



Course of
"Industrial Control System Security"
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Harmonic response function

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Transient and Steady-state

- ✧ Let us consider an *asymptotically stable LTI system*.
- ✧ Given an input signal $u(t)$ and an initial condition $x(0)$, we define
 - ✧ *steady-state response* $y_{ss}(t)$, the regular behavior of the total response $y(t)$ (if exist) after an infinite time from the application of the input.
 - ✧ *transient response* $y_t(t)$, the difference between the total response of the system and the steady-state response $y_t(t) = y(t) - y_{ss}(t)$.



Transient and Steady-state

- ✦ *The steady-state response* of asymptotically stable system is independent from the initial condition.
- ✦ It depends on the particular input applied to the system

polynomial inputs



polynomial steady state

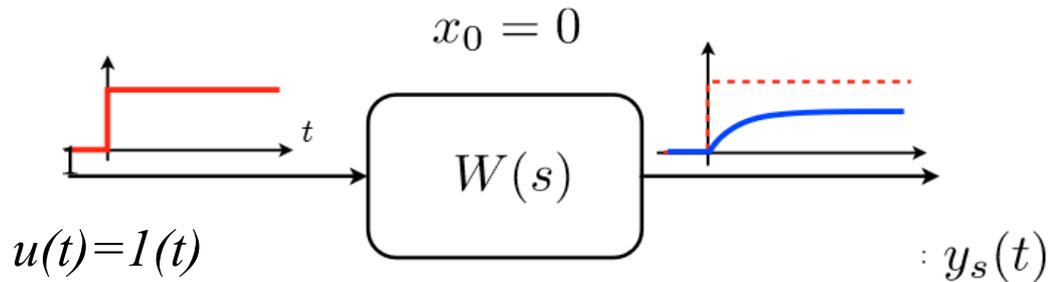
sinusoidal inputs



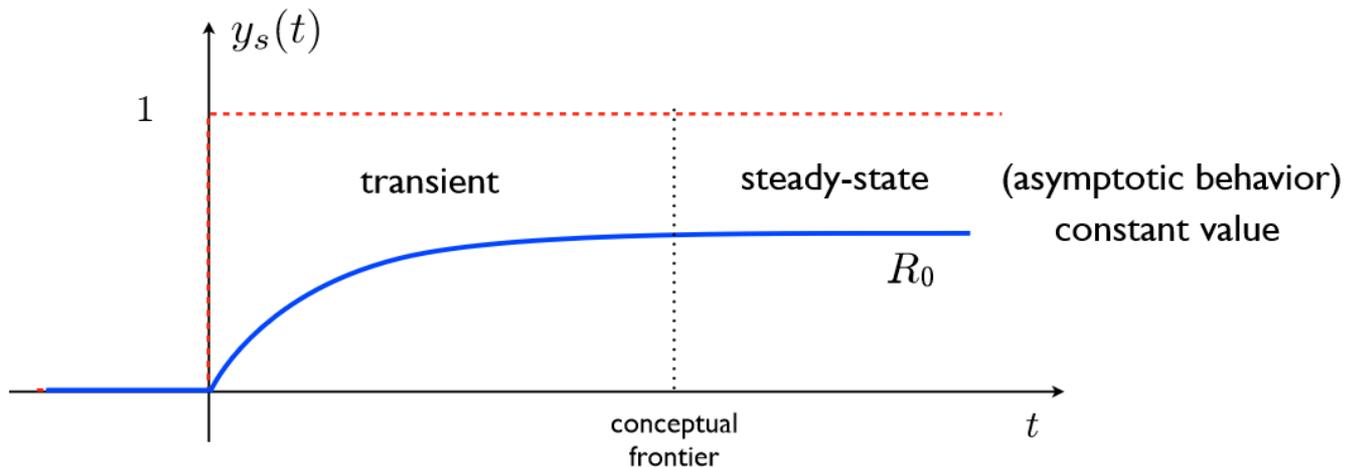
sinusoidal steady state

Step response: Transient and Steady-state

- ✦ The step response is characterized by "decaying" exponential functions related to the system evolution modes and a constant value

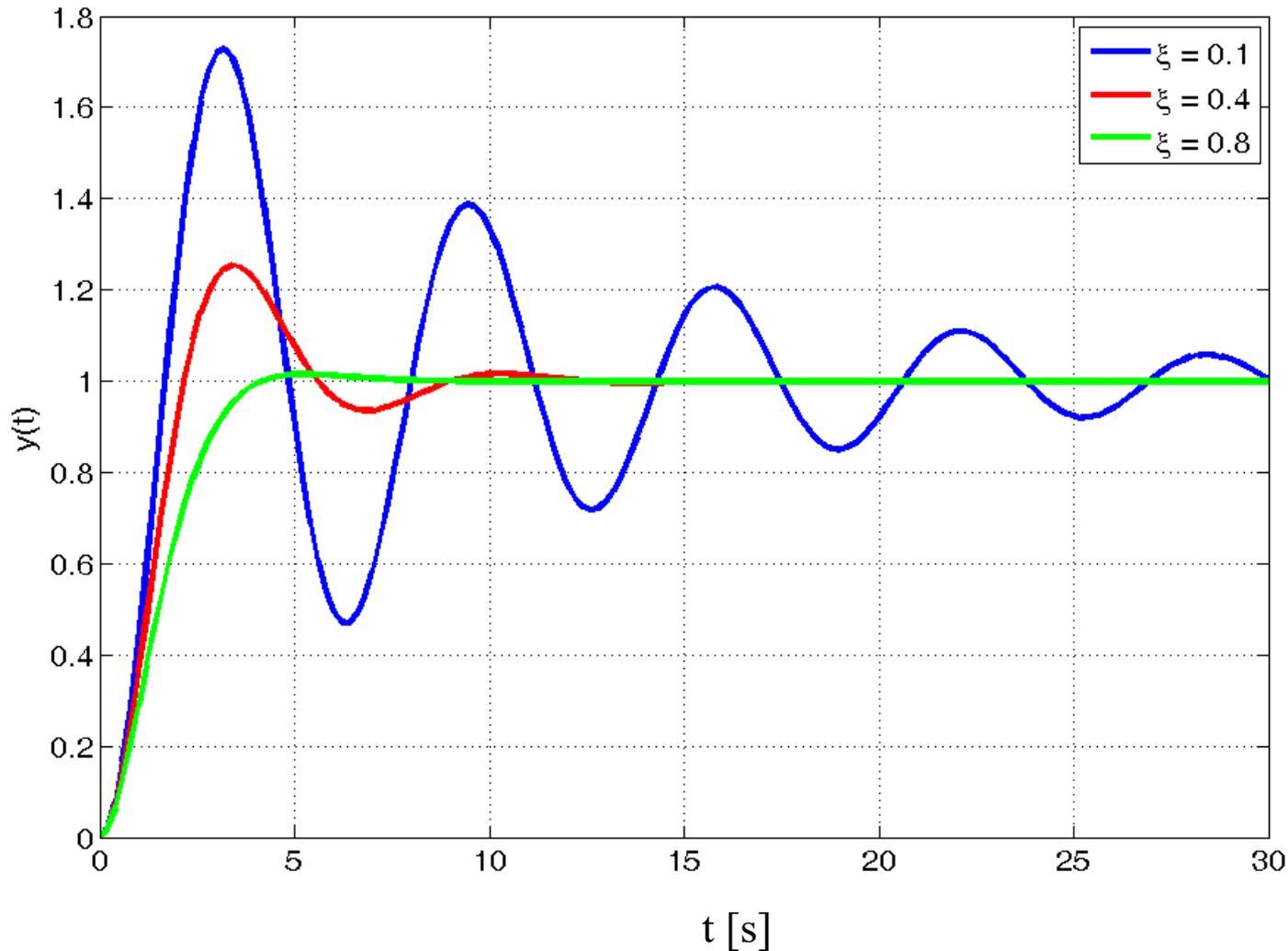


- ✦ The "decaying" exponential functions determine *the transient* part of the response while the constant term is the *steady-state* value.



Step response: Transient and Steady-state

✦ Different evolution modes determine different transient responses.





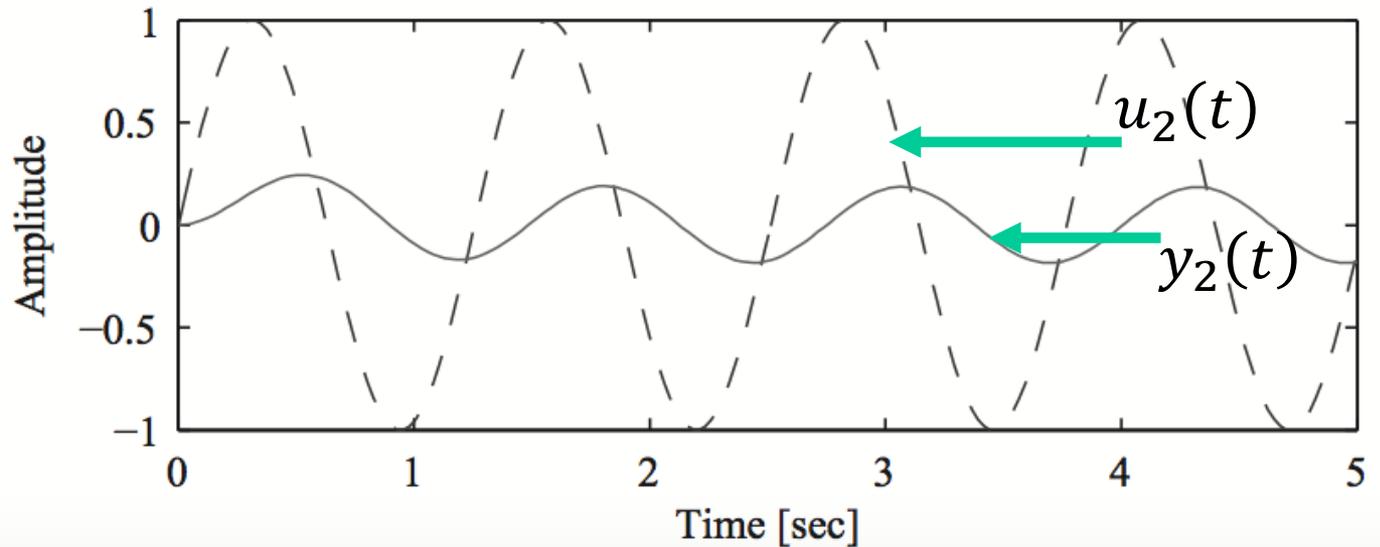
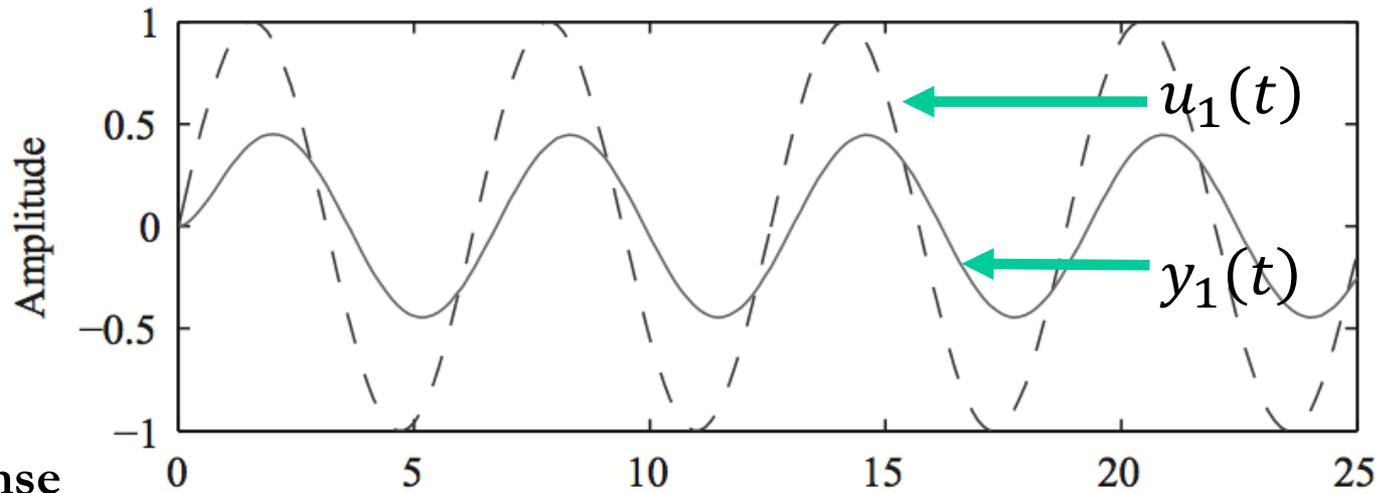
Response at sinusoidal inputs of LTI systems

Let assume a first order LTI system:

$$\dot{y}(t) + 2y(t) = u(t)$$

Compute the response to the following signals:

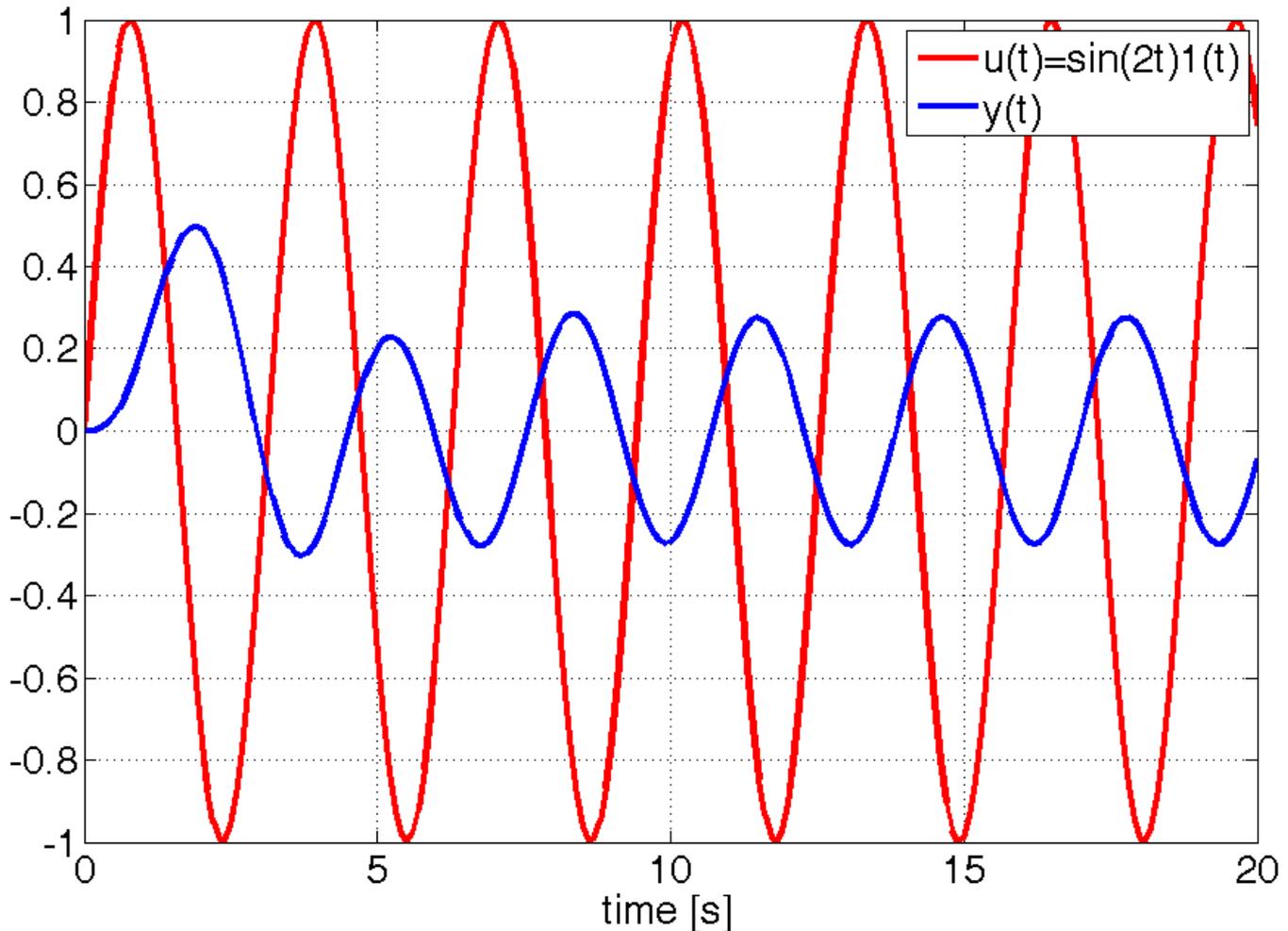
- $u_1(t) = \sin t$
- $u_2(t) = \sin(5t)$





Response to sinusoidal inputs of LTI systems

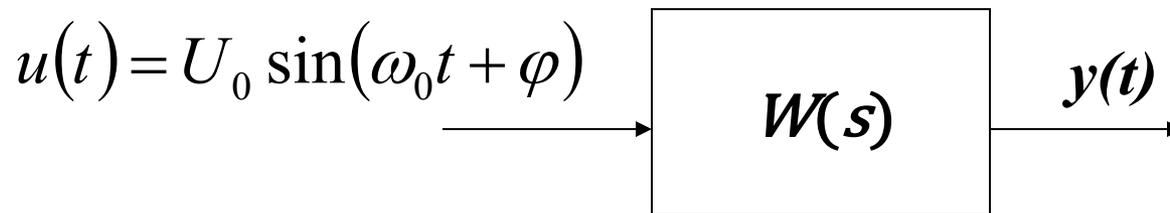
Total response of system $W(s) = 1/(s^2 + s + 1)$ to the input $u(t) = \sin(2t) \cdot 1(t)$.





Steady state response at sinusoidal inputs

- Let us consider an asymptotically stable LTI system with a transfer function $W(s)$ subject to a sinusoidal input signal



- The evaluation of the steady state response of LTI system to sinusoidal inputs is very interest taking into account that *any periodic signal, $f(t) = f(t + T)$, with period T ($\omega_0 = \frac{2\pi}{T}$), can be decomposed in the sum of a finite or infinite sinusoids by means of the Fourier series, as*

$$f(t) = F_0 + \sum_{n=1}^{\infty} [F_{cn} \cos(n\omega_0 t) + F_{sn} \sin(n\omega_0 t)]$$

- In this case, the frequency spectrum (i.e., the coefficients of the Fourier series) of the signal is discrete (i.e., it is defined only a certain frequencies)
- An aperiodic signal* can be analysed in the frequency domain by applying the Fourier transform, defined as $\mathcal{F}(\omega) = \int_{-\infty}^{+\infty} f(t)e^{-j\omega t} dt$. The spectrum becomes a continuous function of ω (i.e. defined for all the frequency values).



Steady state response at sinusoidal inputs

- ✦ It is possible to prove that the steady state response of an LTI system with transfer function $W(s)$ to a sinusoidal inputs $u(t) = U_0 \sin(\omega_0 t + \phi)$ can be written in the time domain as

$$y_{ss}(t) = U_0 |W(s)|_{s=j\omega_0} \sin(\omega_0 t + \phi + \angle W(s)_{s=j\omega_0})$$

where

- ✦ $|W(s)|_{s=j\omega_0}$ is the magnitude of the Laplace transform of $W(s)$ evaluated in $s = j\omega_0$.
- ✦ $\angle W(s)|_{s=j\omega_0}$ is the phase of the Laplace transform of $W(s)$ evaluated in $s = j\omega_0$.



Filters

- ✧ The proposed result can be summarized as follows:
 - ✧ The magnitude of a sinusoidal input signal $u(t) = \sin(\omega_0 t + \phi)$ is *amplified or reduced* by a linear system depending on the value of $|W(s)|_{s=j\omega_0}$.
 - ✧ An input signal $u(t) = \sin(\omega_0 t + \phi)$ is *phase shifted* by a linear system depending on the value of $\angle W(s)|_{s=j\omega_0}$.
- ✧ In other terms, *a linear system can be designed as a filter* able to amplify without distortion a certain set of input signals Ω_1 and reduce or eliminate another signals.
- ✧ Possible structures of filters will be discussed in the following lessons.



Harmonic response function

- ✦ This result underlines the importance of the function $W(j\omega)$ for the analysis of the forced response of LTI systems.
- ✦ The function $W(j\omega)$ is called *harmonic response function* of the system.
- ✦ In the following we present a method able to rapidly evaluate the magnitude and the phase $W(j\omega)$ as a function of ω .



Bode diagrams

- ✦ *Bode diagrams* allows to extract the magnitude and the phase of $W(j\omega)$ as a function of ω
- ✦ Bode diagrams are a main tool for the closed loop control design



$W(j\omega)$ general form

- ✦ Given an asymptotically stable LTI system, the *harmonic response function* $W(j\omega)$ is given by the ratio of polynomial with real and complex conjugate roots

$$W(j\omega) = W(s) \Big|_{s=j\omega} = K \frac{s^{\nu} \prod_i (1 + \sigma_i s)^{m_i} \prod_q \left(1 + \frac{2\xi_q}{\omega_{nq}} s + \frac{s^2}{\omega_{nq}^2} \right)^{\eta_q}}{\prod_j (1 + \tau_j s)^{n_j} \prod_p \left(1 + \frac{2\zeta_p}{\omega_{np}} s + \frac{s^2}{\omega_{np}^2} \right)^{\kappa_p}} \Big|_{s=j\omega}$$



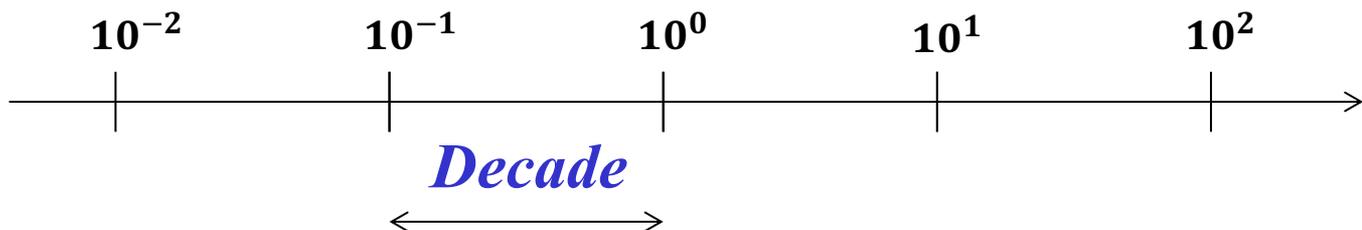
Bode diagrams definition

- ✦ In the Bode diagrams magnitude and phase of $W(j\omega)$ are represented on two different Cartesian planes.
- ✦ *The x-axis of both magnitude and phase Bode diagrams are in a logarithmic scale ($\log_{10}\omega$)*

On a logarithmic scale, the distance between two frequencies ω_1 and ω_2 depends on the difference of the logarithms and hence on the ratio on the frequencies

$$\log(\omega_2) - \log(\omega_1) = \log\left(\frac{\omega_2}{\omega_1}\right)$$

A decade is defined as the distance between two frequencies whose ratio is 10.





Bode diagrams definition

✦ The y-axis of the magnitude and phase Bode diagrams indicate respectively

✦ *the magnitude of the transfer function in dB (decibel)*

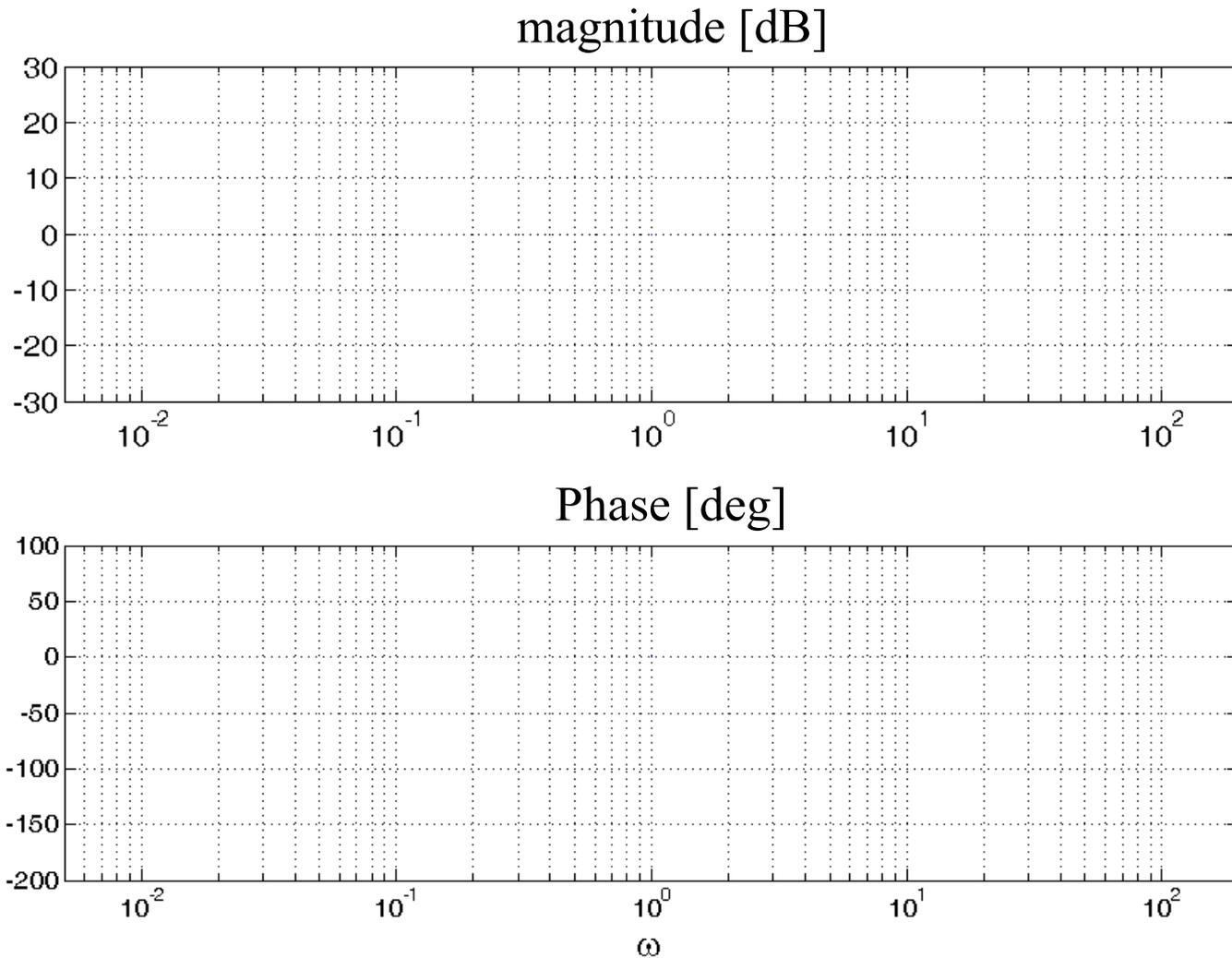
$$|W(j\omega)|_{\text{db}} = 20 \log_{10} |W(j\omega)|$$

✦ *the phase of the transfer function in degrees or radians*

$$\angle W(j\omega)$$

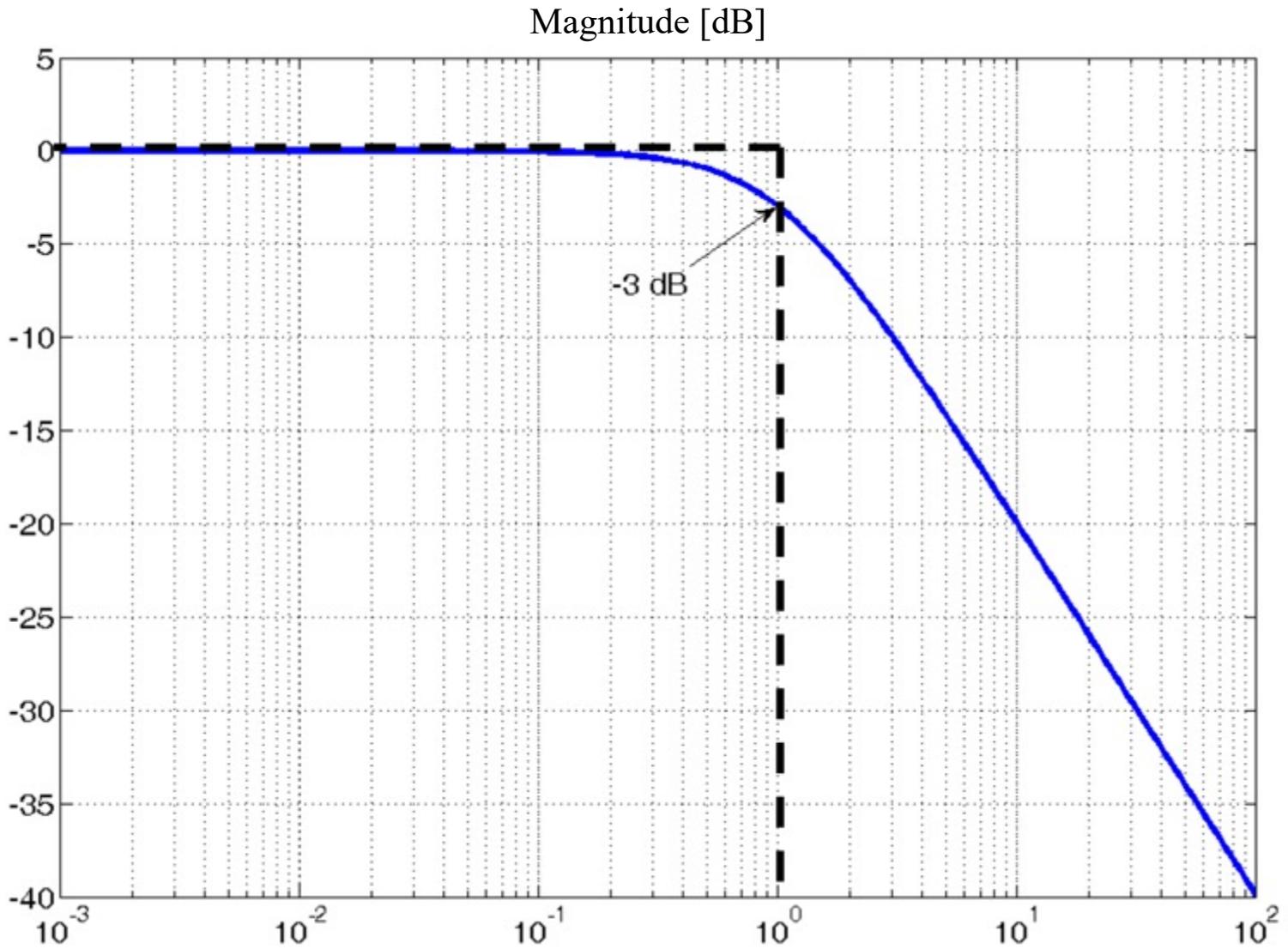


Magnitude and phase diagrams





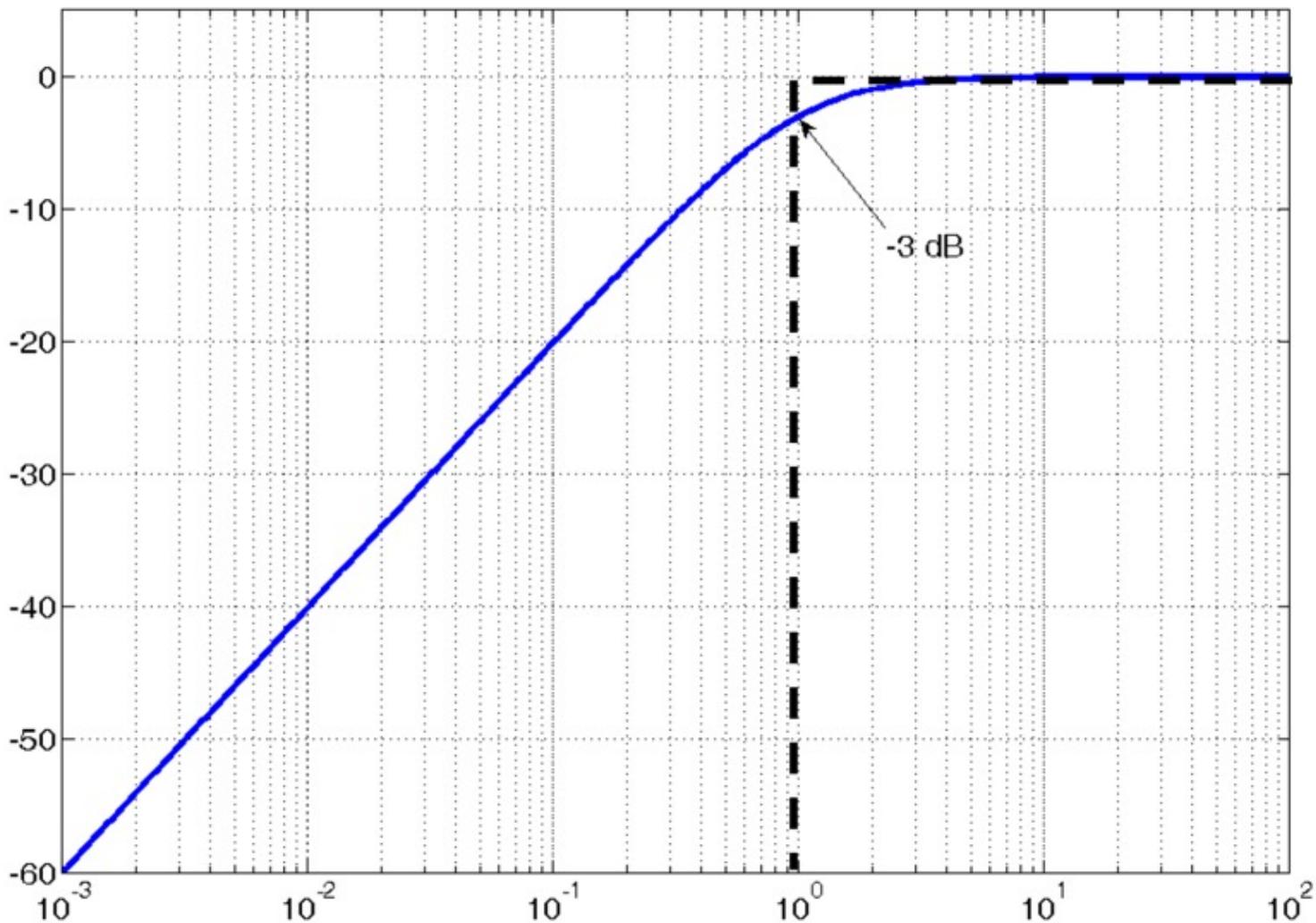
Low-pass filter





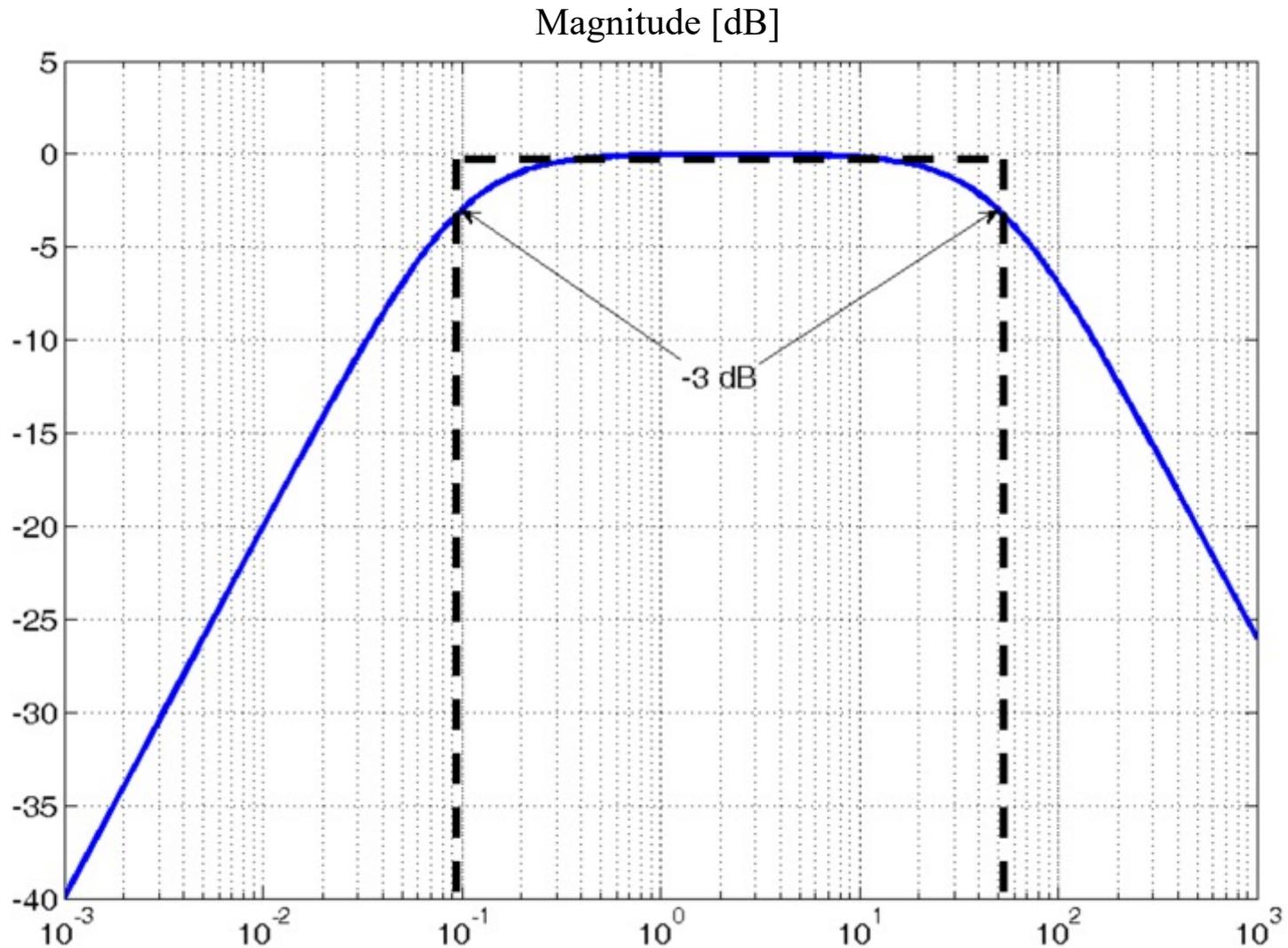
High-pass filter

Magnitude [dB]





Band-pass filter





Real Bode diagrams: trinomial term

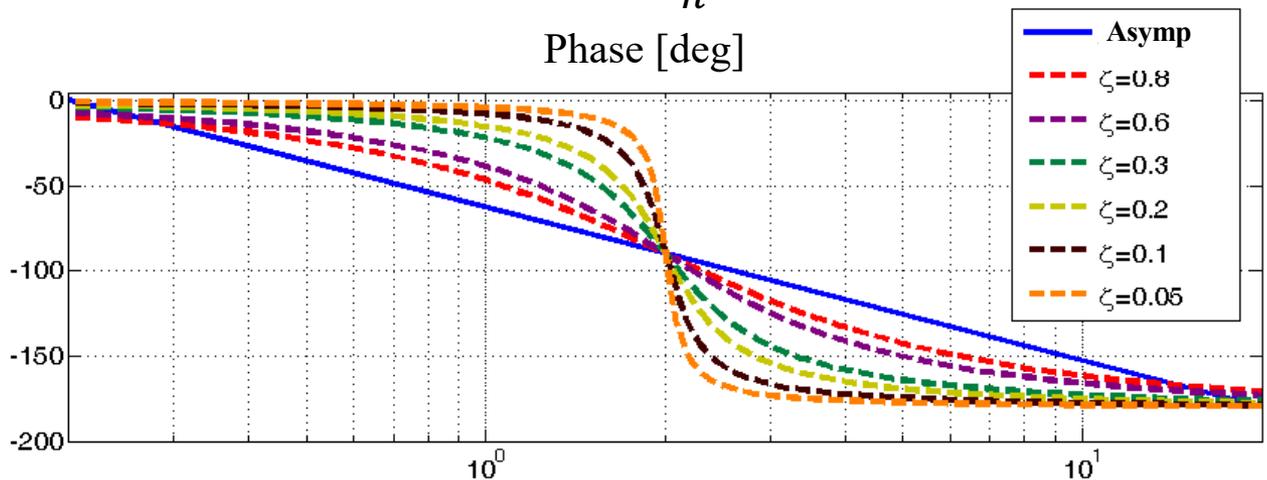
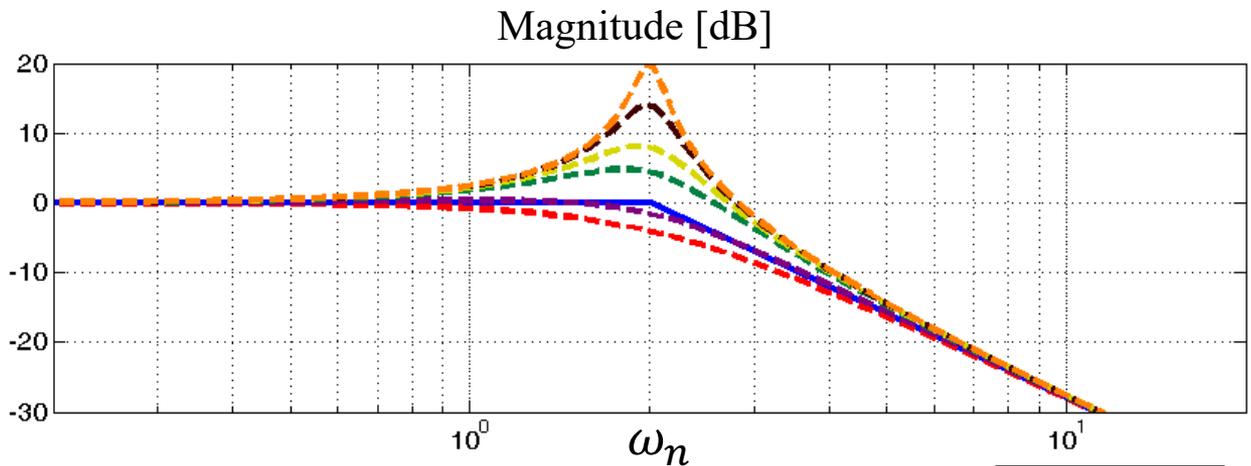
Complex conjugate poles of multiplicity one $W(s) = \left(1 + \frac{2\zeta s}{\omega_n} + \frac{s^2}{\omega_n^2}\right)^{-1}$

Peak module

$$M_p = \frac{1}{2\zeta\sqrt{1-2\zeta^2}}$$

Peak frequency

$$\omega_p = \omega_n\sqrt{1-2\zeta^2}$$



This result can be easily generalized to a generic trinomial term



Response to sinusoidal inputs of a second order LTI system

Let assume a second order LTI system described by the following t.f.:

$$G(s) = \frac{9}{s^2 + s + 9}$$

