



Course of  
"Automatic Control Systems"  
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# Control requirements: Transient performance

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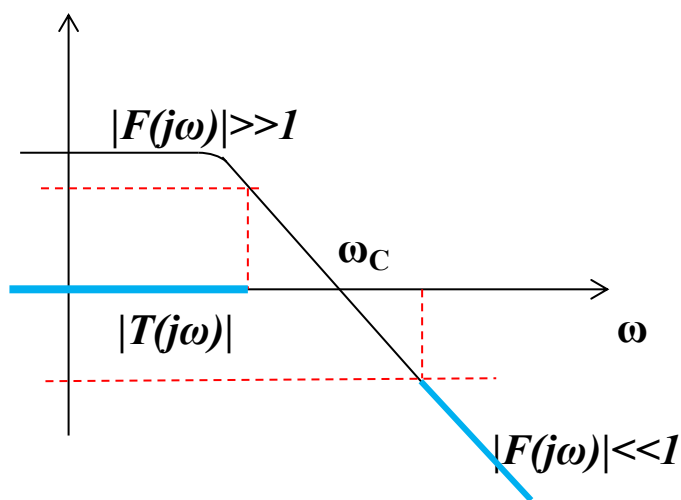
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Team code: **mfs9zfr**

# Transient performance

- ✧ We have introduced two parameters in the frequency domain related to the transient behavior
  - ✧ **Bandwidth  $B_3$  of  $T(s)$**  related to the rise time
  - ✧ **Resonant peak  $M_p$  of  $T(s)$**  related to the overshoot
- ✧ We have also assumed to refer to regularly stable open loop functions such that:
  - ✧ at low frequencies  $F(s) \gg 1 \rightarrow T(s) \cong 1$
  - ✧ at high frequencies  $F(s) \ll 1 \rightarrow T(s) \cong F(s)$



# Transient performance

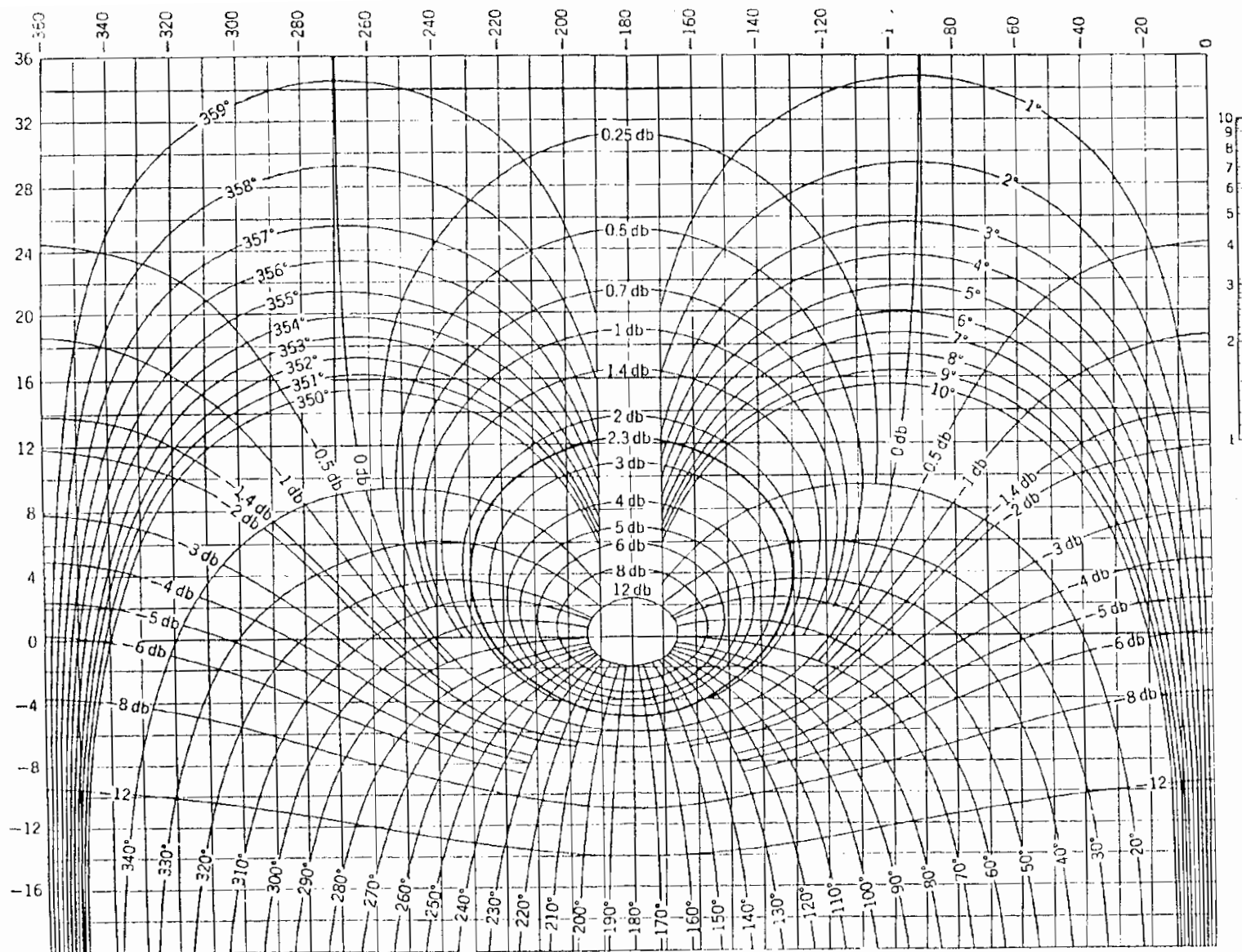
⤴ Hence

- ✧ the bandwidth  $B_3$  of  $T(s)$  is the first frequency such that for all frequencies greater than  $B_3$  the magnitude is less than  $-3db$
- ✧ the resonant peak  $M_p$  of  $T(s)$  is the maximum value assumed by the magnitude of  $T(s)$

⤴ In order to quantify the bandwidth  $B_3$  and resonant peak  $M_p$  of  $T(s)$  we need to analyze the behavior of  $T(s)$  in the two decades with center  $\omega_c$

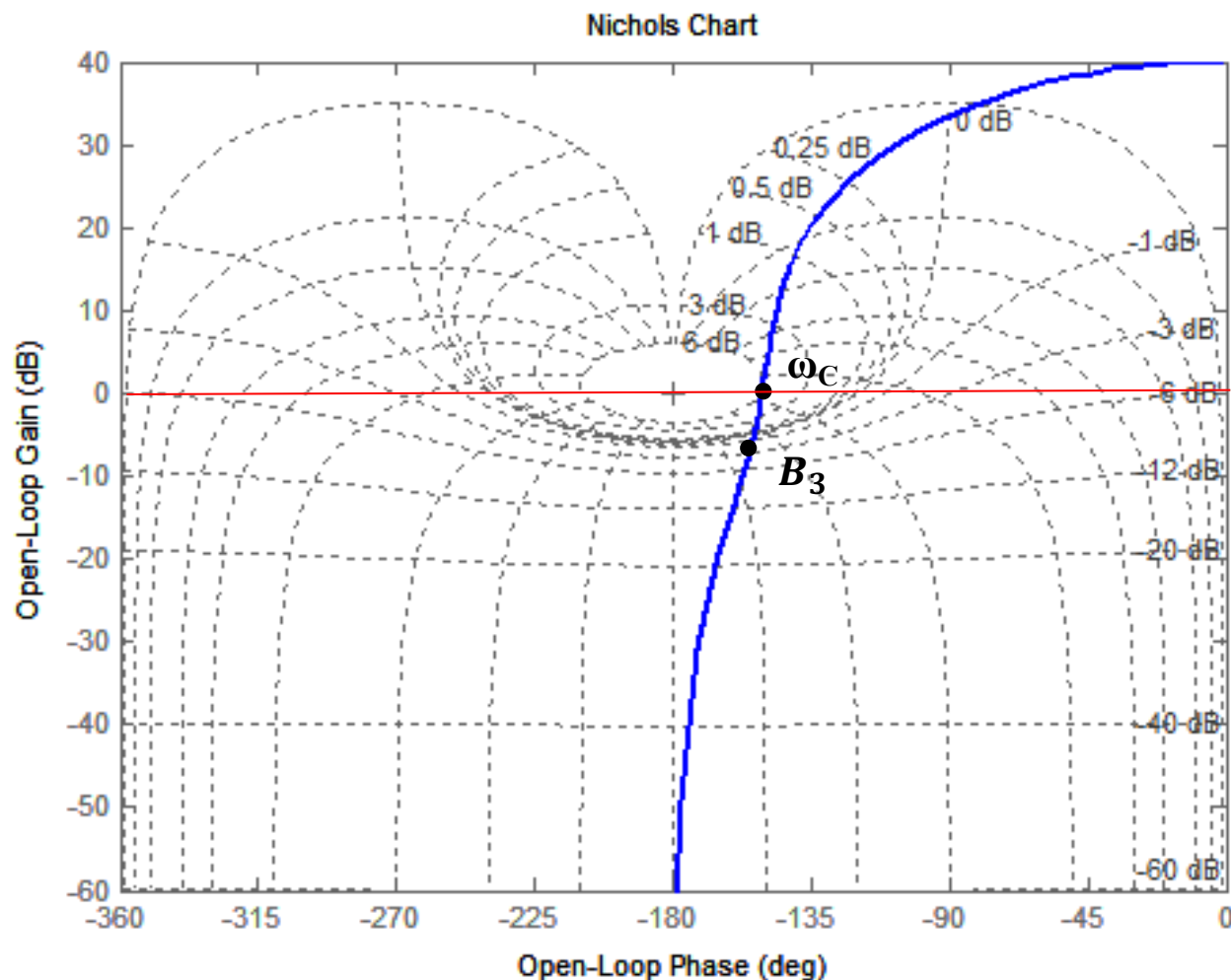
⤴ To this aim, we have introduced the so called *Nichols chart* that relates the magnitude and phase of the open loop function  $F(s)$  to the the magnitude and phase of the closed loop function  $T(s)$

# Nichols chart



# Bandwidth $B_3$ of $T(s)$

- ✧ In order to quantify the **bandwidth  $B_3$**  of  $T(s)$ , let us consider a regularly stable open loop function  $F(s)$  on the Nichols chart.

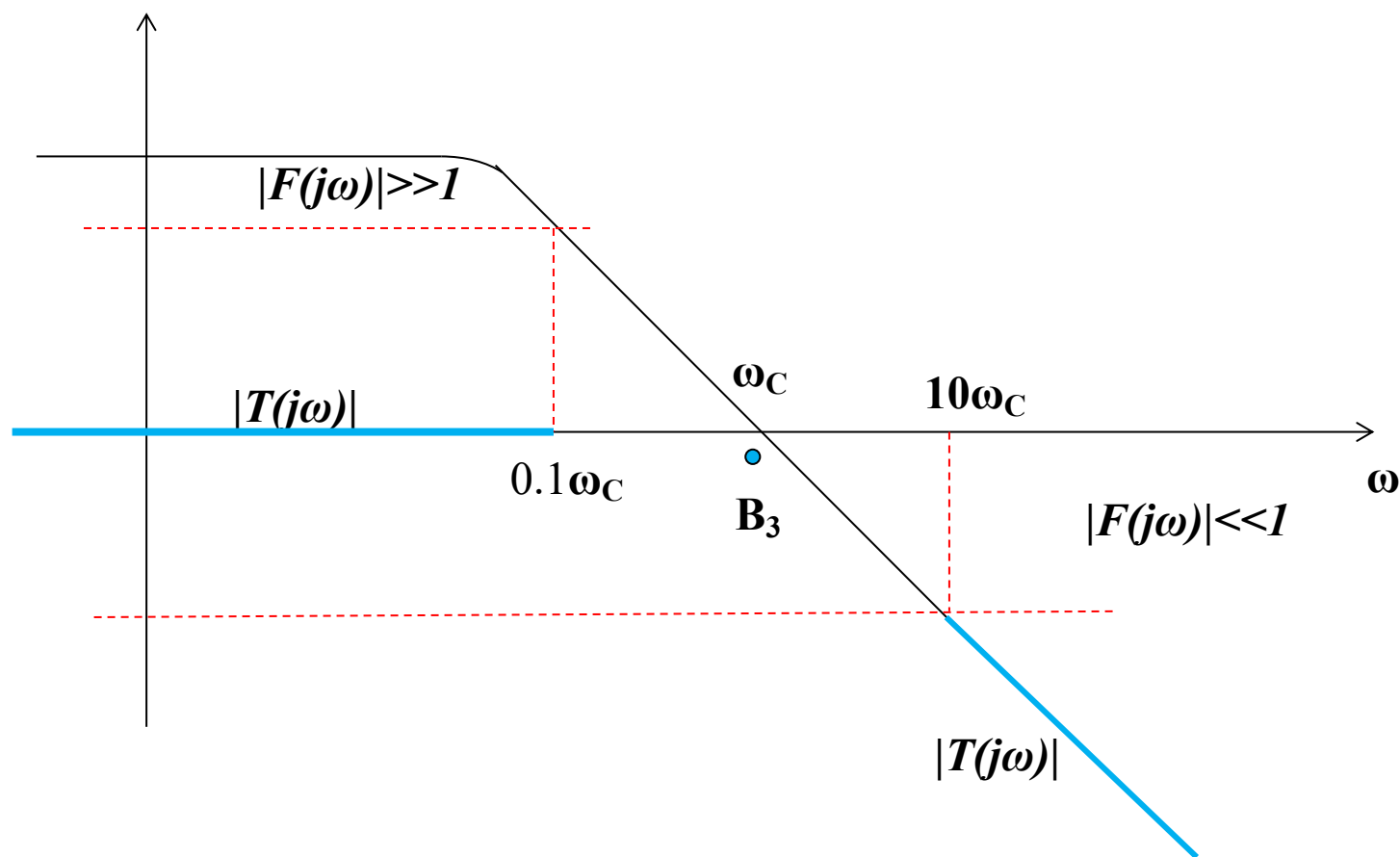


←  $|T(j0)|_{db} \cong 0$

The distance between  $\omega_c$  and  $B_3$  is very small

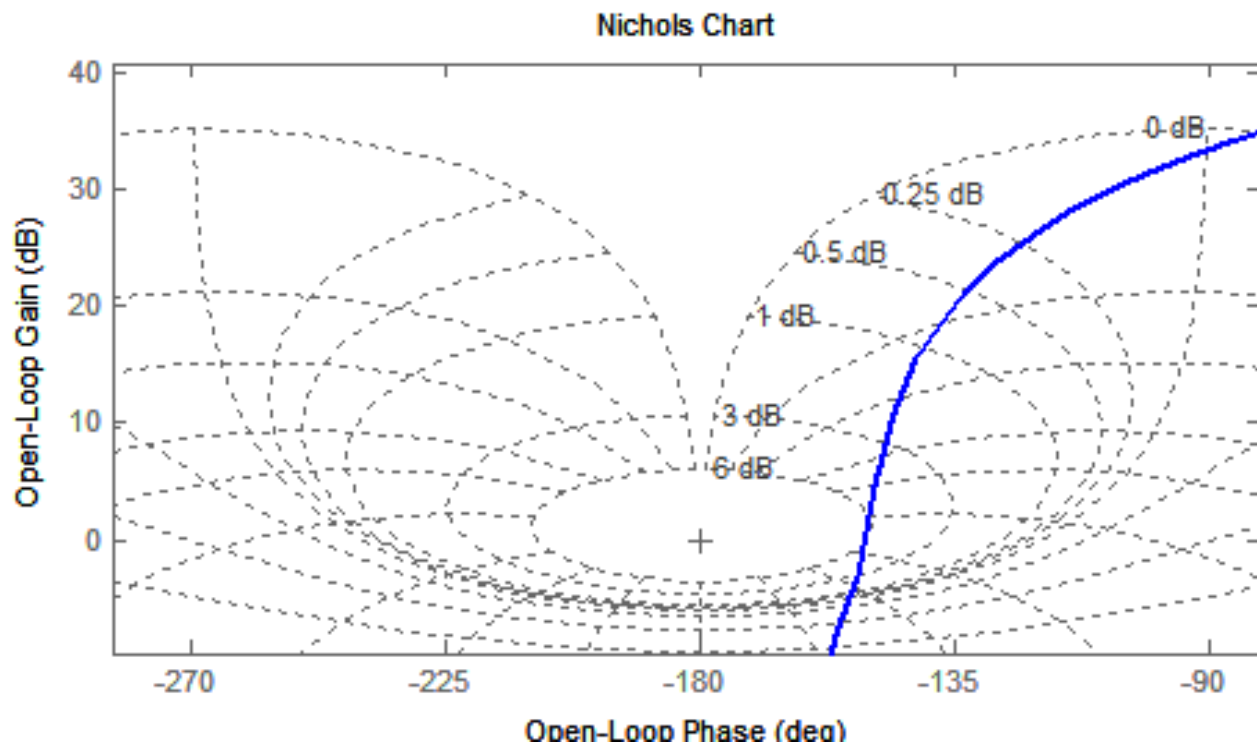
# Bandwidth $B_3$ of $T(s)$

- It implies that we can approximate the bandwidth  $B_3$  with the crossing frequency  $\omega_c$



# Resonant peak $M_p$ of $T(s)$

- ✧ Making use of the Nichols charts, the resonant peak  $M_p$  of  $T(s)$  corresponds to the magnitude of the smallest of the constant magnitude curves that is the tangent to the  $F(s)$  Nichols plot.
- ✧ The closed loop function has a resonant peak only if the Nichols plot of  $F(s)$  intersect the magnitude surface at  $0_{db}$

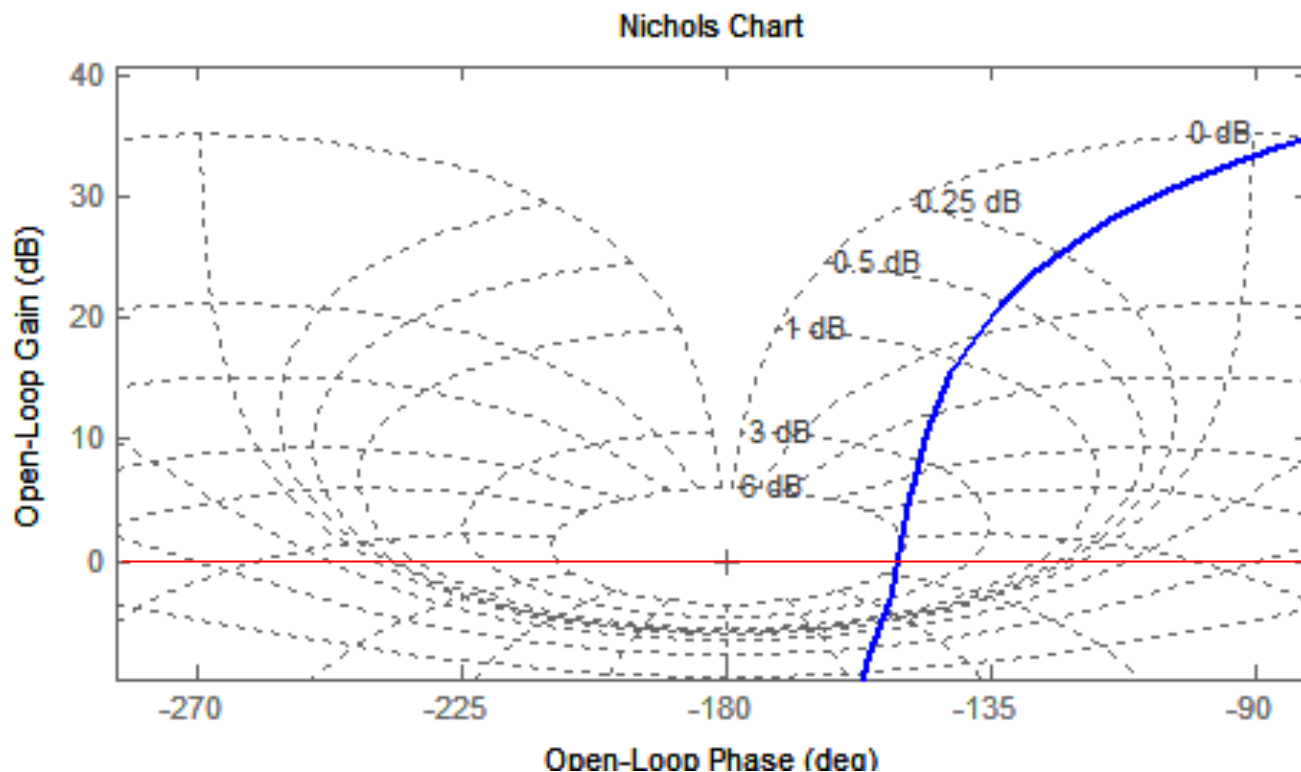


$M_p$  is approximately  $6_{db}$

# Resonant peak $M_p$ of $T(s)$

- ✦ In order to simplify the evaluation of the resonant peak, it is easy to recognized that:

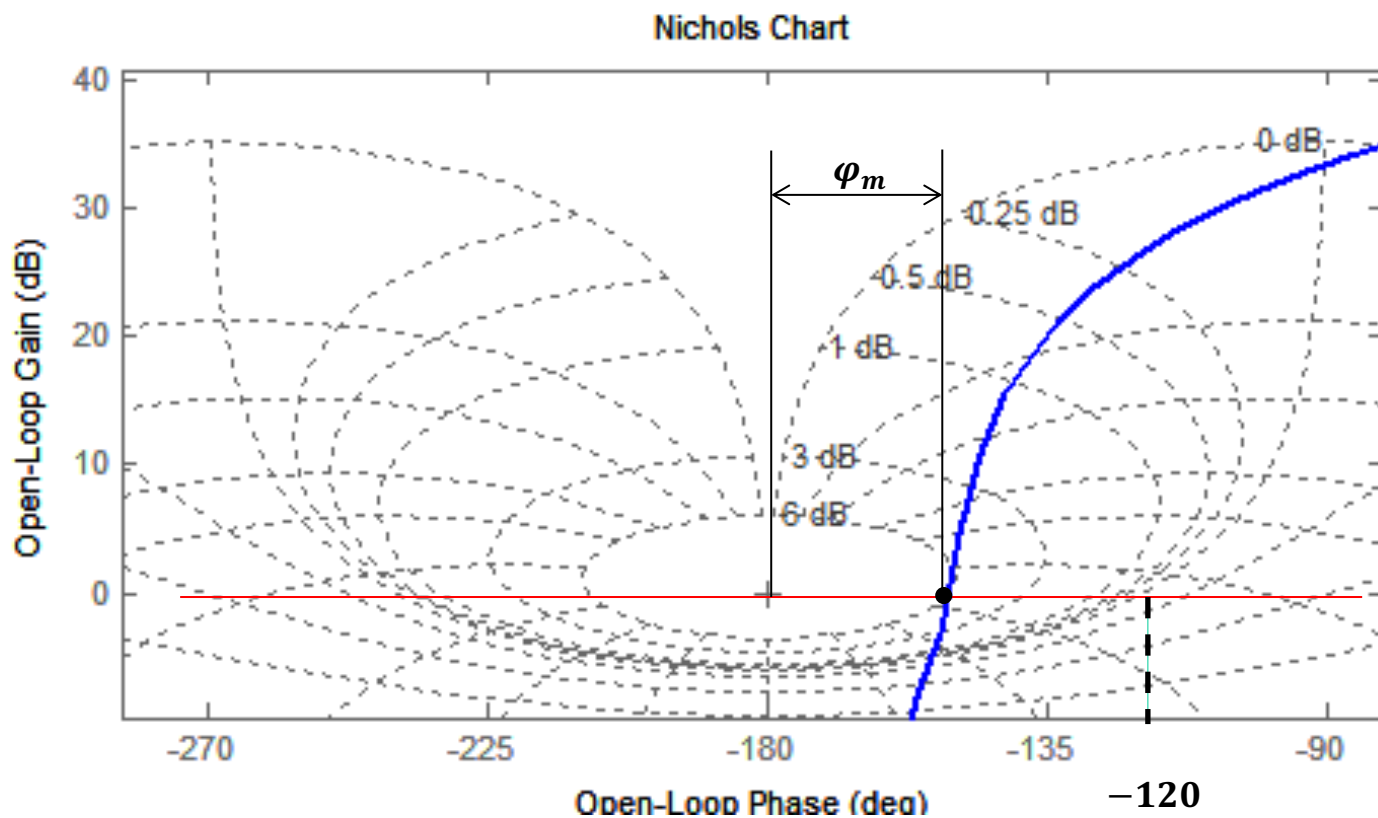
An approximate value of the resonant peak  $M_p$  is given by the value of the constant magnitude curve passing through the intersection of the Nichols plot of  $F(s)$  with the open loop  $0_{db}$  axis.





# Resonant peak $M_p$ of $T(s)$

- From the previous approximation we can conclude that
  - the resonant peak  $M_p$  is strictly related to the phase margin  $\varphi_m$  of  $F(s)$
  - The closed loop function has a resonant peak only if  $\varphi_m < 60^\circ$



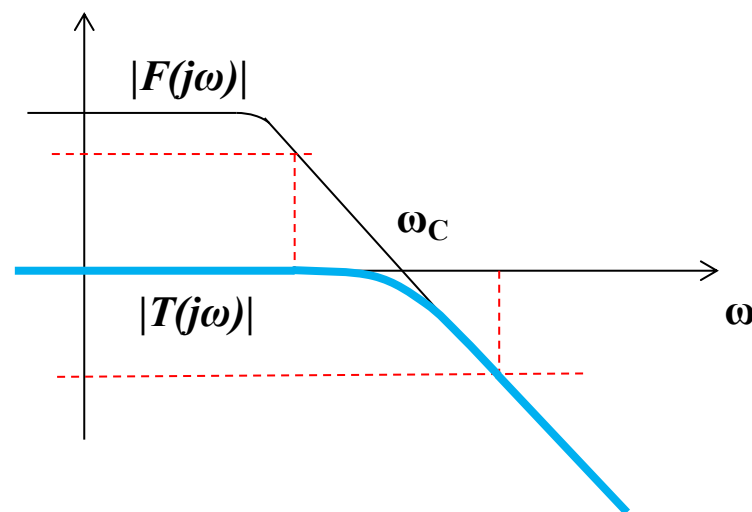
# Resonant peak $M_p$ of $T(s)$

- ✧ The previous results allows to define to possible approximation  $T_a(s)$  of the closed loop function depending on the  $F(s)$  phase margin.

**CASE 1:**  $\varphi_m > 60^\circ$

$$T_a(s) = \frac{1}{1 + s/\omega_c}$$

**First order approximation**



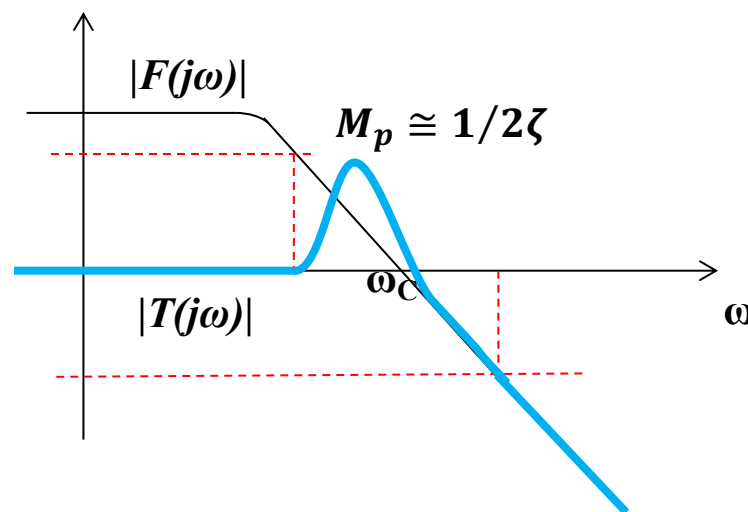
# Resonant peak $M_p$ of $T(s)$

- ✧ The previous results allows to define to possible approximation  $T_a(s)$  of the closed loop function depending on the  $F(s)$  phase margin.

**CASE 2:**  $\varphi_m < 60^\circ$

$$T_a(s) = \frac{1}{1 + 2\zeta s/\omega_c + s^2/\omega_c^2}$$

*Second order approximation*



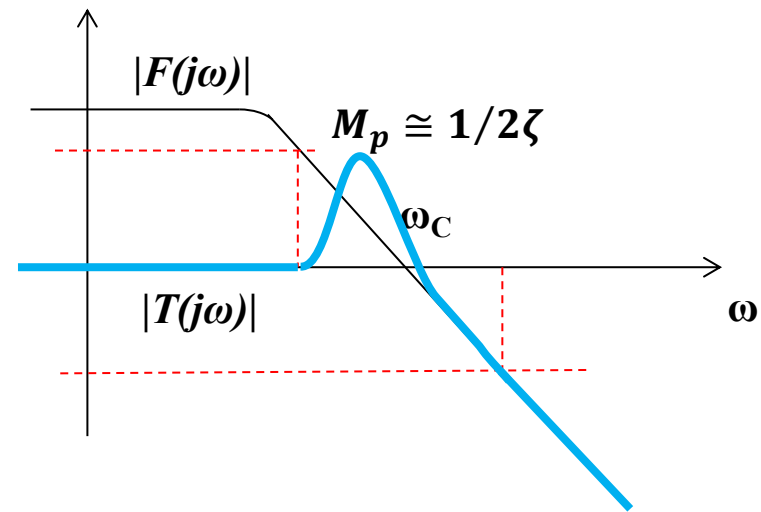
where, imposing the equality  $|T(j\omega_c)| = |T_a(j\omega_c)|$ , it is possible to prove that

$$\zeta \cong \frac{\varphi_m}{100}$$

# Damping factor and phase margin

## Second order approximation

$$T_a(s) = \frac{1}{1 + 2\zeta s/\omega_c + s^2/\omega_c^2}$$

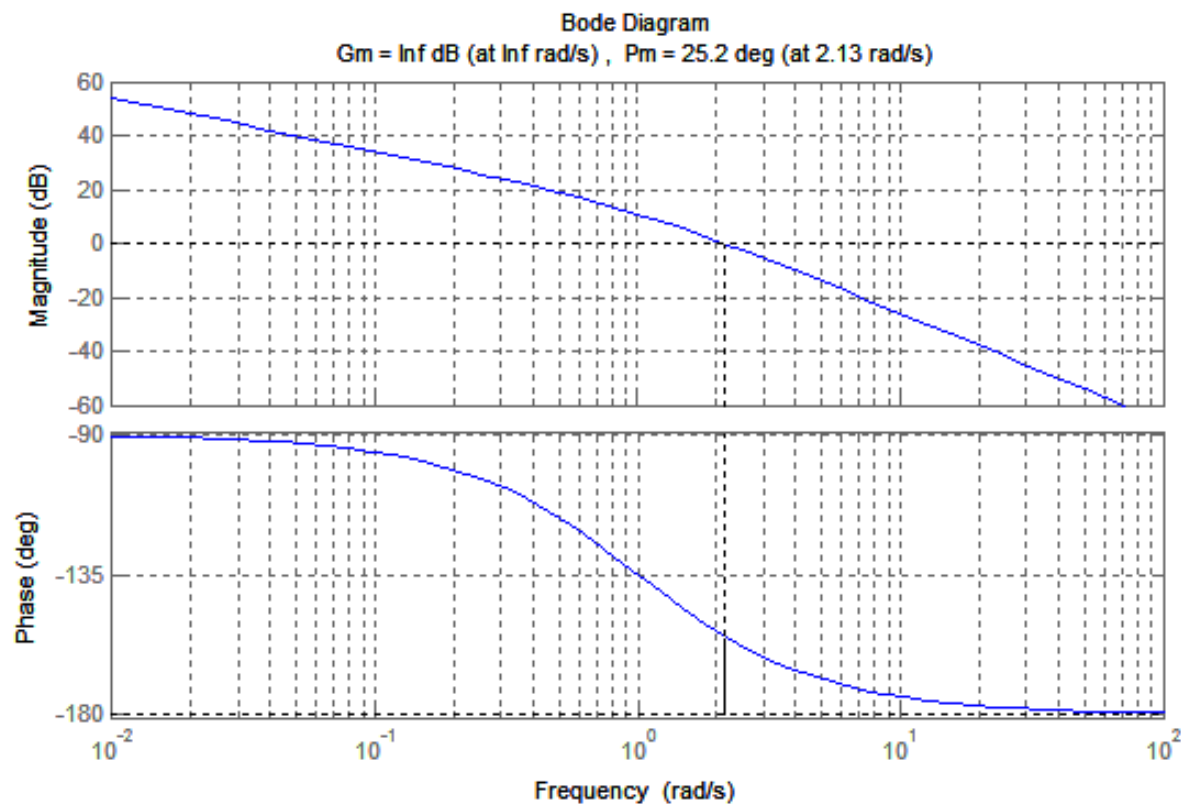


$$\left\{ \begin{array}{l} \varphi_m = 180^\circ - |\varphi_c| \\ |T(j\omega_c)| = \frac{|F(j\omega_c)|}{|1 + F(j\omega_c)|} = \frac{1}{|1 + e^{j\varphi_c}|} = \frac{1}{2\sin(\frac{\varphi_m}{2})} \\ |T_a(j\omega)| = \frac{1}{\sqrt{\left(1 - \frac{\omega^2}{\omega_c^2}\right)^2 + \left(\frac{2\zeta\omega}{\omega_c}\right)^2}} \rightarrow |T_a(j\omega_c)| = \frac{1}{2\zeta} \end{array} \right. \Rightarrow \zeta = \sin(\varphi_m/2) \cong \frac{\varphi_m}{2} * \frac{\pi}{180} \cong \frac{\varphi_m}{100}$$

# Example: closed loop approximate function $T_a(s)$

✧ Let us consider an open loop transfer function

$$F(s) = \frac{5}{s(1+s)}$$



$$\omega_c \cong 2.13 \text{ rad/s}$$

$$\varphi_m \cong 25^\circ$$



*Second order  
approximation of the  
closed loop system*

# Example: closed loop approximate function $T_a(s)$

✧ The second order approximation of the closed loop system is

$$T_a(s) = \frac{1}{1 + 2\zeta s/\omega_n + s^2/\omega_n^2}$$

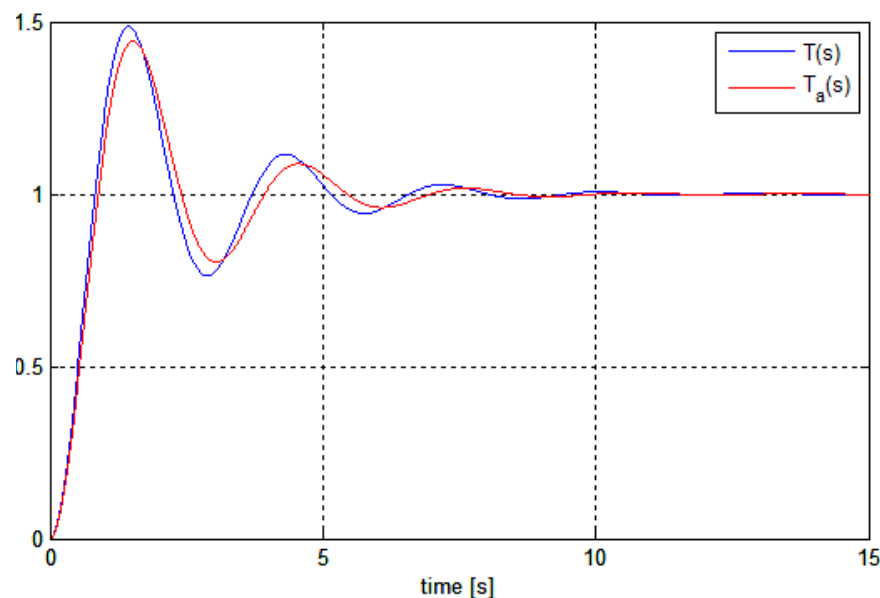
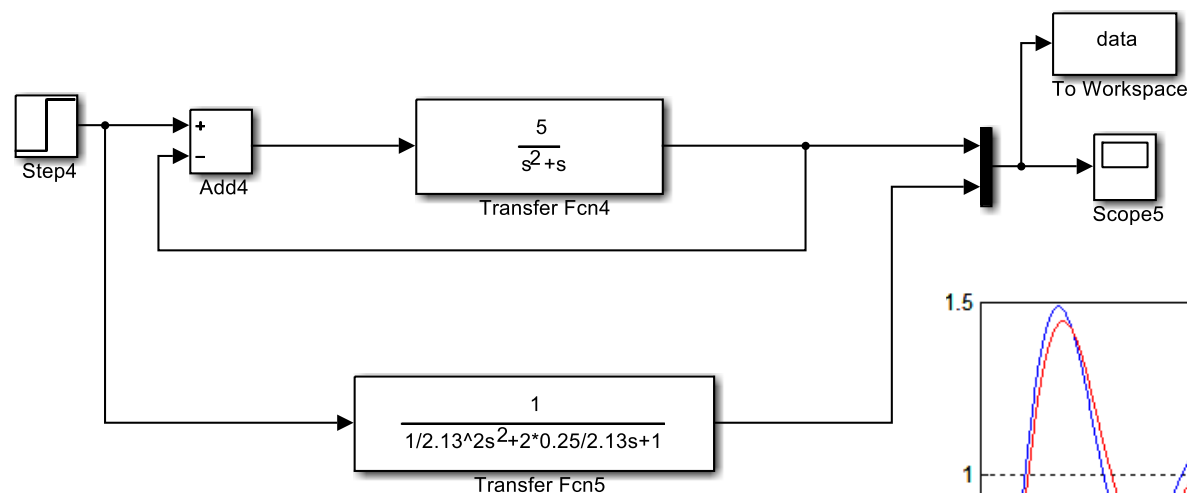
with

➤  $\zeta \cong \frac{\varphi_m}{100} = 0.25$

➤  $\omega_n = \omega_c = 2.13$

# Example: closed loop approximate function $T_a(s)$

- ✧ In order to verify the effectiveness of the second order approximated model  $T_a(s)$ , let us compare the step response of  $T(s)$  and  $T_a(s)$ .



*Rise time and overshoot of  $T_a(s)$  and  $T(s)$  are very similar*