



Course of "Automatic Control Systems"
2023/24

Harmonic response function

Prof. Francesco Montefusco

Department of Economics, Law, Cybersecurity, and Sports Sciences

Università degli Studi di Napoli Parthenope

francesco.montefusco@uniparthenope.it

Team code: **mfs9zfr**



Transient and Steady-state

- ✧ Let us consider an *asymptotically stable LTI system*.
- ✧ Given an input signal $u(t)$ and an initial condition $x(0)$, we define
 - ✧ *steady-state response* $y_{ss}(t)$, the regular behavior of the total response $y(t)$ (if exist) after an infinite time from the application of the input.
 - ✧ *transient response* $y_t(t)$, the difference between the total response of the system and the steady-state response $y_t(t) = y(t) - y_{ss}(t)$.



Transient and Steady-state

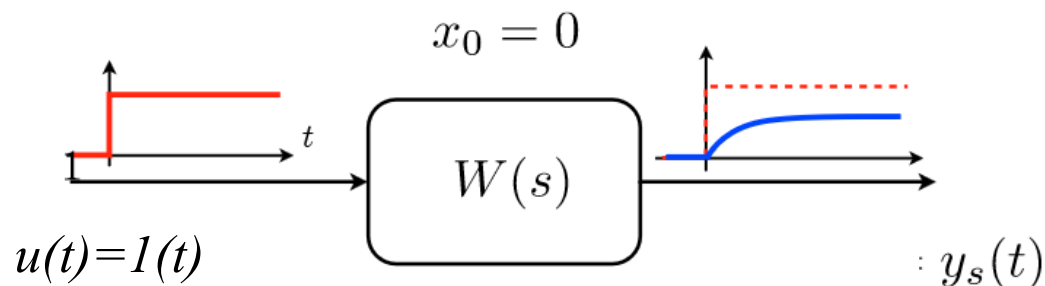
- ✧ *The steady-state response* of asymptotically stable system is independent from the initial condition.
- ✧ It depends on the particular input applied to the system

polynomial inputs \longrightarrow polynomial steady state

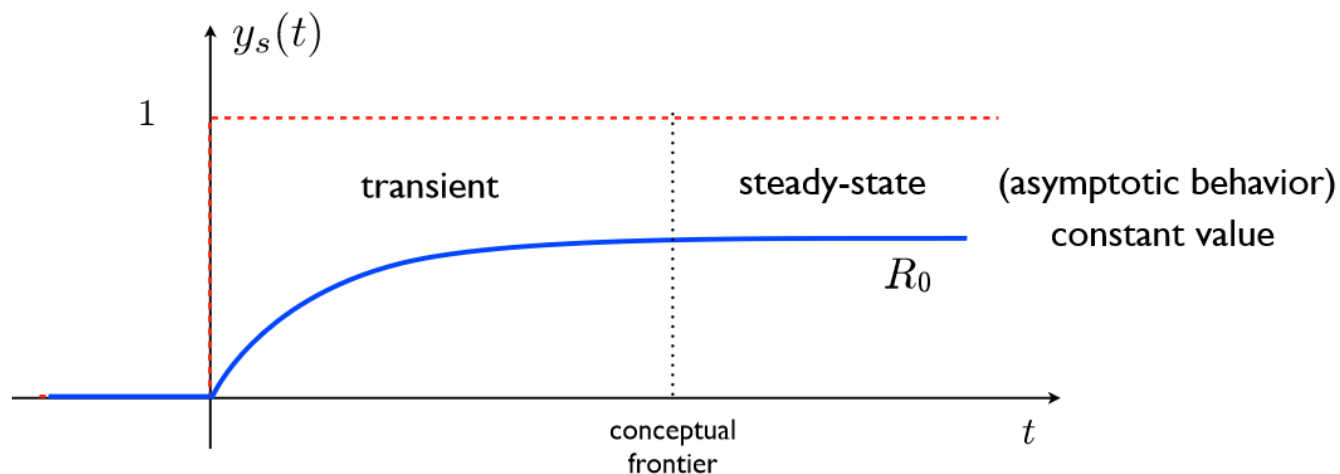
sinusoidal inputs \longrightarrow sinusoidal steady state

Step response: Transient and Steady-state

- ✧ The step response is characterized by "decaying" exponential functions related to the system evolution modes and a constant value

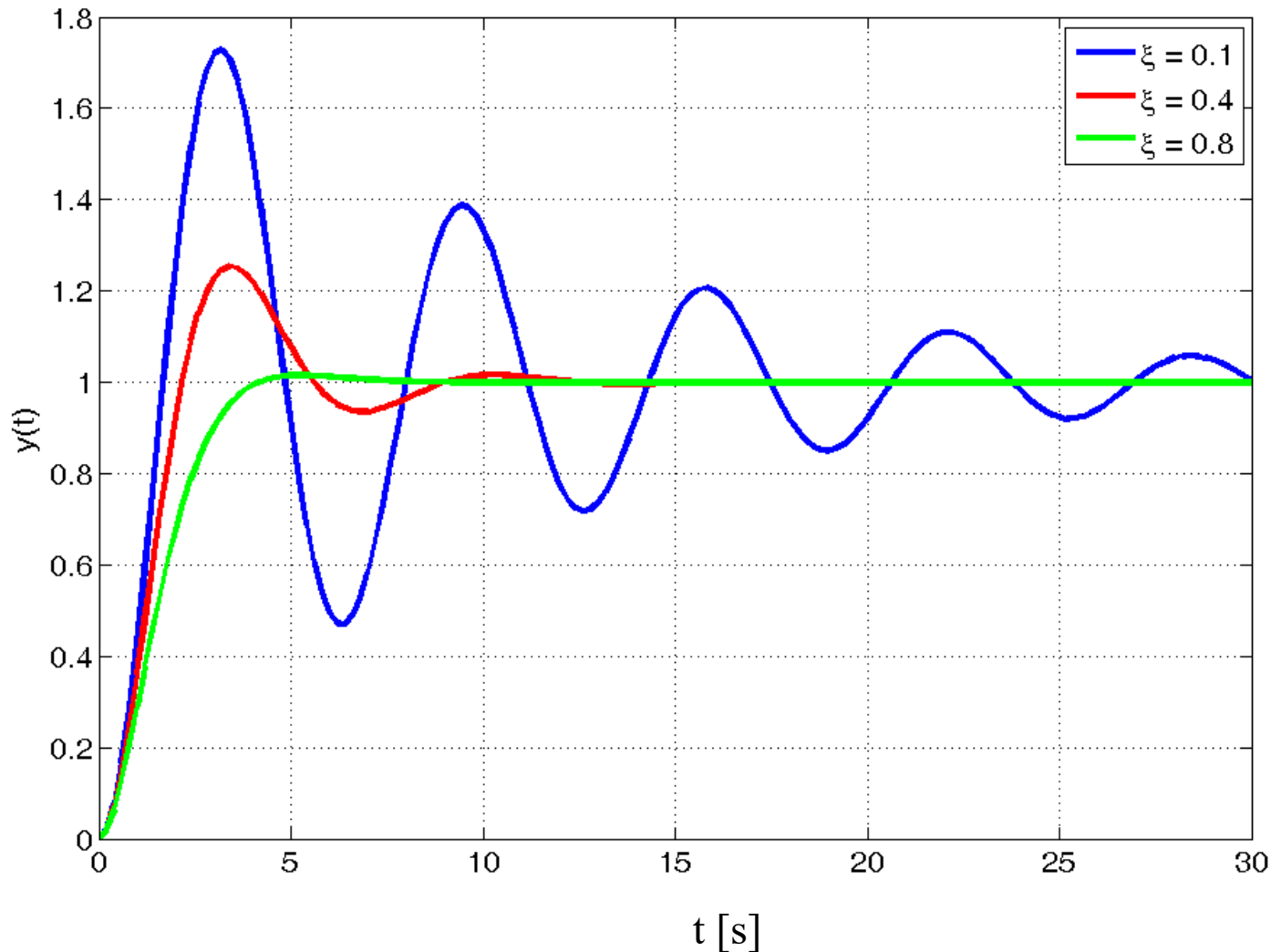


- ✧ The "decaying" exponential functions determine *the transient* part of the response while the constant term is the *steady-state* value.



Step response: Transient and Steady-state

✧ Different evolution modes determine different transient responses.



LTI system response to exponential inputs

Let us consider input signal belonging to the class of complex exponential functions:

- $u(t) = e^{st}, s = \alpha + j\omega$

Recall that

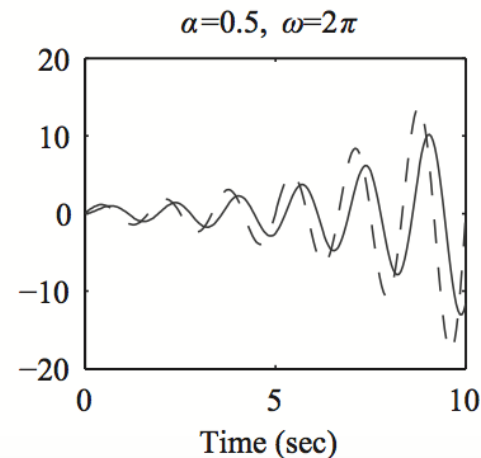
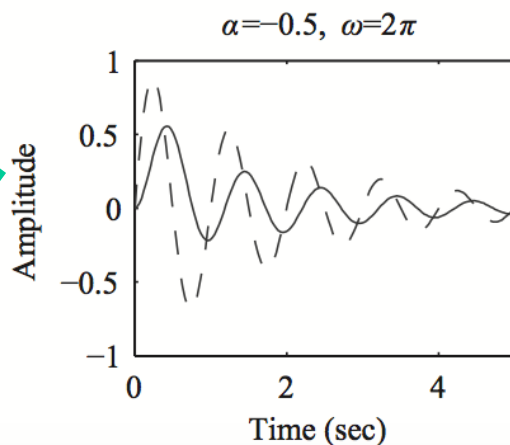
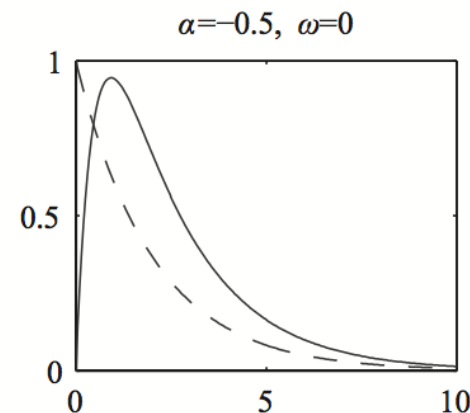
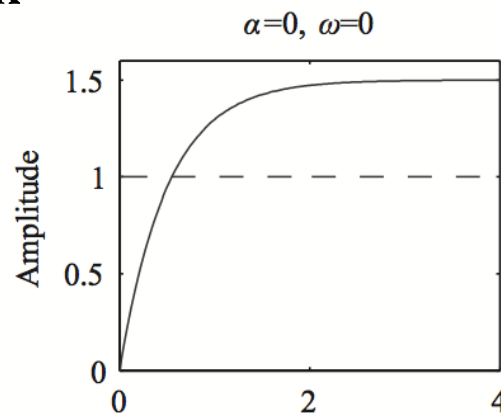
- $e^{st} = e^{(\alpha + j\omega)t}$
 $= e^{\alpha t}(\cos(\omega t) + j \sin(\omega t))$

Many signals may be written as a linear combination of complex exponential functions.



After an initial transient, the LTI response is proportional to the input (i.e. exhibits the same form of the input).

$$\text{LTI: } \dot{y}(t) + 2y(t) = 3u(t)$$



LTI system response to exponential input

- A SISO system of n -th order, $t_0=0$, $x(0)=x_0$:

$$\begin{aligned} \dot{x}(t) &= A x(t) + B u(t) \\ y(t) &= C x(t) + D u(t) \end{aligned} \quad \xrightarrow{\mathcal{L}} \quad \begin{aligned} sX(s) - x_0 &= A X(s) + B U(s) \\ Y(s) &= C X(s) + D U(s) \end{aligned}$$

$$X(s) = (sI - A)^{-1} x_0 + (sI - A)^{-1} B U(s)$$

$$W(s) = C(sI - A)^{-1} B + D$$

$$Y(s) = \underbrace{C(sI - A)^{-1} x_0}_{Y_l} + \underbrace{(C(sI - A)^{-1} B + D)}_{Y_f} U(s)$$

- For exponential input:

$$\begin{aligned} u(t) = e^{\lambda t}, t \geq 0 & \xrightarrow{\mathcal{L}} Y_f(s) = W(s) U(s) = W(s) \frac{1}{s - \lambda} = \dots + \frac{k}{s - \lambda} \\ & \xrightarrow{\mathcal{L}^{-1}} \dots + k e^{\lambda t} \end{aligned}$$

LTI system response to exponential input

- *Initial condition* $x(0)$ that nullifies the evolution modes

$$\Rightarrow x(t) = x(0)e^{\lambda t}$$

By using the state equation

$$\dot{x}(t) = A x(t) + B u(t) \Rightarrow \lambda x(0)e^{\lambda t} = A x(0)e^{\lambda t} + B e^{\lambda t}$$

$$\Rightarrow (\lambda I - A)x(0) = B \Rightarrow x(0) = (\lambda I - A)^{-1}B, \text{ if } \lambda \text{ is not an eigenvalue of } A$$

Then,

$$x(t) = x(0)e^{\lambda t} = (\lambda I - A)^{-1}B e^{\lambda t}, t > 0$$

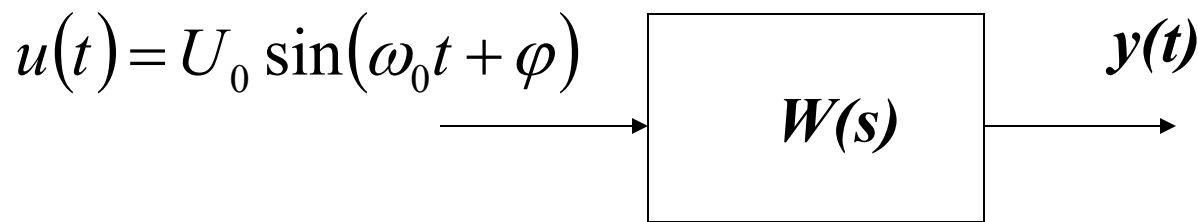
$$y(t) = C x(t) + D u(t) = C(\lambda I - A)^{-1}B e^{\lambda t} + D e^{\lambda t} = (C(\lambda I - A)^{-1}B + D)e^{\lambda t} = W(\lambda)e^{\lambda t}.$$

If the system is asymptotically stable, $x(t) = (\lambda I - A)^{-1}B e^{\lambda t}$, $y(t) = W(\lambda)e^{\lambda t}$,

these functions represent the asymptotic movements of the state and the output of the system, for any initial condition $x(0)$.

Steady state response at sinusoidal inputs

- Let us consider an asymptotically stable LTI system with a transfer function $W(s)$ subject to a sinusoidal input signal



- The evaluation of the steady state response of LTI system to sinusoidal inputs is very interest taking into account that *any signal can be decomposed in the sum of a finite (periodic signal) and infinite number (aperiodic signal) of sinusoids by means of the Fourier series.*

Steady state response at sinusoidal inputs

- ✧ It is possible to prove that the steady state response of an LTI system with transfer function $W(s)$ to a sinusoidal inputs $u(t) = U_0 \sin(\omega_0 t + \phi)$ can be written in the time domain as

$$y_{ss}(t) = U_0 |W(s)|_{s=j\omega_0} \sin(\omega_0 t + \phi + \angle W(s)_{s=j\omega_0})$$

where

- ✧ $|W(s)|_{s=j\omega_0}$ is the magnitude of the Laplace transform of $W(s)$ evaluated in $s = j\omega_0$.
- ✧ $\angle W(s)|_{s=j\omega_0}$ is the phase of the Laplace transform of $W(s)$ evaluated in $s = j\omega_0$.



LTI system response to sinusoidal input

For a sinusoidal input,

$$u(t) = \sin(\omega t), t \geq 0, \omega = \frac{2\pi}{T},$$

we exploit the results achieved for an exponential input.

Indeed, $\sin(\omega t) = \text{Im}(e^{j\omega t})$. **Recall that** $e^{j\omega t} = \cos(\omega t) + j \sin(\omega t)$.

For $\tilde{u}(t) = e^{j\omega t}$, if **A** without eigenvalues in $\pm j\omega$, then there is an initial state $x(0) = (j\omega I - A)^{-1}B$, such that the movements of the state and the output:

- $\tilde{x}(t) = x(0)e^{j\omega t} = (j\omega I - A)^{-1}Be^{j\omega t}, t > 0$
- $$\begin{aligned}\tilde{y}(t) &= C x(t) + D u(t) = C(j\omega I - A)^{-1}Be^{j\omega t} + De^{j\omega t} \\ &= (C(j\omega I - A)^{-1}B + D)e^{j\omega t} = W(j\omega)e^{j\omega t} \\ &= |W(j\omega)|e^{j\arg(W(j\omega))}e^{j\omega t} = |W(j\omega)|e^{j(\omega t + \arg(W(j\omega)))}\end{aligned}$$

Recall that $z = a + ib = r(\cos \theta + i \sin \theta) = re^{j\theta}$ **with** $\theta = \arg(z) = \tan^{-1} \frac{b}{a} + 2k\pi$



LTI system response to sinusoidal input

$$\tilde{x}(t) = (j\omega I - A)^{-1} B e^{j\omega t}, \quad \tilde{y}(t) = |W(j\omega)| e^{j(\omega t + \arg(W(j\omega)))}, t > 0$$

These functions represent the asymptotic movements, for LTI asymptotically stable with $\tilde{u}(t) = e^{j\omega t}$.

For $u(t) = \sin(\omega t) = \text{Im}(e^{j\omega t})$, then

$$x(t) = \text{Im}(\tilde{x}(t)), \quad y(t) = \text{Im}(\tilde{y}(t)) = |W(j\omega)| \sin(\omega t + \arg(W(j\omega))), t > 0$$

In general for $u(t) = U \sin(\omega_0 t + \varphi), t > 0$,

there is an initial state such that the output is a sinusoidal signal:

$$y(t) = Y \sin(\omega_0 t + \psi), t > 0$$

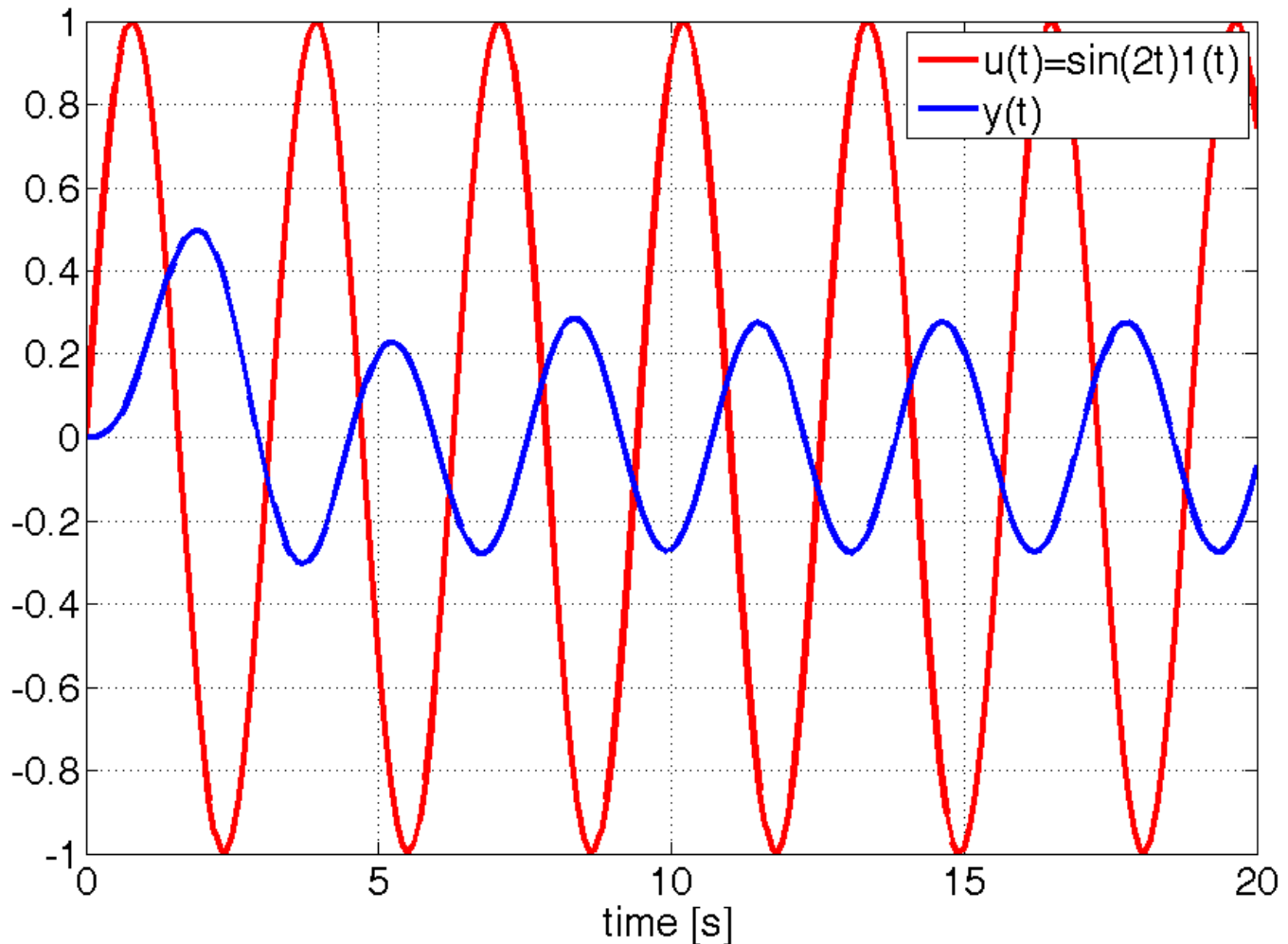
with $Y = |W(j\omega_0)|U$,

where $W(j\omega_0) = C(j\omega_0 I - A)^{-1} B + D$, and $\psi = \varphi + \arg(W(j\omega_0))$.

If the system is a.s. $y(t)$ (and $x(t)$) represents the asymptotic movement of the output (state).

Steady state response at sinusoidal inputs

Total response of system $W(s) = 1/(s^2 + s + 1)$ to the input $u(t) = \sin(2t) \cdot 1(t)$.



- ✧ The proposed result can be summarized as follows:
 - ✧ The magnitude of a sinusoidal input signal $u(t) = \sin(\omega_0 t + \phi)$ is *amplified or reduced* by a linear system depending on the value of $|W(s)|_{s=j\omega_0}$.
 - ✧ An input signal $u(t) = \sin(\omega_0 t + \phi)$ is *phase shifted* by a linear system depending on the value of $\angle W(s)|_{s=j\omega_0}$.
- ✧ In other terms, *a linear system can be designed as a filter* able to amplify without distortion a certain set of input signals Ω_1 and reduce or eliminate another signals.
- ✧ Possible structures of filters will be discussed in the following lessons.



Harmonic response function

- ✧ This result underlines the importance of the function $W(j\omega)$ for the analysis of the forced response of LTI systems.
- ✧ The function $W(j\omega)$ is called *harmonic response function* of the system.
- ✧ In the following we present a method able to rapidly evaluate the magnitude and the phase $W(j\omega)$ as a function of ω .

$W(j\omega)$ general form

- ✧ Given an asymptotically stable LTI system, the *harmonic response function* $W(j\omega)$ is given by the ratio of polynomial with real and complex conjugate roots

$$W(j\omega) = W(s) \Big|_{s=j\omega} = K \frac{s^\nu \prod_i (1 + \sigma_i s)^{m_i} \prod_q \left(1 + \frac{2\xi_q}{\omega_{nq}} s + \frac{s^2}{\omega_{nq}^2} \right)^{\eta_q}}{\prod_j (1 + \tau_j s)^{n_j} \prod_p \left(1 + \frac{2\zeta_p}{\omega_{np}} s + \frac{s^2}{\omega_{np}^2} \right)^{\kappa_p}} \Big|_{s=j\omega}$$



$W(j\omega)$ general form

- ✧ *Bode diagrams* allows to extract the magnitude and the phase of $W(j\omega)$ as a function of ω
- ✧ Bode diagrams are a main tool for the closed loop control design
- ✧ For the closed loop control problems we will be interested to analyze magnitude and the phase of transfer functions $W(s)$ also in case of stable and unstable systems
- ✧ In that cases, $W(s)|_{s=j\omega}$ will be not the harmonic function.