



Course of "Industrial Automation"
2023/24

Analysis of the Sample and Hold - Sampled-Data Systems

Prof. Francesco Montefusco

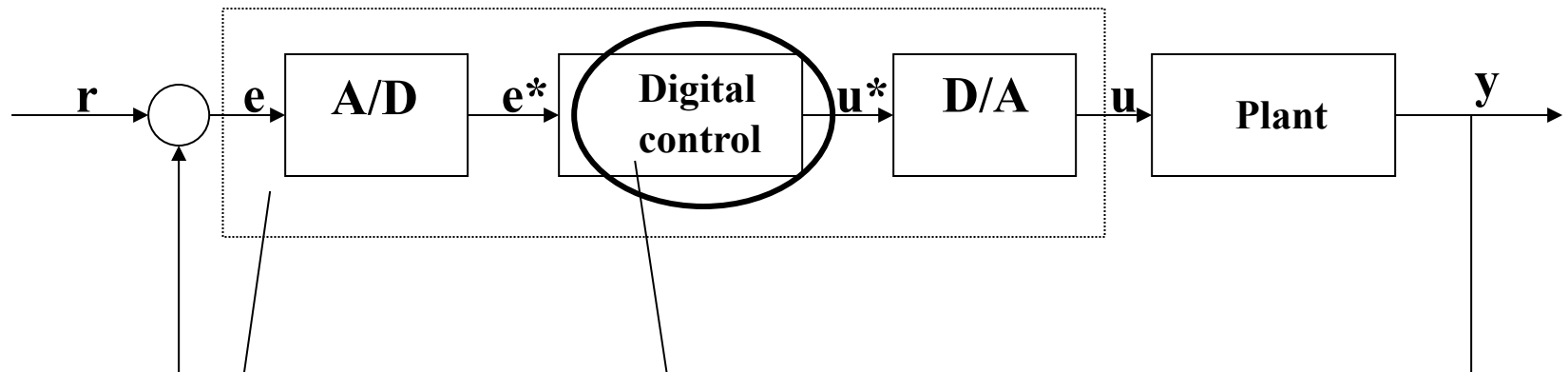
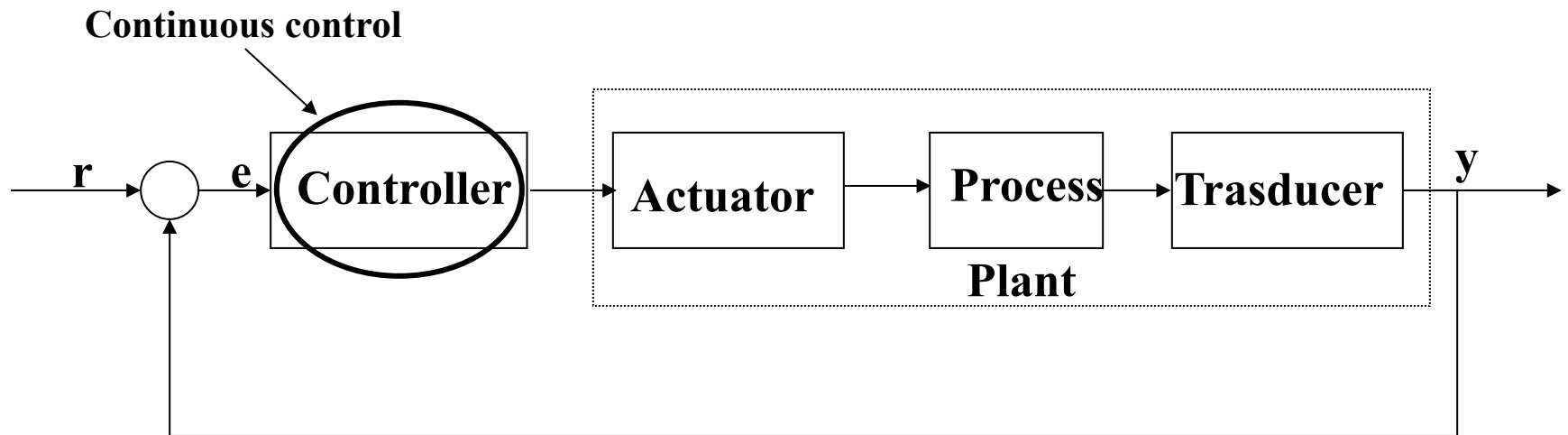
Department of Economics, Law, Cybersecurity, and Sports Sciences

Università degli Studi di Napoli Parthenope

francesco.montefusco@uniparthenope.it

Team code: **vgxlryz**

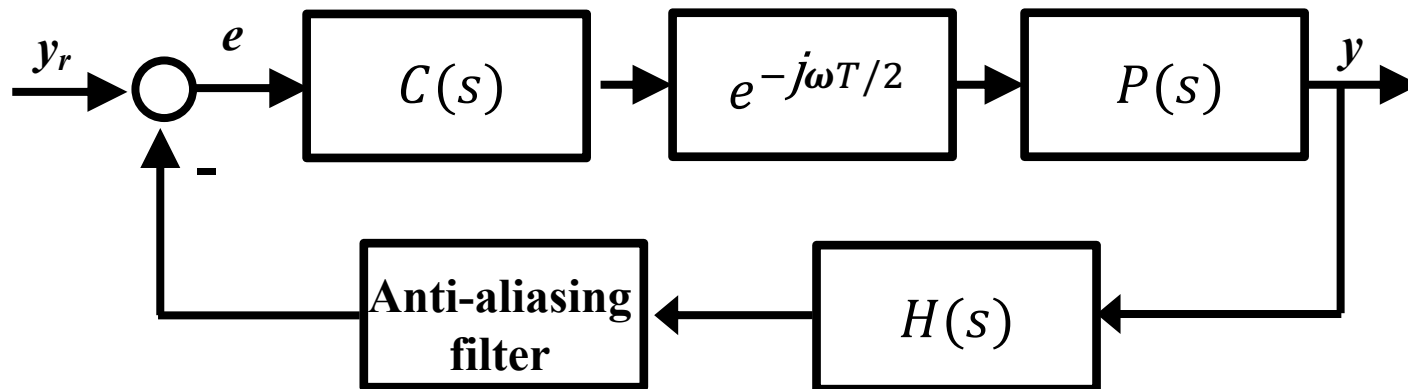
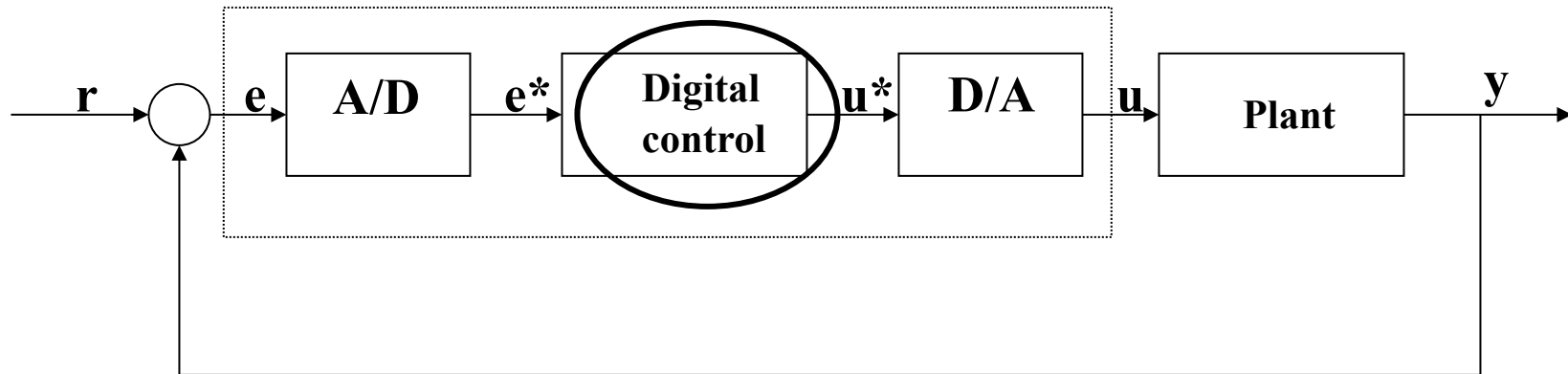
Continuous vs. digital



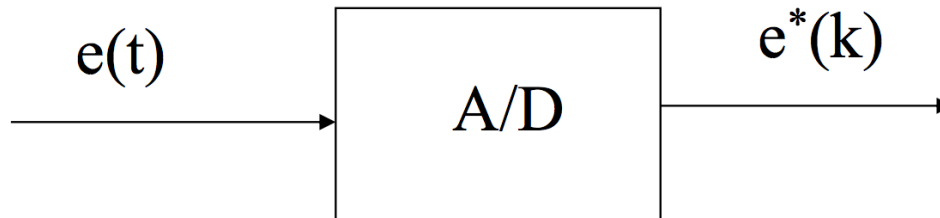
Continuous-time system

Discrete-time system

Scheme of the digital control system in continuous-time

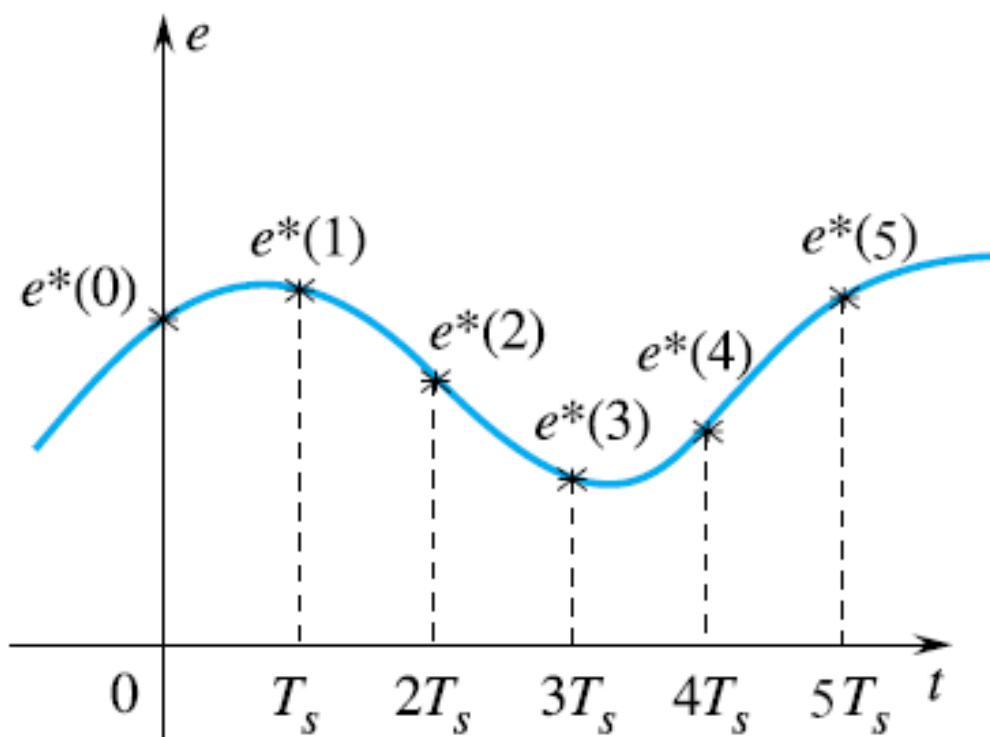


- The digital controller is a discrete-time system and the plant to be controlled is a continuous-time system.
- It is needed a device that transforms a continuous signal into a discrete one.



- Such device is the analog-to-digital converter (A/D).

Ideal sampler



- Periodic sampling: the sampling instants are equally spaced, or k , i.e. $t_k = kT_s$ ($k=0,1,2,\dots$), with T_s representing the sampling time.
- The hold circuit holds the value of the sampled signal over a specified period of time.

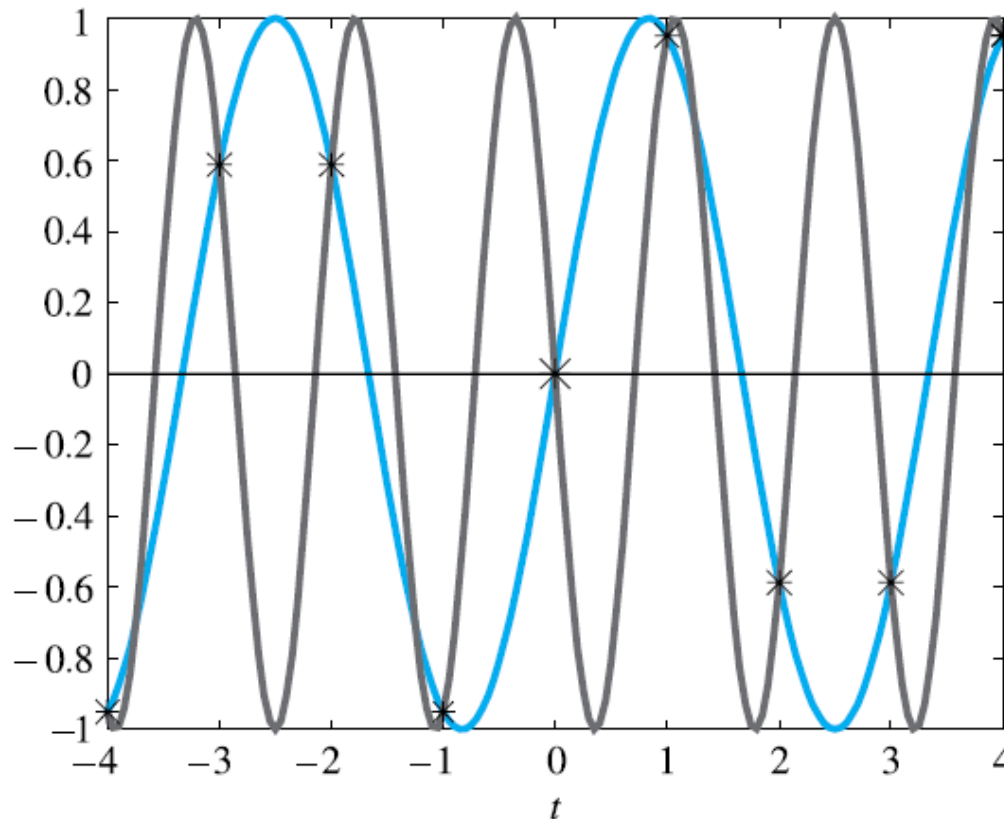


Sampling operation

- The common problem when sampling a signal is the loss of information.
- Indeed, it is obvious that the same signal $e^*(k)$ can be generated by infinite continuous-time functions $e(t)$.
- Hence, given a signal $e^*(k)$ it is impossible to go back to the original signal $e(t)$.

Sampling operation - example

Given a set of signals, $e_h(t) = \sin((\alpha + 2h)\pi t)$



$$e_0(t) = \sin(0.6\pi t)$$

$$e_{-1}(t) = \sin(-1.4\pi t)$$

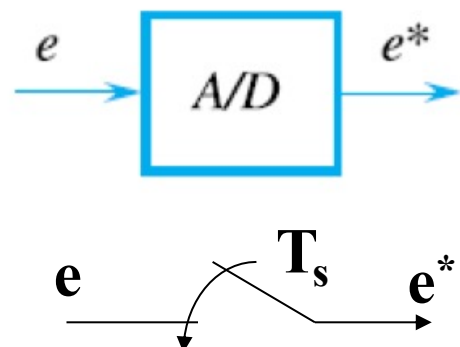
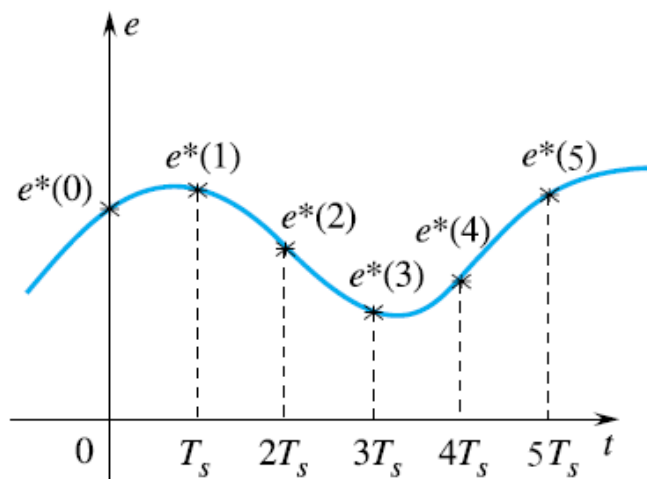
$$\text{---} e_0(t)$$

$$\text{---} e_{-1}(t)$$

$$T_s = 1$$

$$e_0^*(k) = e_{-1}^*(k)$$

Ideal sampler – Spectrum of a sampled signal

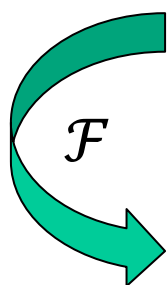


$$\omega_s = 2\pi f_s = \frac{2\pi}{T_s}$$

$$e^*(k) = e(kT_s)$$

Assume $e_s(t)$ as the mathematical representation of the sampling operation:

$$e_s(t) = e(t) \sum_{k=0}^{\infty} \delta(t - kT_s) = \sum_{k=0}^{\infty} e(kT_s) \delta(t - kT_s)$$

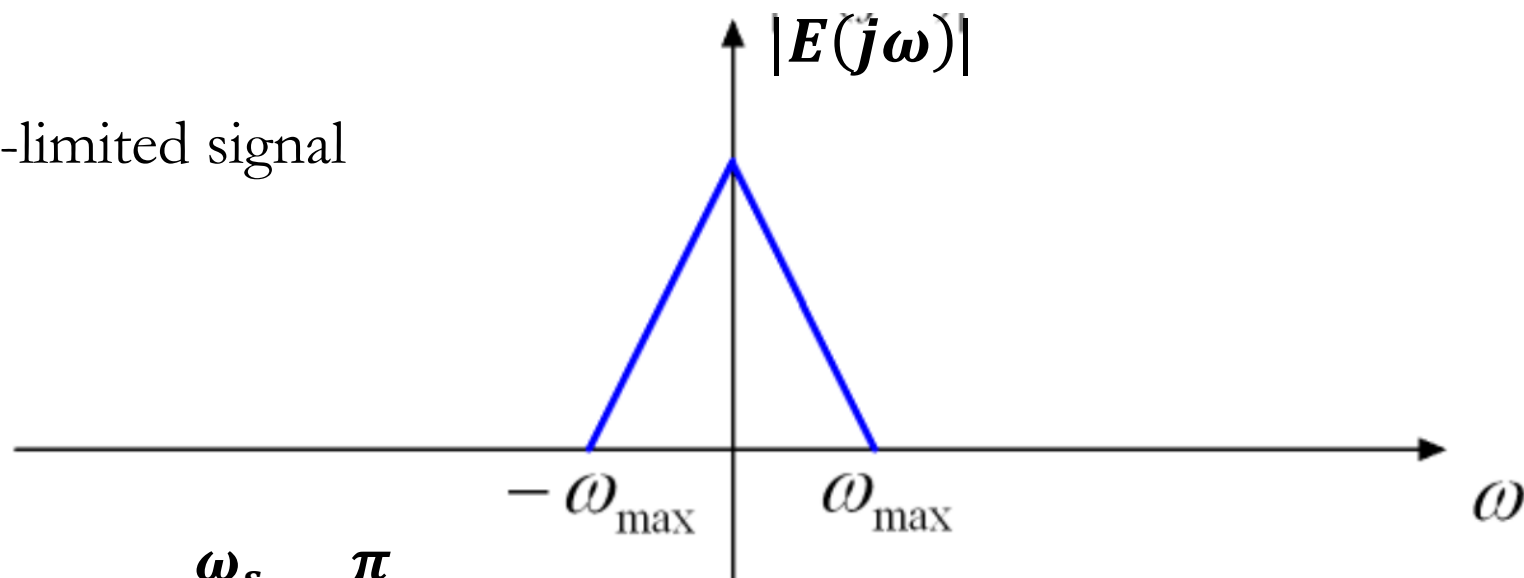


(Fourier transform)

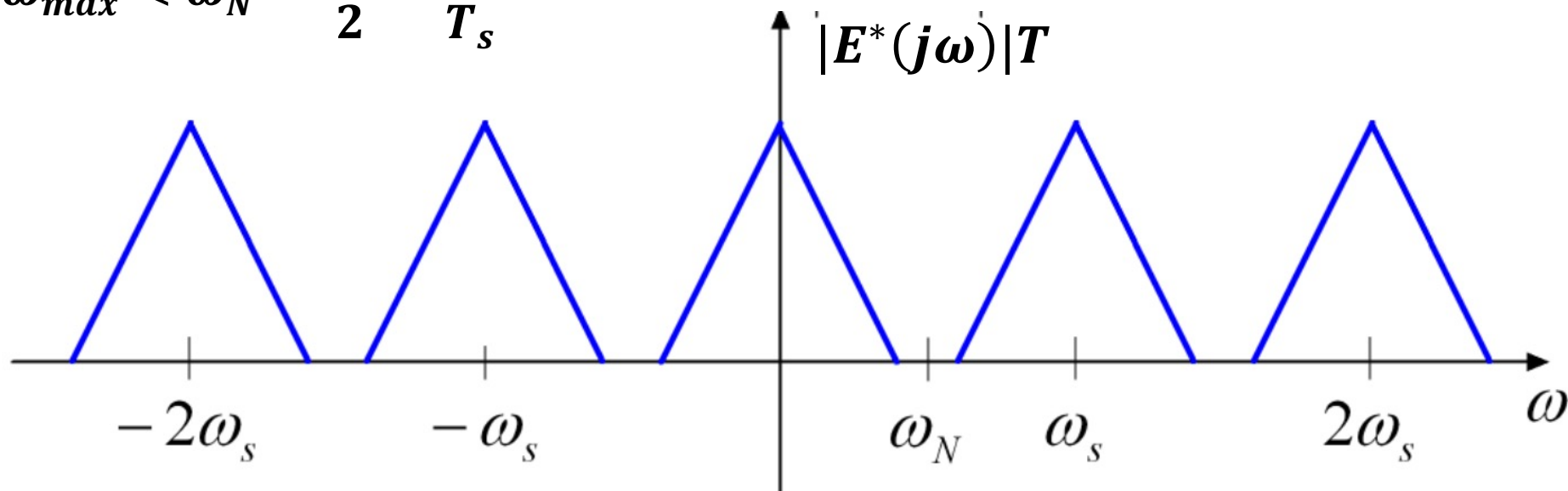
$$E^*(j\omega) = \frac{1}{T} \sum_{n=-\infty}^{+\infty} E(j\omega + jn\omega_s)$$

Ideal sampler – Spectrum of a sampled signal

Band-limited signal

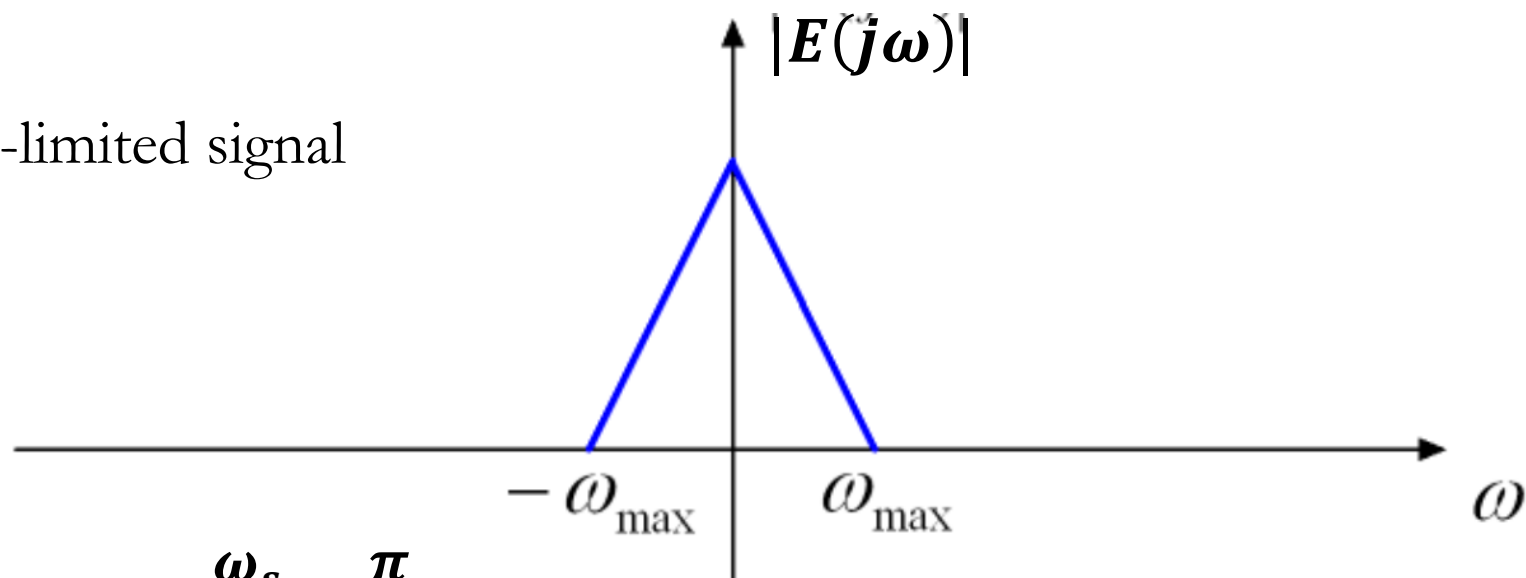


$$\omega_{\max} < \omega_N = \frac{\omega_s}{2} = \frac{\pi}{T_s}$$

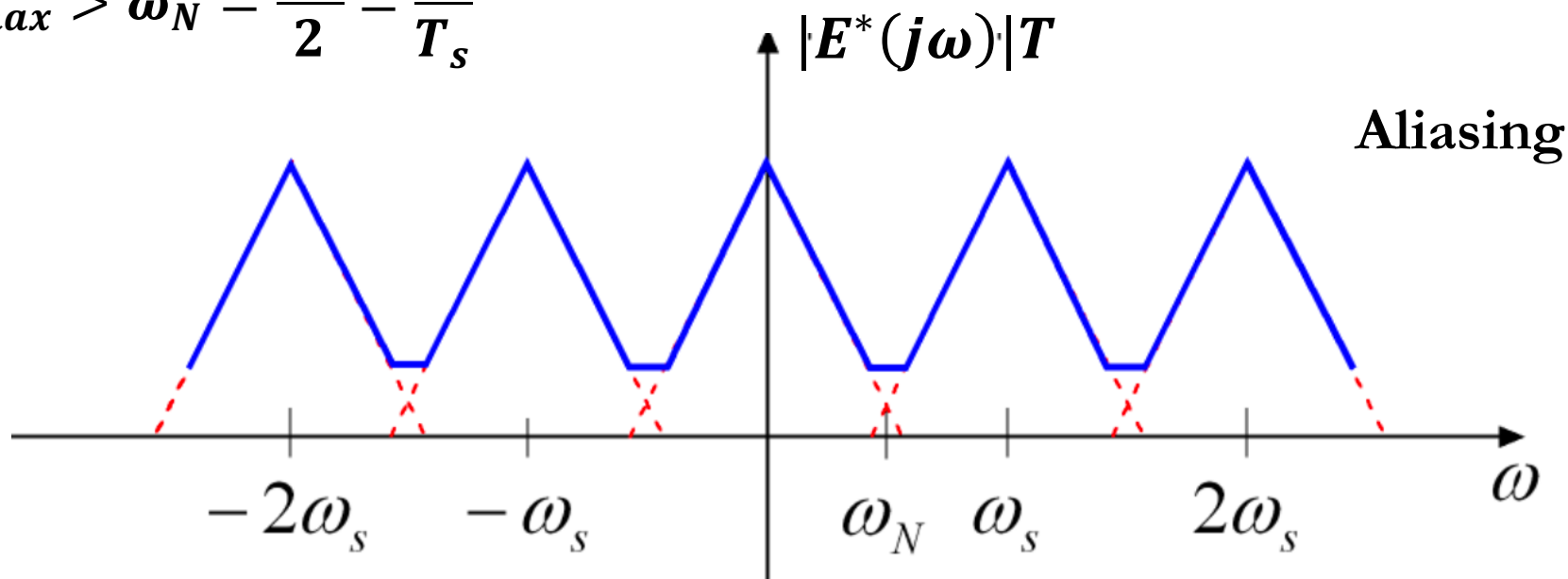


Ideal sampler – Spectrum of a sampled signal

Band-limited signal



$$\omega_{\max} > \omega_N = \frac{\omega_s}{2} = \frac{\pi}{T_s}$$



Aliasing



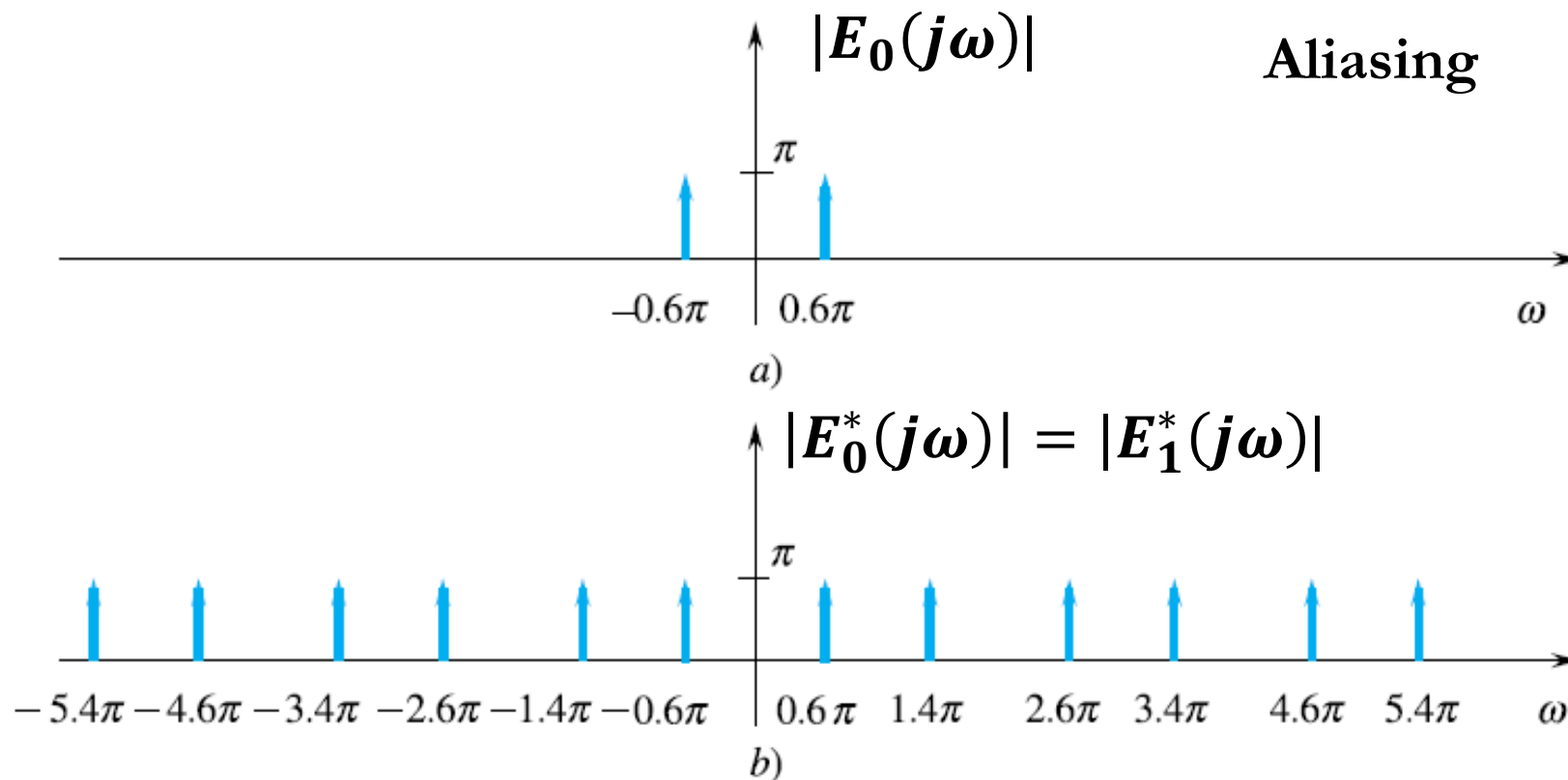
Shannon's Theorem

In order for an analog signal ($e(t)$) to be reconstructed from its sampled version ($e^*(k)$), by Shannon's theorem, it must have a strictly limited bandwidth and $\omega_s > 2\omega_{max}$

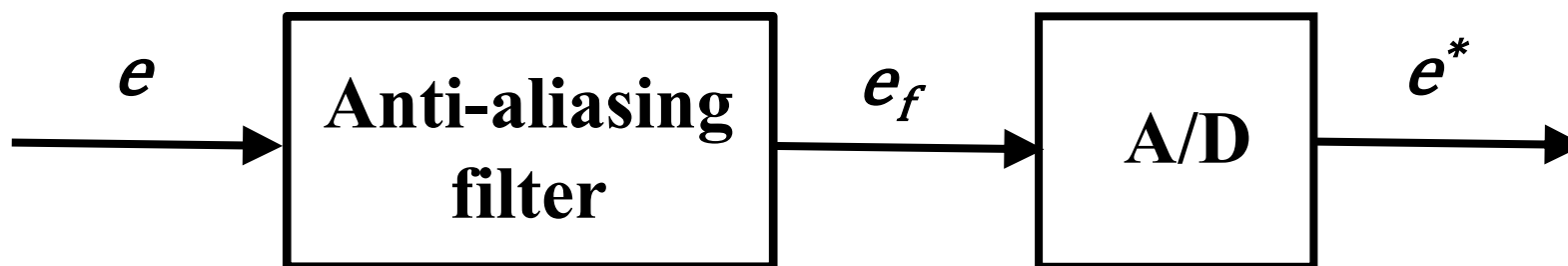
$$\omega_s > 2\omega_{max}$$

$$e_0(t) = \sin(0.6\pi t)$$

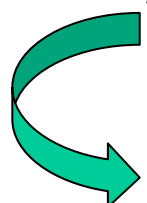
$$e_{-1}(t) = \sin(-1.4\pi t)$$



Antialiasing filter



In this way the spectrum of the signal to be sampled doesn't have significant components for $\omega > \omega_f$

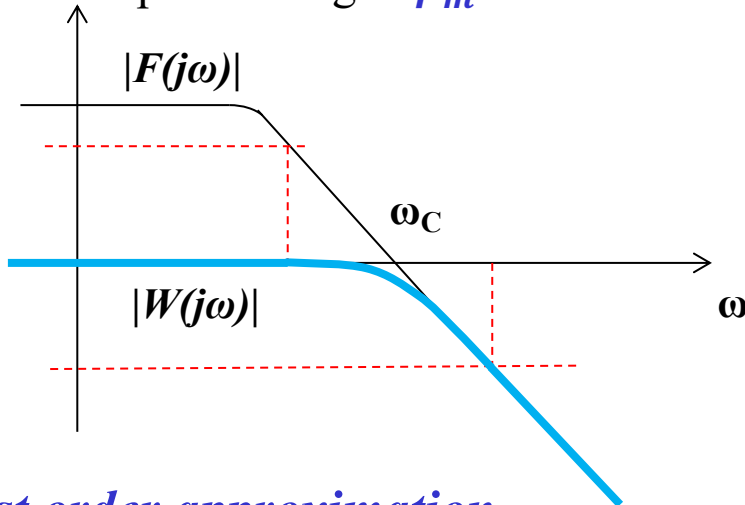
$$\omega_f < \omega_N = \frac{\omega_s}{2}$$

$$\omega_s > 2\omega_f$$

Bandwidth of the control system

Taking into account the bandwidth of the control system, approximated by ω_c , then for Shannon's Theorem

$$\omega_s > 2\omega_c$$

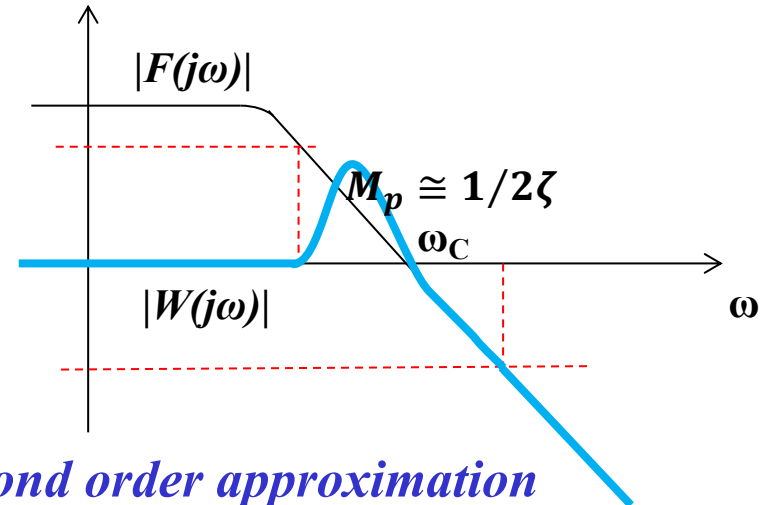
CASE 1: phase margin $\varphi_m > 60^\circ$



First order approximation

$$W_a(s) = \frac{1}{1 + s/\omega_c}$$

CASE 2: phase margin $\varphi_m < 60^\circ$



Second order approximation

$$W_a(s) = \frac{1}{1 + 2\zeta s/\omega_c + s^2/\omega_c^2} \quad \text{and} \quad \zeta \cong \frac{\varphi_m}{100}$$



Antialiasing filter – Bandwidth of the control system

The antialiasing filter can reduce the phase margin by destabilizing the entire control system, then

$$\omega_f \gg \omega_c$$

By taking into account all the constraints

$$\omega_s > 2\omega_f \gg \omega_c$$

In general ω_s is given by

$$\alpha\omega_c < \omega_s < 10\alpha\omega_c$$

with $5 \leq \alpha \leq 10$

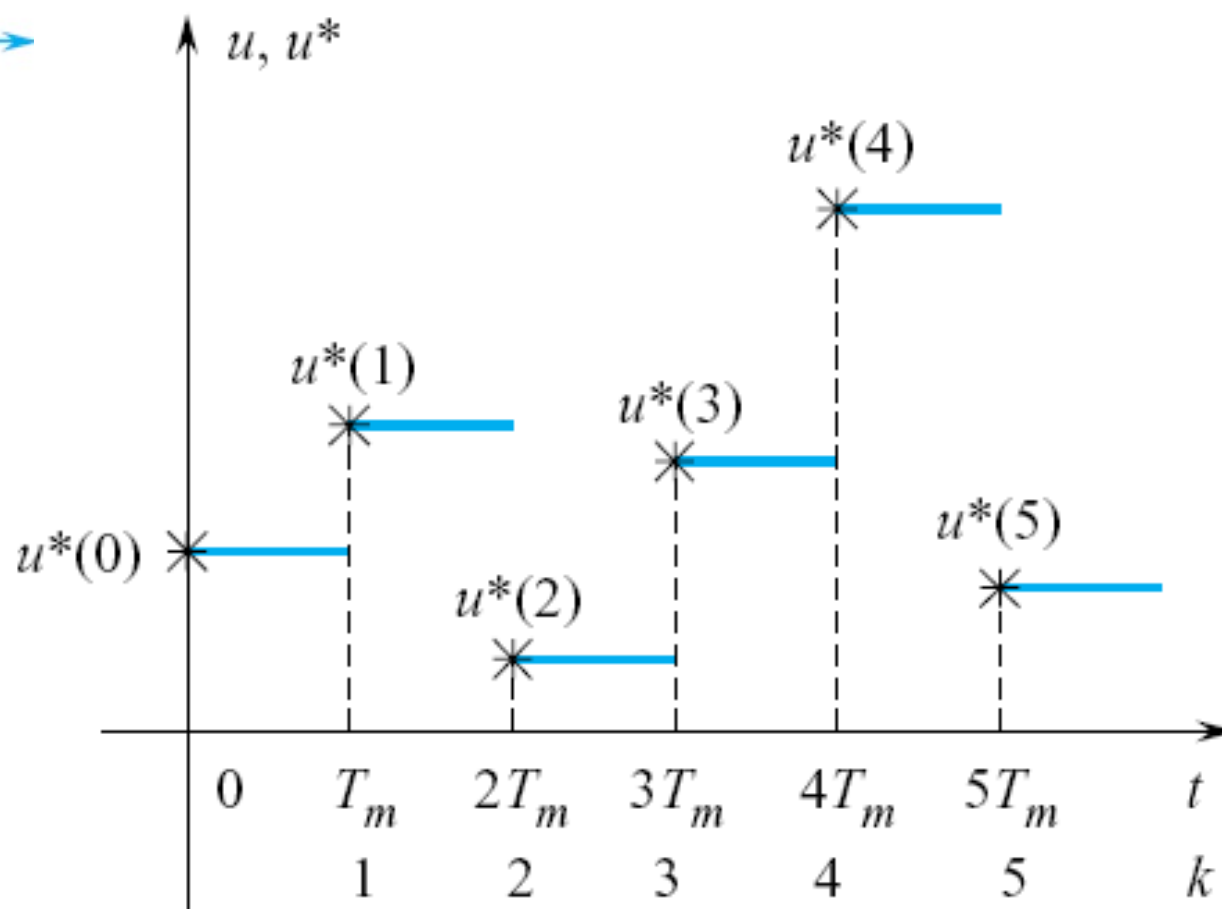


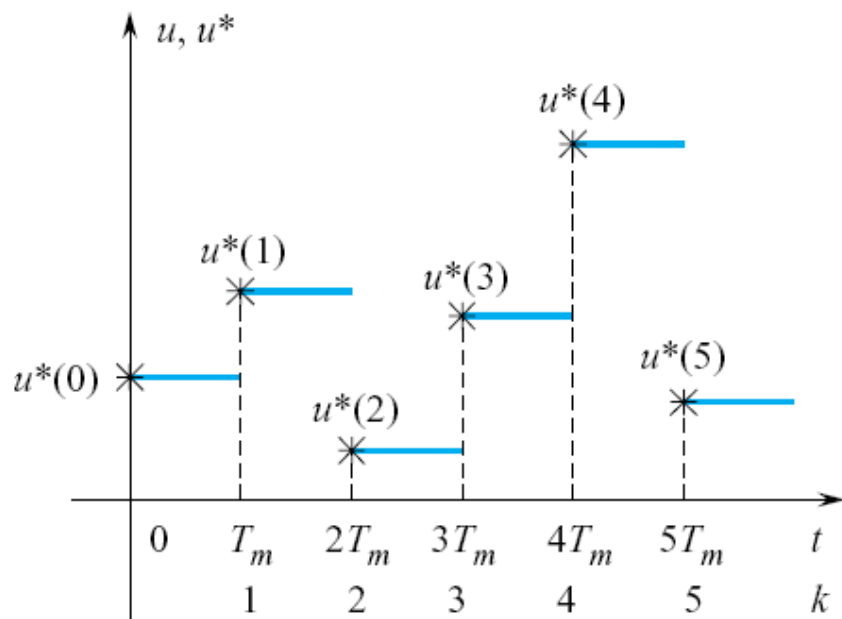
- It is a device that transforms a digital input (binary numbers) to an analog output.
- The most commonly used D/A converter is the zero order hold (ZOH), which operates as follows:

$$u(t) = u^*(k) \quad t \in [kT_m, (k+1)T_m]$$

- T_m is the sample time

ZOH circuit

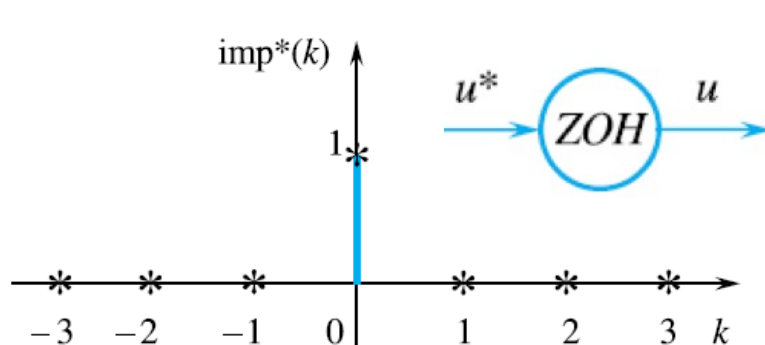




$$u^* \rightarrow \text{ZOH} \rightarrow u \quad \omega_m = 2\pi f_m = \frac{2\pi}{T_m}$$

$$u(t) = u^*(k) \quad t \in [kT_m, (k+1)T_m]$$

Relationship in terms of transform between the input samples $u^*(k)$ and the output signal $u(t)$ ($T = T_m$)




$$u(t) = h_0(t) = 1(t) - 1(t - T)$$

$$\downarrow \mathcal{L}$$

$$H_0(s) = \frac{1 - e^{-sT}}{s}$$

In general, for an input sequence $u^*(k)$ with zeta-Transform $U^*(z)$, the corresponding output signal

$$u(t) = \sum_{k=0}^{\infty} u^*(k) h_0(t - kT) \xrightarrow{\mathcal{L}} U(s) = \sum_{k=0}^{\infty} u^*(k) e^{-skT} H_0(s) = H_0(s) U^*(e^{sT}).$$

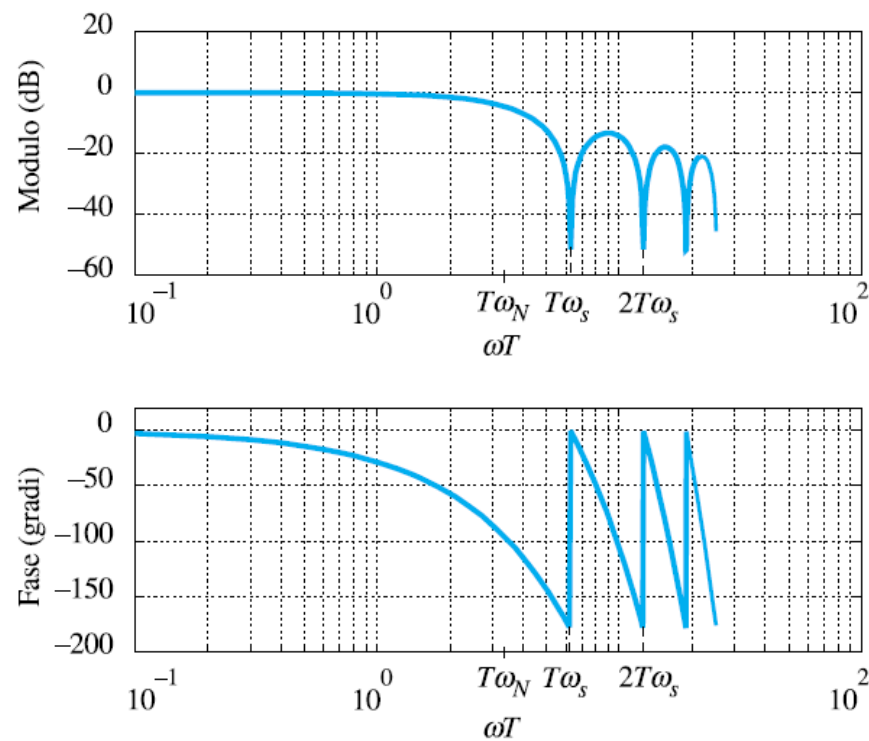
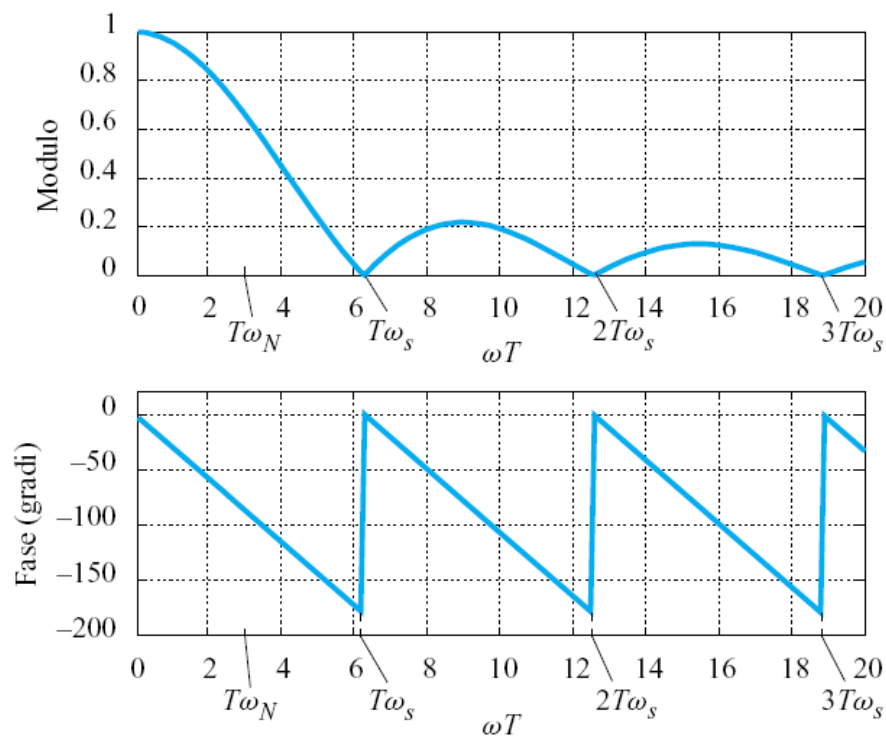
 $H_0(s) = \frac{U(s)}{U^*(e^{sT})}$, it can be assumed as the tf of ZOH

Moreover, for $s = j\omega$, the ZOH frequency response can be evaluated

$$H_0(j\omega) = \frac{1 - e^{-j\omega T}}{j\omega} = e^{-j\omega T/2} \frac{e^{-j\omega T/2} - e^{j\omega T/2}}{2j} 2j = T e^{-j\omega T/2} \frac{\sin \omega T/2}{\omega T/2}$$

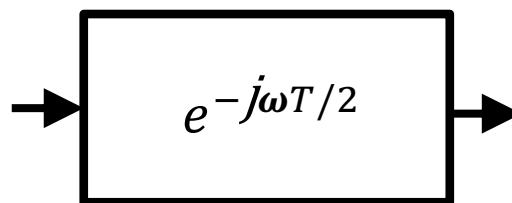
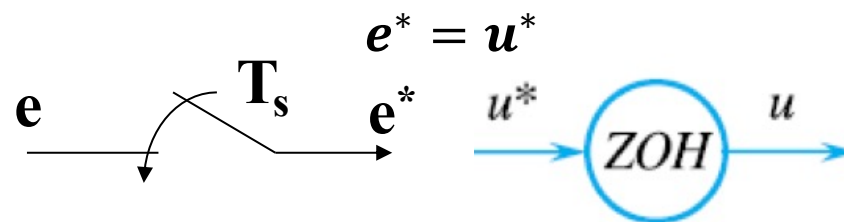
Frequency response of **ZOH**:

Bode Diagrams of $\mathbf{H_0(j\omega)/T}$ in linear and log. scale ($\omega_N = \pi/T$)



Sampler – ZOH series

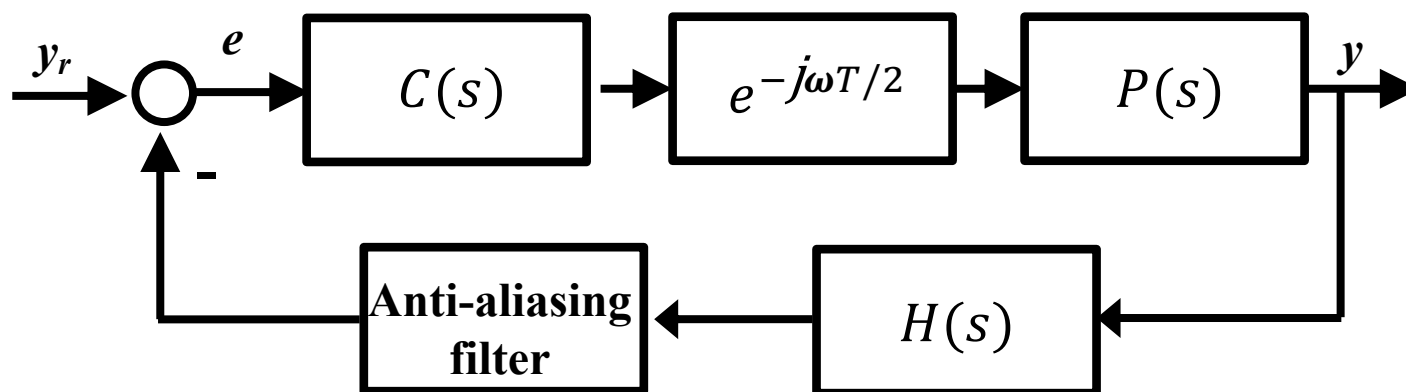
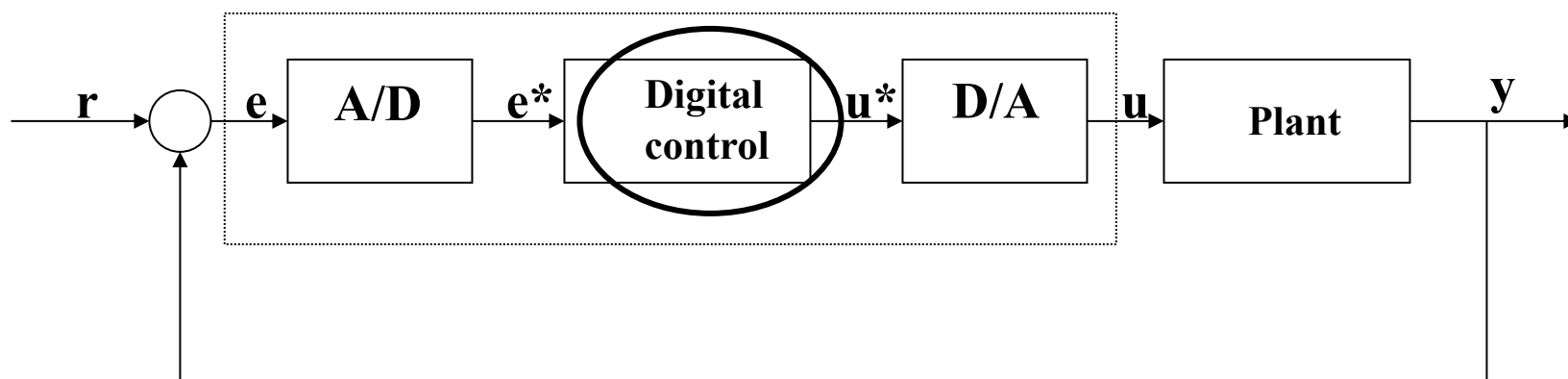
- By working in the frequency range $\omega < \frac{\omega_s}{8}$, it is possible to approximate the sampler-zoh series (hp $T_s = T_m = T$) with a delay element



$$\frac{\omega T}{2} \Big|_{\omega = \frac{\omega_s}{8}} \approx 22^\circ$$

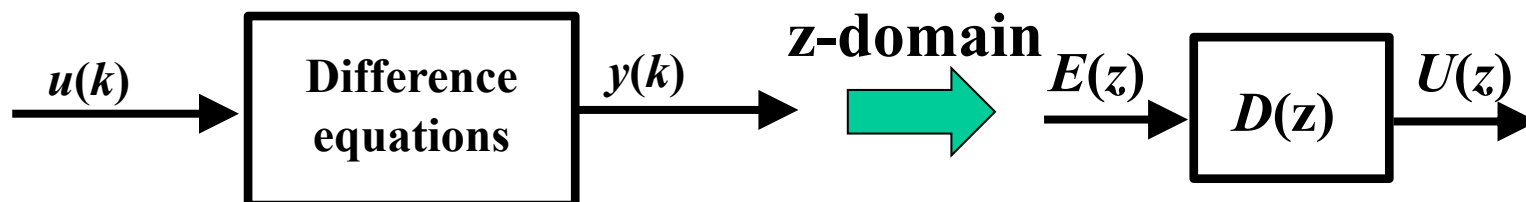
- where this term introduces a maximum delay equal to
- The presence of a numerical control tends to destabilize the entire system.

Scheme of the digital control system in continuous-time



From analog to digital

- Implementation of the digital control:



- From $C(s)$ we want to find an equivalent $D(z)$:
- A transformation allows the transition from continuous time to discrete time such that

$$C(s) \cong D(z)$$

same static and dynamic performance

$$s \longrightarrow z$$

- Several transformations:

The Laplace transform of an ideally sampled signal corresponds to the Zeta of the sampled sequence with the substitution

$$z = e^{sT}$$

By a first-order Padé approximant of the natural logarithm function,

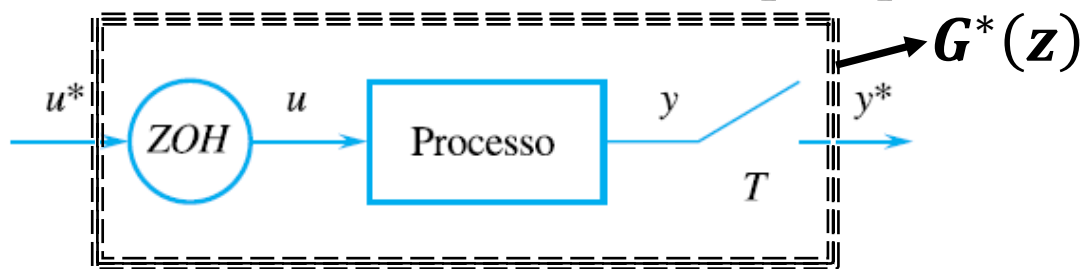
$$s = \frac{2z - 1}{Tz + 1}$$

Others: By Euler's method,

$$s = \frac{z-1}{T} \text{ (forward rectangular rule) and } s = \frac{z-1}{zT} \text{ (backward)}$$

Sampled-data system – 1

Here, we develop the analysis needed to compute the discrete transfer function between the samples that come from the digital computer to the D/A converter and the samples picked up by A/D converter.



This scheme represents a discrete time system describing the continuous time systems at the sampling times (it describes the relationship between u^* and y^*)

The discrete tf, $G^*(z)$, corresponds to the z-Transform of the output samples y_δ^* ($Y_\delta^*(z)$) when the input samples are the unit pulse $\delta(k)$ at $k = 0$:

$$u_\delta^*(k) = \delta(k) \rightarrow U_\delta^*(z) = Z(\delta(k)) = 1 \rightarrow G^*(z) = \frac{Y_\delta^*(z)}{U_\delta^*(z)} = Y_\delta^*(z)$$

Sampled -data system - 2



For $u^*(k) = \delta(k) \rightarrow u(t) = h_0(t) = 1(t) - 1(t - T)$

$$\xrightarrow{\mathcal{L}} H_0(s) = \frac{1 - e^{-sT}}{s}$$

Then $y_\delta(t)$ is the difference between the step response of $G(s)$ (i.e., response to $1(t)$, denoted with $y_s(t)$) and the delayed (T) step response, denoted with $y_s(t - T)$. Thus, by applying Laplace,

$$Y_\delta(s) = H_0(s)G(s) = \frac{1 - e^{-sT}}{s} G(s) = (1 - e^{-sT}) \frac{G(s)}{s} = (1 - e^{-sT}) Y_s(s)$$

$$\xrightarrow{\mathcal{L}^{-1}} y_\delta(t) = y_s(t) - y_s(t - T)$$

By sampling: $y_\delta^*(kT) = y_s(KT) - y_s((k - 1)T)$

And by applying z-transform ($Y(z) = Z(y_s(KT))$):

$$Y_\delta^*(z) = Y(z) - \frac{Y(z)}{z} = \frac{z-1}{z} Y(z)$$

$$\rightarrow G^*(z) = Y_{\delta}^*(z) = \frac{z-1}{z} Y(z) = \frac{z-1}{z} Z \left(\mathcal{L}^{-1} \left(\frac{G(s)}{s} \right) \Big|_{t=KT} \right)$$

Summarizing, by this procedure it is possible to obtain the discrete tf of the sampled-data system, $G^*(z)$:

1. Determine the step response of the continuous LTI system in the Laplace domain, $Y_s(s) = \frac{G(s)}{s}$.
2. Antitransform $Y_s(s)$ thereby determining the samples of the output $y_s(kT)$.
3. Compute the z-transform of the output samples $y_s(kT)$:
 $Z(y_s(kT))$
4. Determine the tf of $G^*(z) = \frac{z-1}{z} Z(y_s(kT))$

Sampled -data system - Example

What is the discrete transfer function of

$$G(s) = \frac{1}{s(s+1)},$$

preceded by a ZOH?

Solution:

1. $Y(s) = \frac{G(s)}{s} = \frac{1}{s^2(s+1)} = \frac{1}{s^2} - \frac{1}{s} + \frac{1}{s+1}$
2. $y_s(kT) = \mathcal{L}^{-1}(Y(s))|_{t=KT} = (t - 1 + e^{-t})1(t)|_{t=KT} = (kT - 1 + e^{-kT})1(kT)$
3. $Z(y_s(kT)) = \frac{Tz}{(z-1)^2} - \frac{z}{z-1} + \frac{z}{z-e^{-T}}$
4. $G^*(z) = \frac{z-1}{z} \left(\frac{Tz}{(z-1)^2} - \frac{z}{z-1} + \frac{z}{z-e^{-T}} \right) = \frac{T}{z-1} - 1 + \frac{z-1}{z-e^{-T}}$