}{|\vec{\mathbf{r}}-\vec{\mathbf{r}}'|} d\vec{\mathbf{r}}' = \frac{\mu}{4\pi} \int_0^{2\pi} d\phi' I \frac{e^{-j\beta|\vec{\mathbf{r}}-\vec{\mathbf{r}}'|}}{|\vec{\mathbf{r}}-\vec{\mathbf{r}}'|} a \hat{i}'_{\phi}$$

$$\approx \frac{j\beta I \mu \Delta S}{4\pi} \frac{e^{-j\beta r}}{r} \left[ 1 + \frac{1}{j\beta r} \right] \sin \vartheta \hat{i}_{\phi}$$

.. by assuming that the current  $I$  in the small loop is constant and that the radius of the loop  $a \ll \lambda$

# Small loop antenna

$$\mathbf{J} = I \delta(z) \delta(r - a) \hat{i}_\phi$$

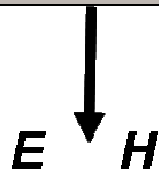


$$\nabla^2 \mathbf{A} + k^2 \mathbf{A} = -\mu \mathbf{J} \quad \text{Vector Helmholtz equation}$$



$$\mathbf{A} \approx \frac{j\beta I \mu \Delta S}{4\pi} \frac{e^{-j\beta r}}{r} \left[ 1 + \frac{1}{j\beta r} \right] \sin \theta \hat{i}_\phi$$

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} \quad \text{and} \quad \mathbf{E} = -j\omega \mathbf{A} + \frac{\nabla \nabla \cdot \mathbf{A}}{j\omega \epsilon \mu}$$



$\mathbf{E}$   $\mathbf{H}$



# Small loop antenna

The E.M. field radiated by the small loop antenna

$$\left\{ \begin{array}{l} H_r = \frac{I\Delta S}{2\pi} \left( \frac{j\beta}{r^2} + \frac{1}{r^3} \right) \cos \vartheta \exp(-j\beta r) \\ H_\vartheta = \frac{I\Delta S}{4\pi} \left( \frac{(j\beta)^2}{r} + \frac{j\beta}{r^2} + \frac{1}{r^3} \right) \sin \vartheta \exp(-j\beta r) \\ E_\varphi = -\frac{\zeta I\Delta S}{4\pi} \left( \frac{(j\beta)^2}{r} + \frac{j\beta}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{array} \right.$$

... for  $r \gg \lambda$  simplifies as

$$\left\{ \begin{array}{l} H_r = 0 \\ H_\vartheta = \frac{-E_\varphi}{\zeta} \\ E_\varphi = \frac{\zeta \beta \Delta s I}{2\lambda r} \sin \vartheta \exp(-j\beta r) \end{array} \right.$$

# Small loop antenna

In the far-field region, we have

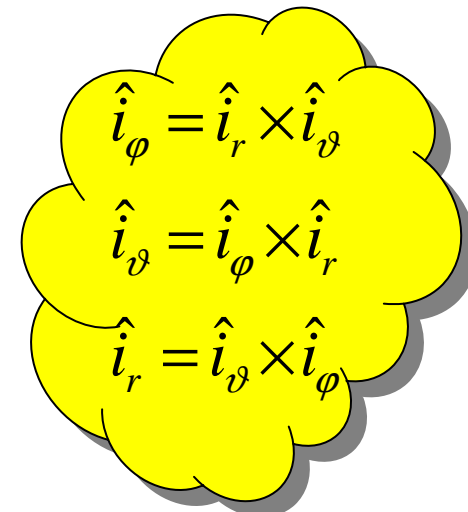
$$\left\{ \begin{array}{l} H_r = 0 \\ H_\vartheta = \frac{-E_\varphi}{\zeta} \\ E_\varphi = \frac{\zeta \beta \Delta s I}{2\lambda r} \sin \vartheta \exp(-j\beta r) \end{array} \right.$$



$$\zeta \mathbf{H} = \hat{i}_r \times \mathbf{E}$$

and the Poynting vector is:

$$\mathbf{S} = \frac{1}{2} \mathbf{E} \times \mathbf{H}^* = \frac{1}{2} \frac{|E_\varphi|^2}{\zeta} \hat{i}_r = \frac{1}{2} \frac{|\mathbf{E}|^2}{\zeta} \hat{i}_r$$



# Small loop antenna

- Similarly to the elementary electrical dipole, to further characterize the small loop antenna behavior one can evaluate the Poynting vector and the associated power over a sphere centered in the origin:

$$P = \frac{1}{2} \oiint_S \left[ \mathbf{E} \times \mathbf{H}^* \right] \cdot \hat{i}_r dS = -\frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\varphi H_\vartheta^*$$

$$\begin{aligned} \hat{i}_\varphi &= \hat{i}_r \times \hat{i}_\vartheta \\ \hat{i}_\vartheta &= \hat{i}_\varphi \times \hat{i}_r \\ \hat{i}_r &= \hat{i}_\vartheta \times \hat{i}_\varphi \end{aligned}$$

$$\text{I) } dS = r^2 \sin \vartheta d\vartheta d\varphi$$

$$\text{II) } \left[ \mathbf{E} \times \mathbf{H}^* \right] \cdot \hat{i}_r = \left[ \left( E_\varphi \hat{i}_\varphi \right) \times \left( H_\vartheta^* \hat{i}_\vartheta + H_r^* \hat{i}_r \right) \right] \cdot \hat{i}_r = -E_\varphi H_\vartheta^*$$

# Small loop antenna

$$P = \frac{1}{2} \oiint_S [\mathbf{E} \times \mathbf{H}^*] \cdot \hat{i}_r dS = -\frac{1}{2} \int_0^{2\pi} d\varphi \int_0^\pi d\vartheta r^2 \sin \vartheta E_\varphi H_\vartheta^* = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 \left[ 1 + j \frac{1}{(\beta r)^3} \right] |I|^2$$

$$\begin{cases} H_r = \frac{I \Delta S}{2\pi} \left( \frac{j\beta}{r^2} + \frac{1}{r^3} \right) \cos \vartheta \exp(-j\beta r) \\ H_\vartheta = \frac{I \Delta S}{4\pi} \left( \frac{(j\beta)^2}{r} + \frac{j\beta}{r^2} + \frac{1}{r^3} \right) \sin \vartheta \exp(-j\beta r) \\ E_\varphi = -\frac{\zeta I \Delta S}{4\pi} \left( \frac{(j\beta)^2}{r} + \frac{j\beta}{r^2} \right) \sin \vartheta \exp(-j\beta r) \end{cases}$$

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 |I|^2$$

$$P_2 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

# Elementary electrical dipole vs. Small loop antenna

## Elementary electrical dipole

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 |I|^2$$

$$P_2 = -\frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\Delta z}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

## Small loop antenna

$$P = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 |I|^2$$

$$P_2 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

# Small loop antenna

The reactive part depends on  $r$ . Its sign is positive showing that there is an excess of stored **magnetic** energy in the neighbor of the magnetic dipole (see Poynting's theorem)

$$P_r = P_1 + jP_2$$

$$P_1 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 |I|^2$$

$$P_2 = \frac{1}{2} \frac{2\pi}{3} \zeta \left( \frac{\beta \Delta S}{\lambda} \right)^2 \frac{1}{(\beta r)^3} |I|^2$$

# Small loop antenna

WHY?

